



Physical bounds on small antennas as convex optimization problems

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Design of small antennas

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