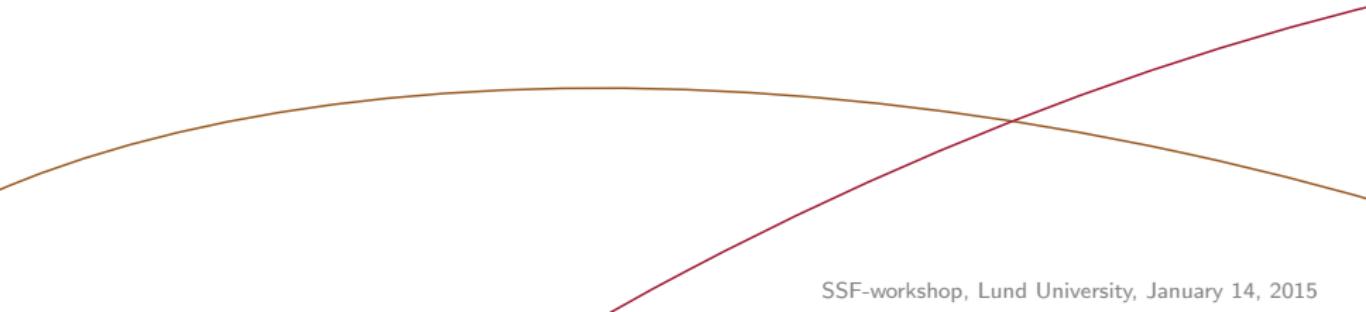




# Electromagnetic energy and antennas

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- ▶ Doruk Tayli, Lund University
- ▶ Sven Nordebo, Linnæus University
- ▶ Lars Jonsson, KTH

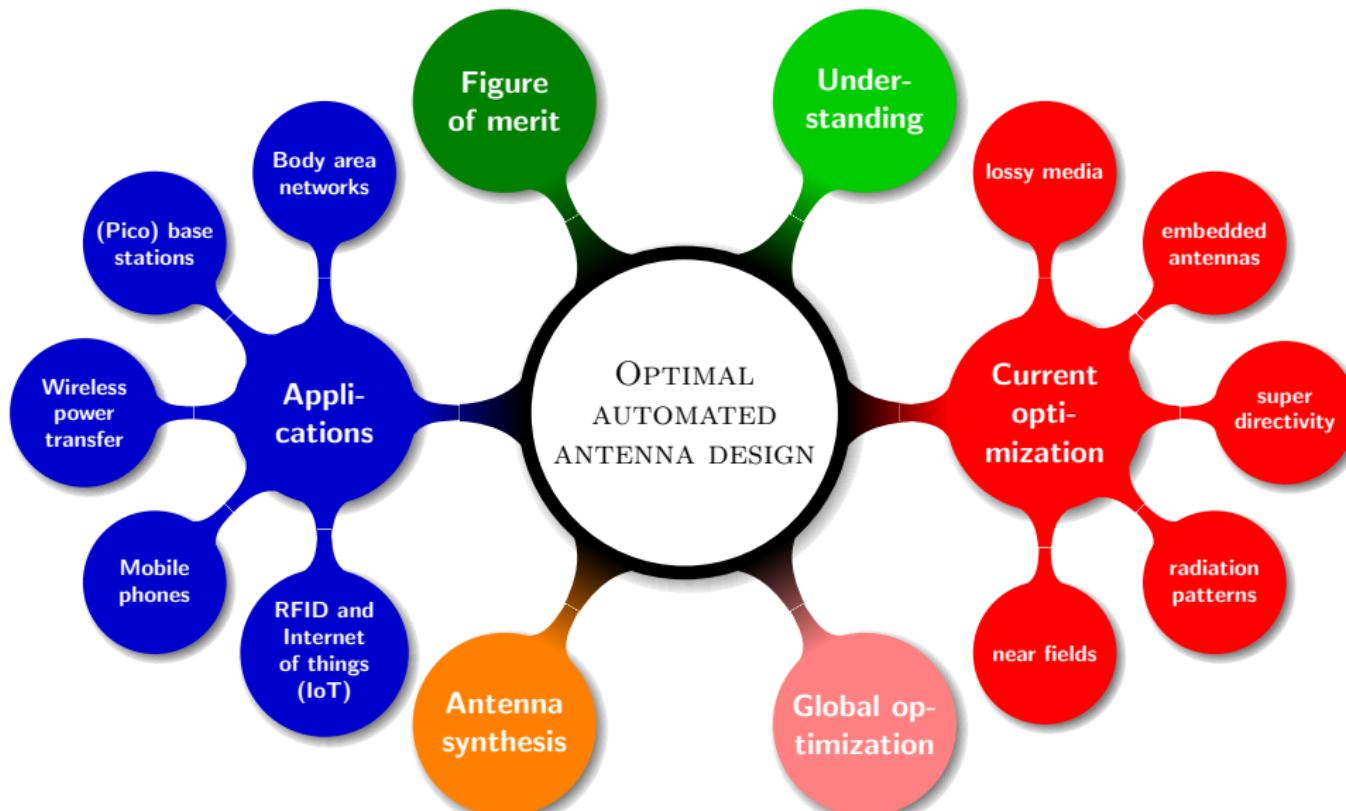


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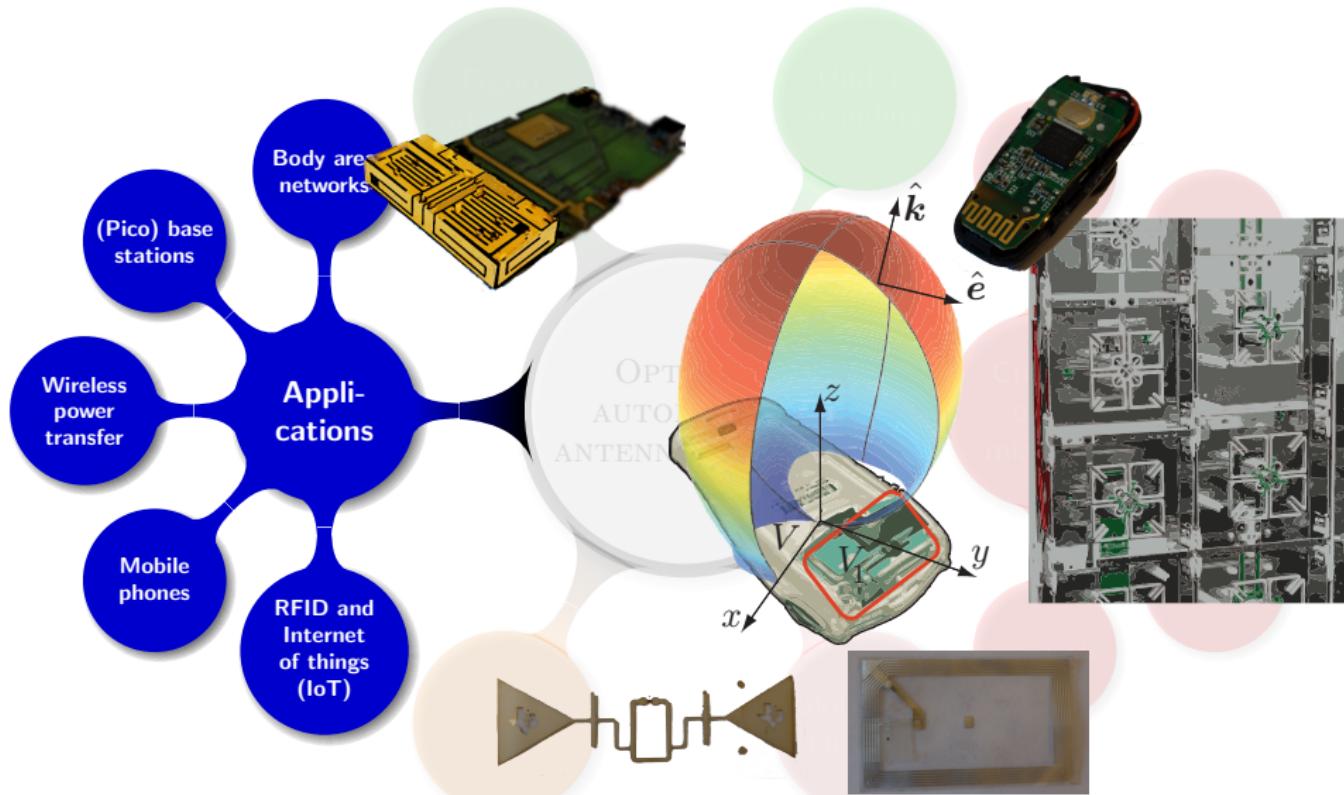


SWEDISH FOUNDATION for  
STRATEGIC RESEARCH

# Optimal (automated) antenna design



# Optimal (automated) antenna design

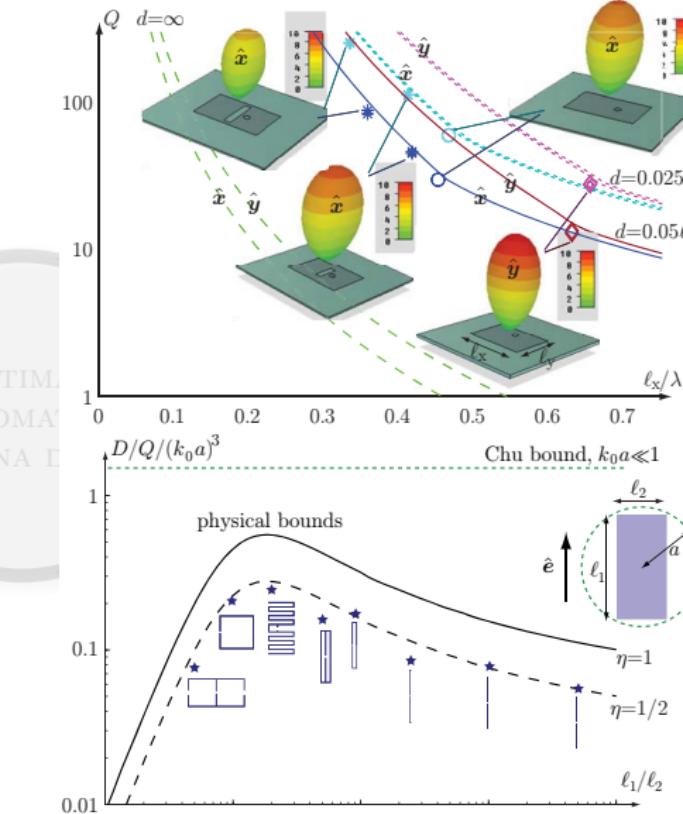


# Optimal (automated) antenna design

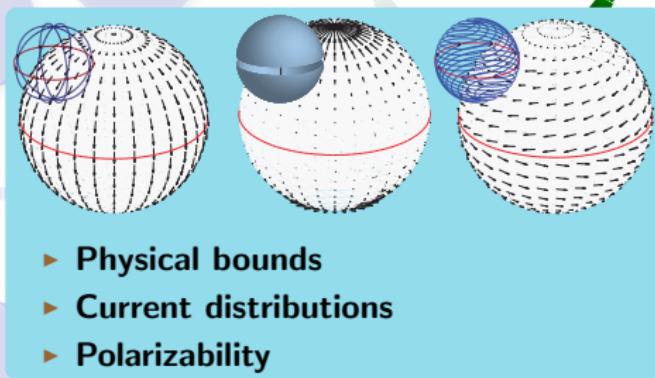
Figure  
of merit

Performance of an antenna design in relation to the optimal performance

- ▶ % from the optimal design
- ▶ a useful number to compare designs
- ▶ is it worth to improve a design?
- ▶ ...

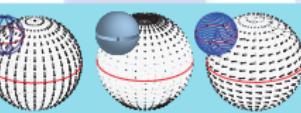


# Optimal (automated) antenna design



Understanding

# Optimal (automated) antenna design



- ▶ Optimal current distribution
- ▶ Physical bounds
- ▶ Convex optimization
- ▶ ...

OPTIMAL  
AUTOMATED  
ANTENNA DESIGN

Current  
optimization

near fields

radiation patterns

super directivity

embedded  
antennas

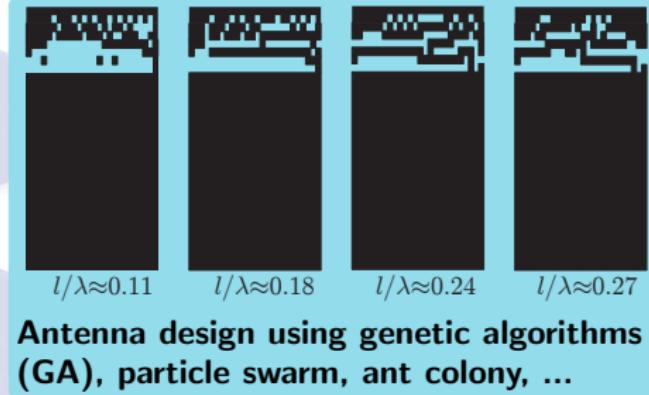
lossy media

multiple  
sources

multiple  
outputs

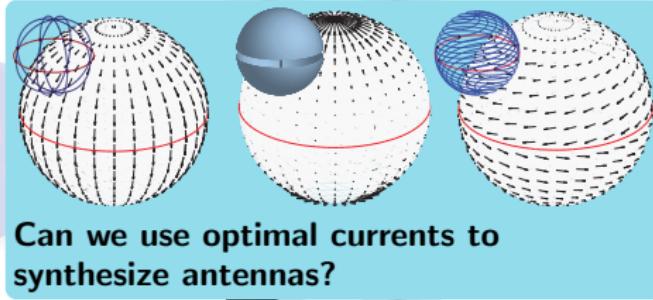
multiple  
polarizations

# Optimal (automated) antenna design



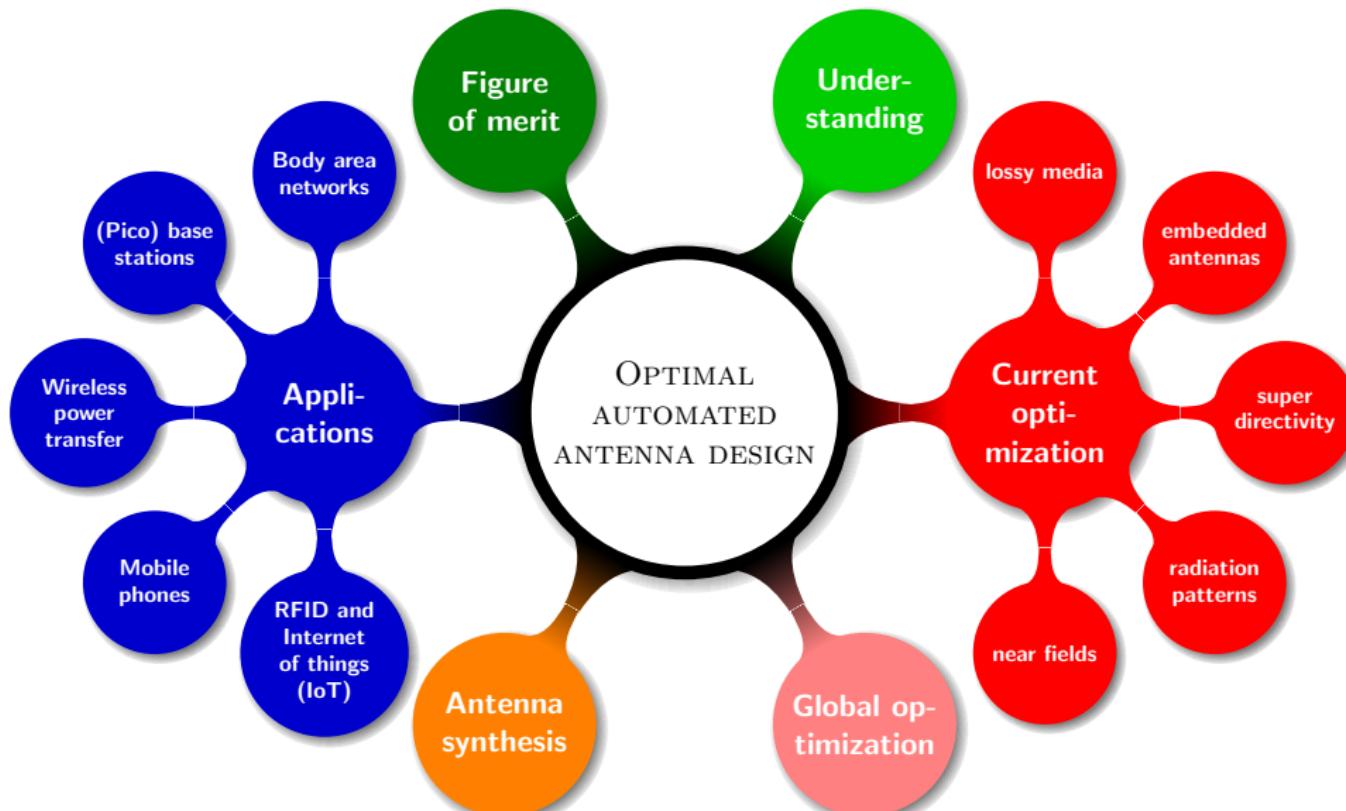
Global optimization

# Optimal (automated) antenna design



Antenna  
synthesis

# Optimal (automated) antenna design



# Optimization of antenna currents: examples

## Gain over Q

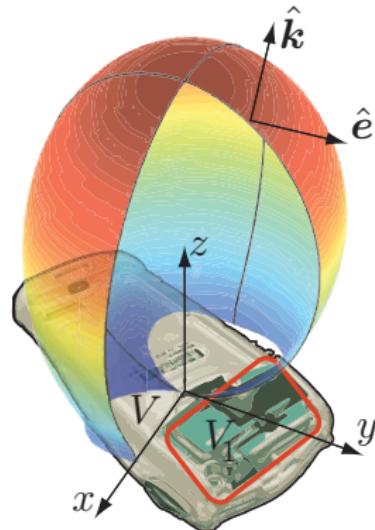
minimize    Stored energy  
subject to    Radiation intensity =  $P_0$

**Q for superdirective**  $D \geq D_0$ .

minimize    Stored energy  
subject to    Radiation intensity =  $D_0 P_{\text{rad}} / (4\pi)$   
                 Radiated power  $\leq P_{\text{rad}}$

## Embedded structures

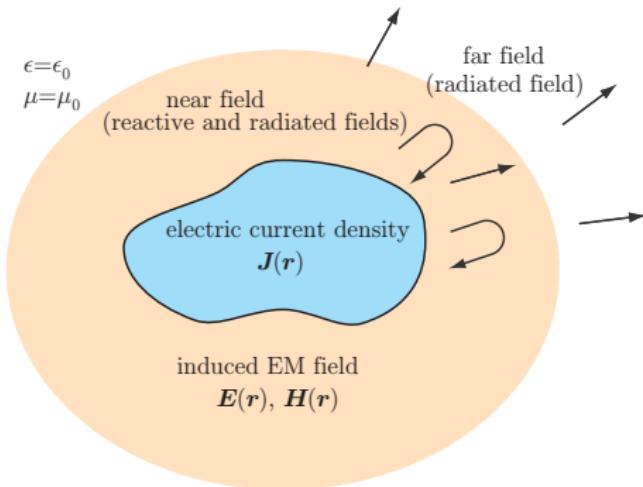
minimize    Stored energy  
subject to    Radiation intensity =  $P_0$   
                 Correct induced currents



Need to:

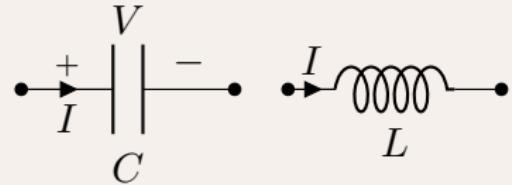
1. Express the *stored energy* in the current density  $\mathbf{J}$ .
2. Solve the optimization problems.

# What is (stored) EM energy?



- ▶ Time average energy density  $\epsilon_0|\mathbf{E}|^2/4$  and  $\mu_0|\mathbf{H}|^2/4$ .
- ▶ What is stored and radiated?
- ▶ How can we express the (stored) energy in the current density?
- ▶ Here, currents in free space.

## Lumped elements



Time average stored energy in capacitors

$$W^{(E)} = \frac{C|V|^2}{4} = \frac{|I|^2}{4\omega^2 C}$$

and in inductors

$$W^{(M)} = \frac{L|I|^2}{4}$$



$$\frac{\epsilon_0}{4} \int_{\mathbb{R}_r^3} |\mathbf{E}|^2 - \frac{|\mathbf{F}|^2}{r^2} dV$$

Far fields  
and  $X'_{in}$

$Q$

Current  
density

STORED ENERGY  
AND  $Q$

Brune

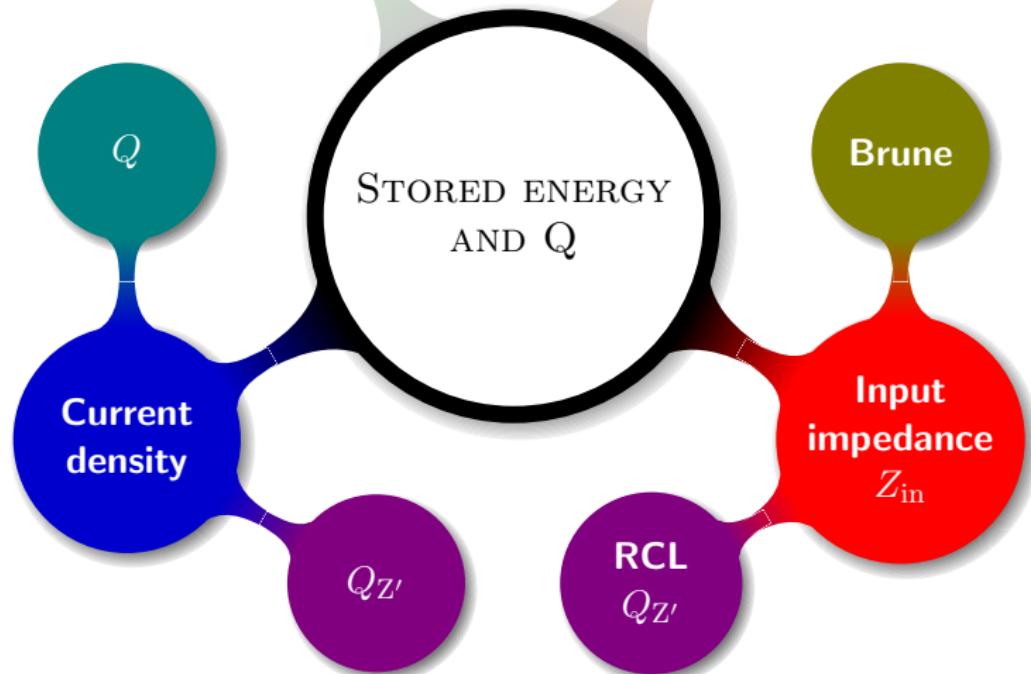
Input  
impedance  
 $Z_{in}$

$Q_{Z'}$

RCL  
 $Q_{Z'}$

$$\frac{\epsilon_0}{4} \int_{\mathbb{R}_r^3} |\mathbf{E}|^2 ds - \frac{|\mathbf{F}|^2}{r^2} dV$$

$$\frac{|I_0|^2}{4} X'_{in} - \frac{1}{2\eta_0} \text{Im} \int_{\Omega} \mathbf{F}' \cdot \mathbf{F}^* d\Omega$$



$$\frac{\epsilon_0}{4} \int_{\mathbb{R}_r^3} |\mathbf{E}|^2 ds - \frac{|\mathbf{F}|^2}{r^2} dV$$

$$\frac{|I_0|^2}{4} X'_{in} - \frac{1}{2\eta_0} \text{Im} \int_{\Omega} \mathbf{F}' \cdot \mathbf{F}^* d\Omega$$

$Q$

STORED ENERGY  
AND  $Q$

Current  
density

$Q_{Z'}$

Kirchhoff  
 $\mathbf{Z}\mathbf{I}_{in} = \mathbf{V}$   
 $\frac{1}{4} \mathbf{I}^H \mathbf{X}' \mathbf{I}$

Input  
 $Z_{in} I_{in} = V_{in}$   
 $Z_{in}$

$$|Z'_{in}| = \frac{|\mathbf{I}^T \mathbf{X}' \mathbf{I}|}{|I_{in}|^2}$$

## STORED ENERGY AND Q

$$\frac{1}{4} \mathbf{I}^H \mathbf{X}' \mathbf{I}$$

$$\text{MoM} \\ \mathbf{Z} \mathbf{I}_{\text{arity}} = \mathbf{V}$$

$$\frac{1}{4} |\mathbf{I}^T \mathbf{Z}' \mathbf{I}|$$

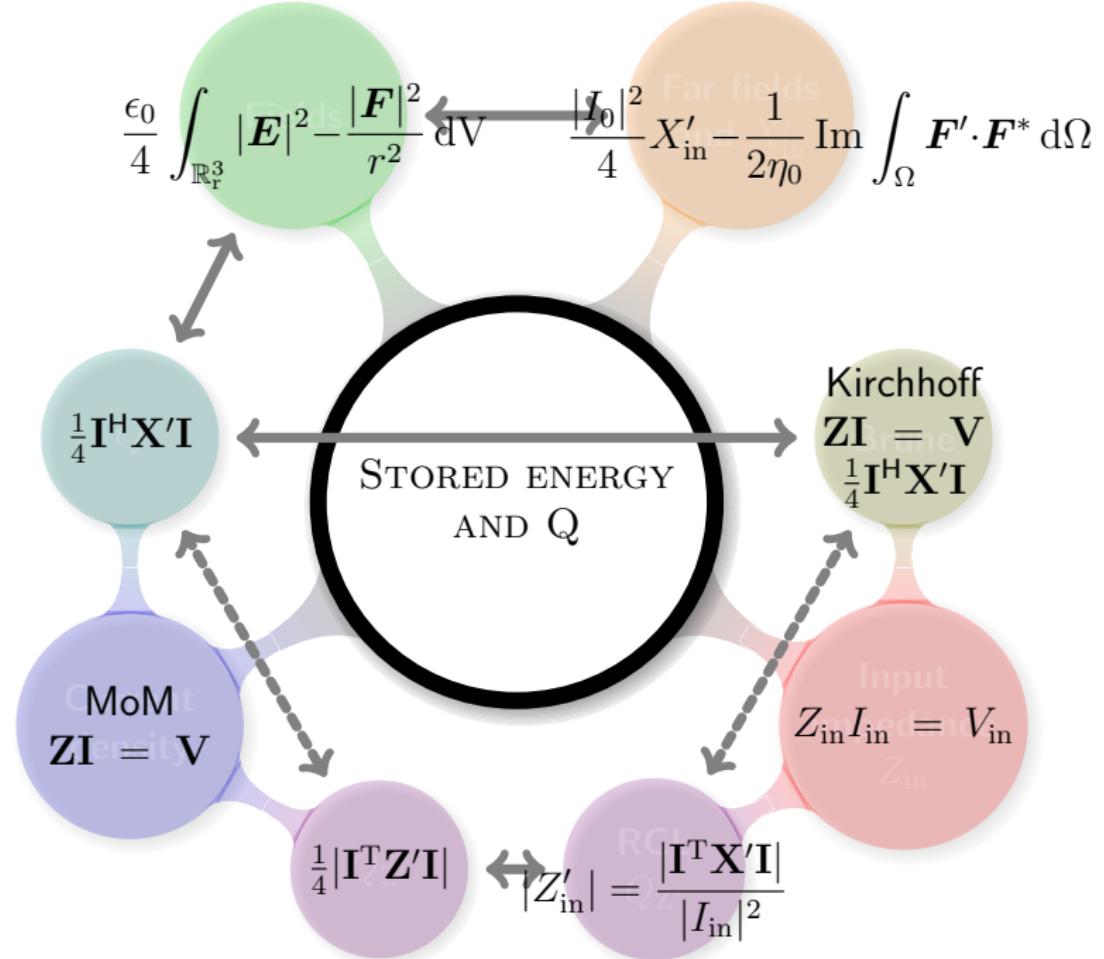
$$|Z'_{\text{in}}| = \frac{|\mathbf{I}^T \mathbf{X}' \mathbf{I}|}{|I_{\text{in}}|^2}$$

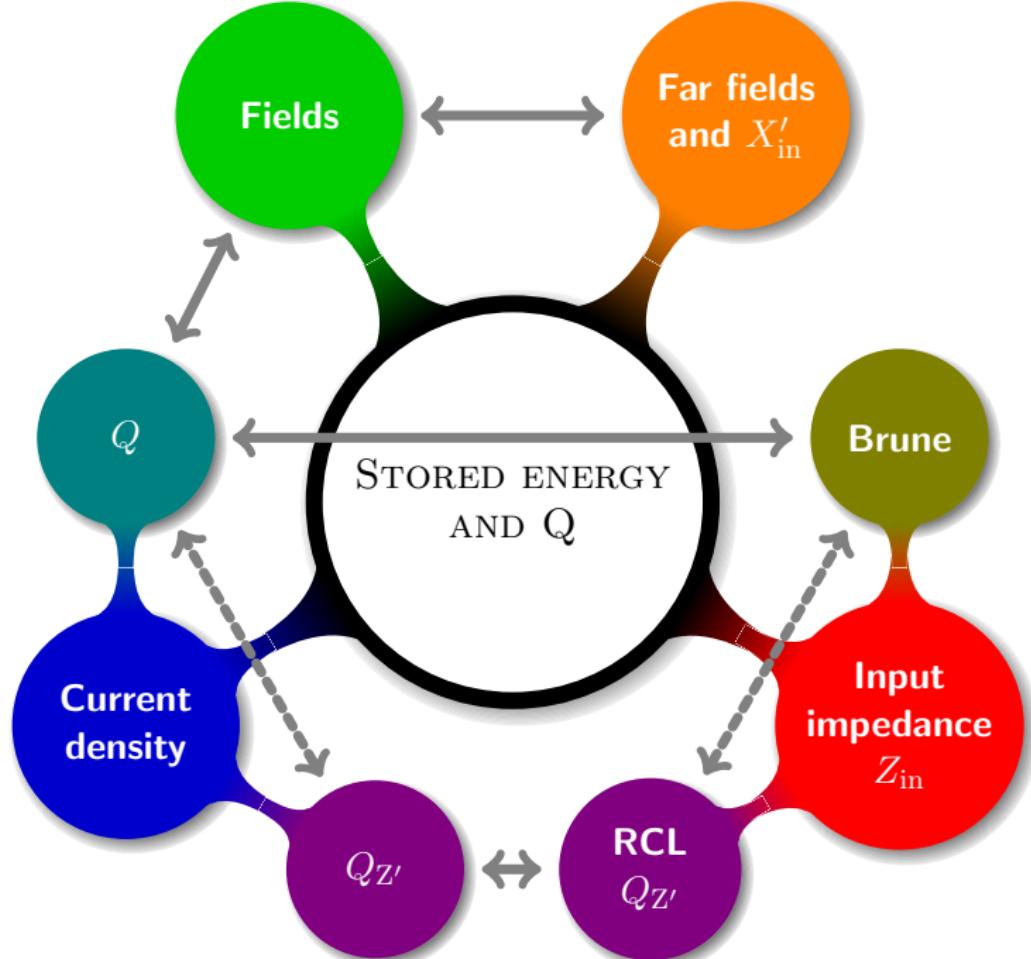
$$\text{Kirchhoff} \\ \mathbf{Z} \mathbf{I}_{\text{brane}} = \mathbf{V} \\ \frac{1}{4} \mathbf{I}^H \mathbf{X}' \mathbf{I}$$

$$\text{Input} \\ Z_{\text{in}} I_{\text{in}} = V_{\text{in}} \\ Z_{\text{in}}$$

$$\frac{\epsilon_0}{4} \int_{\mathbb{R}_r^3} |\mathbf{E}|^2 ds - \frac{|\mathbf{F}|^2}{r^2} dV$$

$$\frac{|I_0|^2}{4} X'_{\text{in}} - \frac{1}{2\eta_0} \text{Im} \int_{\Omega} \mathbf{F}' \cdot \mathbf{F}^* d\Omega$$





## MoM for $Q$ and $Q_{Z'}$ (I)

---

Use a method of moments (MoM) formulation of the electric field integral equation (EFIE). Impedance matrix  $\mathbf{Z} = \mathbf{R} + j\mathbf{X}$

$$\frac{Z_{mn}}{\eta} = j \int_S \int_S \left( k^2 \psi_{m1} \cdot \psi_{n2} - \nabla_1 \cdot \psi_{m1} \nabla_2 \cdot \psi_{n2} \right) \frac{e^{-jkr_{12}}}{4\pi kr_{12}} dS_1 dS_2$$

where  $\psi_{n1} = \psi_n(\mathbf{r}_1)$ ,  $\psi_{n2} = \psi_n(\mathbf{r}_2)$ ,  $n = 1, \dots, N$ , and  $r_{12} = |\mathbf{r}_1 - \mathbf{r}_2|$ .

The current density is  $\mathbf{J}(\mathbf{r}) = \sum_{n=1}^N I_n \psi_n(\mathbf{r})$  with the expansion coefficients determined from

$$\mathbf{ZI} = \mathbf{V} \quad \text{or} \quad \mathbf{I} = \mathbf{Z}^{-1} \mathbf{V} = \mathbf{YV}$$

where  $\mathbf{V}$  is a column matrix with the excitation coefficients.

The input admittance is

$$Y_{in} = 1/Z_{in} = \mathbf{V}^T \mathbf{YV} / V_{in}^2$$

where  $Z_{in} = R_{in} + jX_{in}$  is the input impedance.

## MoM for $Q$ and $Q_{Z'}$ (II)

---

Differentiate the MoM impedance matrix

$$\begin{aligned}\frac{k \partial Z_{mn}}{\eta \partial k} = & \int_V \int_V j \left( k^2 \psi_{m1} \cdot \psi_{n2} + \nabla_1 \cdot \psi_{m1} \nabla_2 \cdot \psi_{n2} \right) \frac{e^{-jkr_{12}}}{4\pi kr_{12}} \\ & + \left( k^2 \psi_{m1} \cdot \psi_{n2} - \nabla_1 \cdot \psi_{m1} \nabla_2 \cdot \psi_{n2} \right) \frac{e^{-jkr_{12}}}{4\pi} dS_1 dS_2\end{aligned}$$

Differentiated input admittance (frequency independent  $\mathbf{V}$  (MoM))

$$V_{\text{in}}^2 Y'_{\text{in}} = (\mathbf{V}^T \mathbf{Y} \mathbf{V})' = \mathbf{V}^T \mathbf{Y}' \mathbf{V} = -\mathbf{I}^T \mathbf{Z}' \mathbf{I}.$$

The stored energy determined from  $\mathbf{X}' = \text{Im } \mathbf{Z}'$

$$W_{\mathbf{X}'}^{(\text{E})} + W_{\mathbf{X}'}^{(\text{M})} = \frac{1}{4} \mathbf{I}^H \mathbf{X}' \mathbf{I}$$

is identical to the stored energy expression (free space) introduced by Vandenbosch (IEEE-TAP 2010), see ?? and already considered by Harrington (1968, 1971, 1975).

## $Q$ and $Q_{Z'}$ for free-space self-resonant antennas

Assume for simplicity a **self-resonant** antenna (circuit)

$$Q_{Z'} = \frac{\omega |Z'_{\text{in}}|}{2R_{\text{in}}} = \frac{\omega |\mathbf{I}^T \mathbf{Z}' \mathbf{I}|}{2\mathbf{I}^H \mathbf{R} \mathbf{I}}$$

and using MoM with the stored energy by Vandenbosch

$$Q = \frac{2\omega \max\{W_{\mathbf{X}'}^{(\text{E})}, W_{\mathbf{X}'}^{(\text{M})}\}}{P_d} = \frac{\omega \mathbf{I}^H \mathbf{X}' \mathbf{I}}{2\mathbf{I}^H \mathbf{R} \mathbf{I}}$$

Transpose for  $Q_{Z'}$  and Hermitian transpose for  $Q$

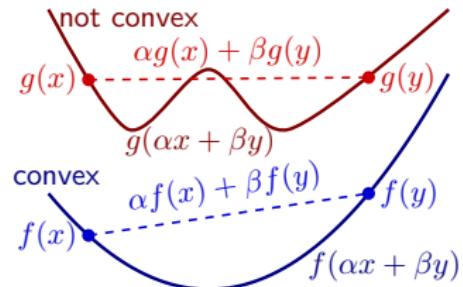
- $\mathbf{I}^H \mathbf{X}' \mathbf{I} \geq 0$  for positive semidefinite matrices  $\mathbf{X}'$ .
- $|\mathbf{I}^T \mathbf{Z}' \mathbf{I}| = 0$  for some  $\mathbf{I}$  (rank > 1).

See also Capek+etal. IEEE-TAP 2014 for  $Q_{Z'}$  using  $\mathbf{I}^H$  and  $\mathbf{I}'$  and  
for stored energy and Q-factors in lumped circuits.

# Convex optimization

minimize  $f_0(\mathbf{x})$

subject to  $f_i(\mathbf{x}) \leq 0, i = 1, \dots, N_1$   
 $\mathbf{A}\mathbf{x} = \mathbf{b}$



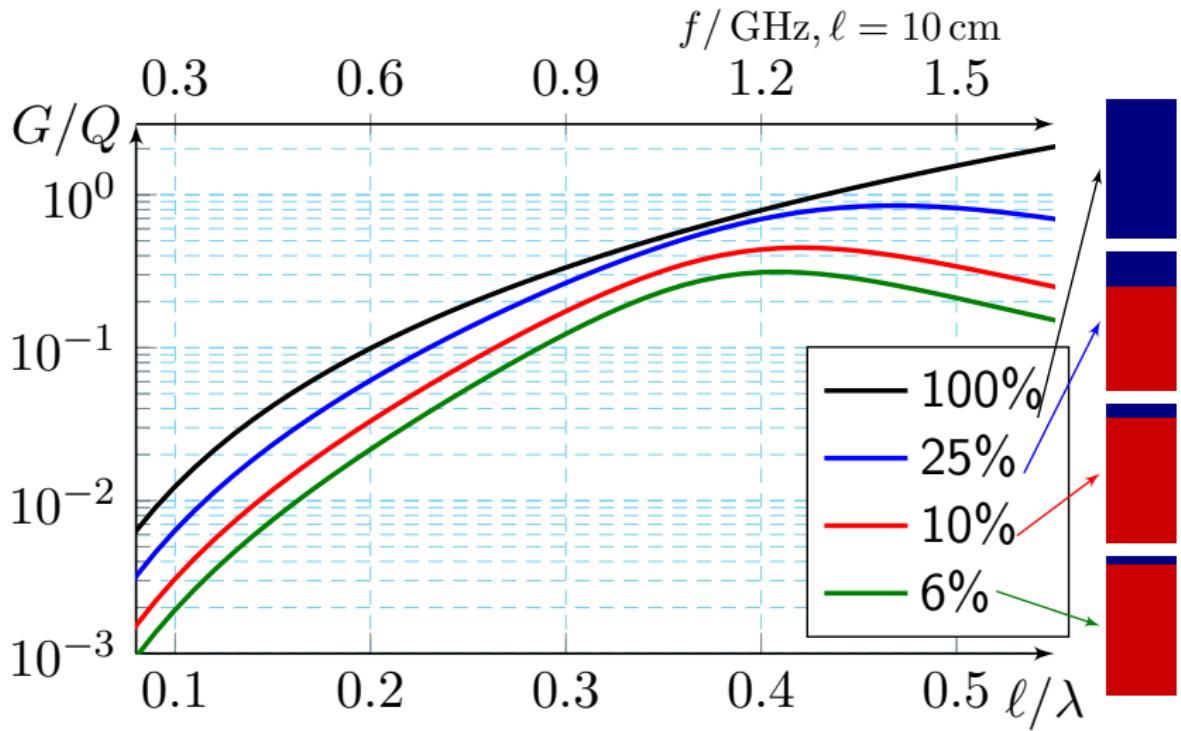
where  $f_i(x)$  are convex, i.e.,  $f_i(\alpha\mathbf{x} + \beta\mathbf{y}) \leq \alpha f_i(\mathbf{x}) + \beta f_i(\mathbf{y})$  for  $\alpha, \beta \in \mathbb{R}, \alpha + \beta = 1, \alpha, \beta \geq 0$ .

Solved with efficient standard algorithms. No risk of getting trapped in a local minimum. A problem is 'solved' if formulated as a convex optimization problem.

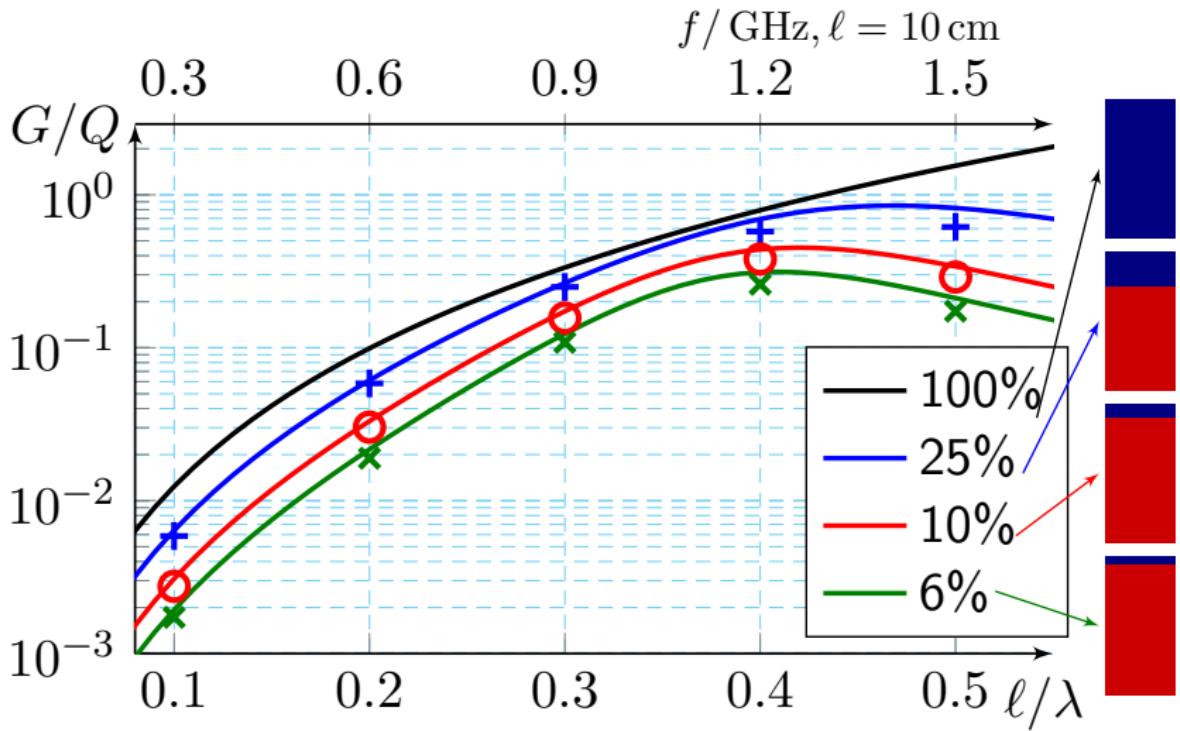
Antenna performance expressed in the current density  $\mathbf{J}$ , e.g.,

- ▶ Radiated field  $\mathbf{F}(\hat{\mathbf{k}}) = -\hat{\mathbf{k}} \times \hat{\mathbf{k}} \times \int_V \mathbf{J}(\mathbf{r}) e^{j\hat{\mathbf{k}} \cdot \mathbf{r}} dV$  is affine.
- ▶ Radiated power, stored electric and magnetic energies, and Ohmic losses are positive semi-definite quadratic forms in  $\mathbf{J}$ .

# Finite ground plane with {6, 10, 25, 100}% antenna region



# Finite ground plane with {6, 10, 25, 100}% antenna region



# Why convex optimization?

**Solved** if formulated as a convex optimization problem.

Consider the  $G/Q$  problem

$$\begin{aligned} & \text{minimize} && \max\{\mathbf{I}^H \mathbf{X}_e \mathbf{I}, \mathbf{I}^H \mathbf{X}_m \mathbf{I}\} \\ & \text{subject to} && \mathbf{F}^H \mathbf{I} = 1 \end{aligned}$$

Many (optimization) algorithms can be used to solve this problem.

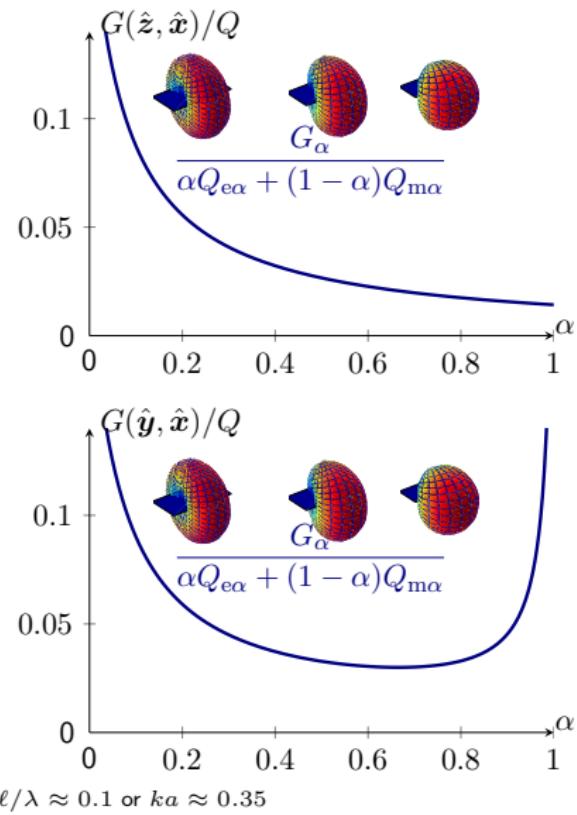
- ▶ Can e.g., use any of the solvers included in CVX.
  - ▶ Very simple to use.
  - ▶ Good for small problems but less efficient for larger problems.
- ▶ A dedicated solver for quadratic programs.
  - ▶ More efficient for larger problems.
- ▶ Random search, eg genetic algorithms (GA), particle swarms,....
  - ▶ Very inefficient. Note you do not (should not) use (GA, ...) to solve e.g.,  $\mathbf{Ax} = \mathbf{b}$  ( $\min. \|\mathbf{Ax} - \mathbf{b}\|$ ).
- ▶ We also use a dual formulation
  - ▶ Computational efficient for large problems.
  - ▶ Illustrates dual problems and posteriori error estimates.

## Why convex optimization: illustration

The upper bound on  $G/Q|_{\text{ub}}$  is obtained by solving the dual (relaxed) problem, i.e., finding the minimum of the (blue) curve

$$\frac{G}{Q} \Big|_{\text{ub}} \leq \frac{G_\alpha}{\alpha Q_{e\alpha} + (1 - \alpha)Q_{m\alpha}}$$

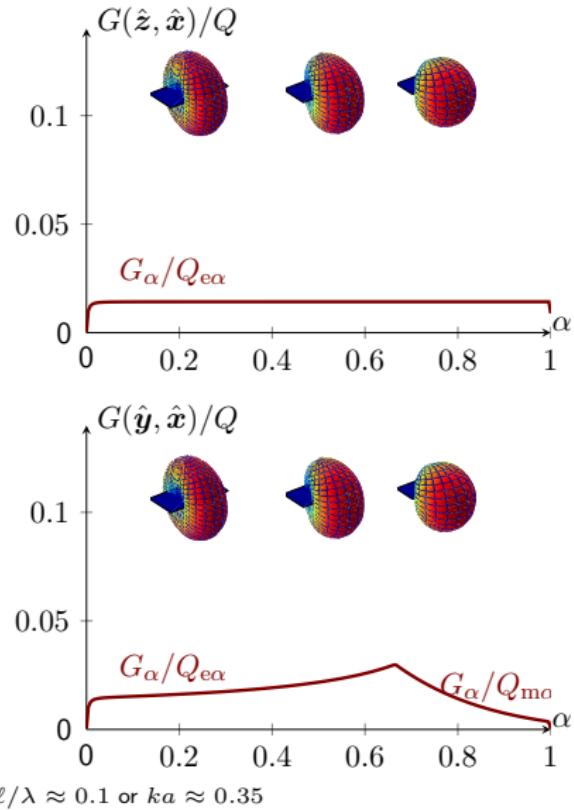
This is efficiently solved by golden section search and parabolic interpolation.



## Why convex optimization: illustration

We also compute the actual  $G/Q$  for the current  $\mathbf{I}_\alpha$  to get

$$\frac{G_\alpha}{\max\{Q_{e\alpha}, Q_{m\alpha}\}} \leq \left. \frac{G}{Q} \right|_{ub}$$



## Why convex optimization: illustration

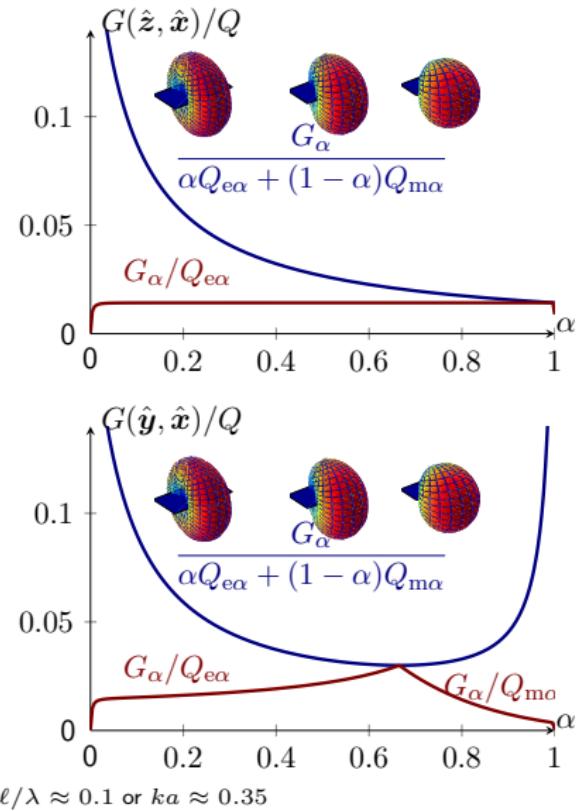
The upper bound on  $G/Q|_{\text{ub}}$  is obtained by solving the dual (relaxed) problem, i.e., finding the minimum of the (blue) curve

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This is efficiently solved by golden section search and parabolic interpolation.

We also compute the actual  $G/Q$  for the current  $\mathbf{I}_\alpha$  to get

$$\frac{G_\alpha}{\max\{Q_{e\alpha}, Q_{m\alpha}\}} \leq \frac{G}{Q} \Big|_{\text{ub}}$$



# Why: simple optimization formulations

## Super directivity:

$$\text{minimize} \quad \max\{\mathbf{I}^H \mathbf{X}_e \mathbf{I}, \mathbf{I}^H \mathbf{X}_m \mathbf{I}\}$$

$$\text{subject to} \quad \mathbf{F}^H \mathbf{I} = 1$$

$$\mathbf{I}^H \mathbf{R}_r \mathbf{I} \leq 4\pi / (\eta_0 D_0)$$

## Prescribed far field:

$$\text{minimize} \quad \max\{\mathbf{I}^H \mathbf{X}_e \mathbf{I}, \mathbf{I}^H \mathbf{X}_m \mathbf{I}\}$$

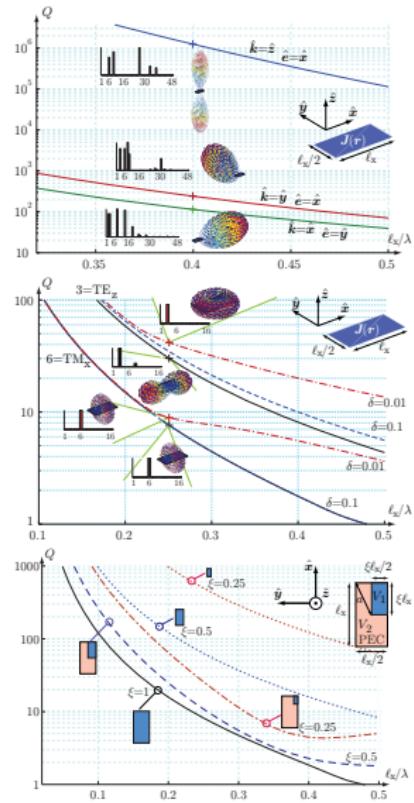
$$\text{subject to} \quad \int_{\Omega} |\mathbf{F}(\hat{\mathbf{k}}) - \mathbf{F}_0(\hat{\mathbf{k}})|^2 d\Omega_{\hat{\mathbf{k}}} < \delta$$

## Embedded antennas:

$$\text{minimize} \quad \max\{\mathbf{I}^H \mathbf{X}_e \mathbf{I}, \mathbf{I}^H \mathbf{X}_m \mathbf{I}\}$$

$$\text{subject to} \quad \mathbf{F}^H \mathbf{I} = 1$$

$$\mathbf{I}_2 = \mathbf{C} \mathbf{I}_1$$



# Summary

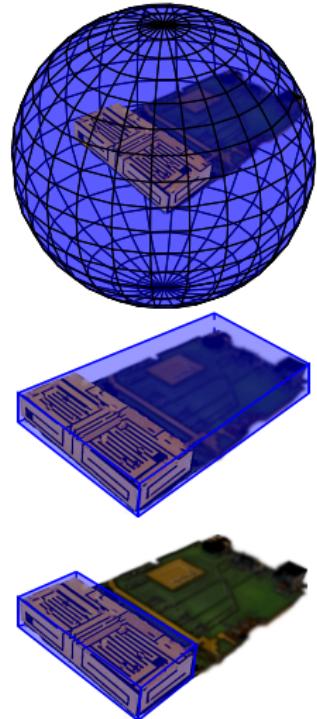
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- ▶ Stored energy expressed in the current density, fields, and input impedance.
- ▶ Can we define stored energy for a Herglotz function?
- ▶ Energy in complex media?
- ▶ Optimization of the antenna structure (global optimization) and the antenna currents (convex optimization).
- ▶ Convex optimization for bounds and optimal currents:  $G/Q$ , superdirective, embedded, ...
- ▶ Closed form solutions for small antennas.

Initial results for efficiency, more realistic geometries (phones), SAR, MIMO. Investigating dielectrics, volume currents, magnetic currents, ...

Slides at:

<http://www.eit.lth.se/staff/mats.gustafsson>



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See also: <http://www.eit.lth.se/staff/mats.gustafsson>

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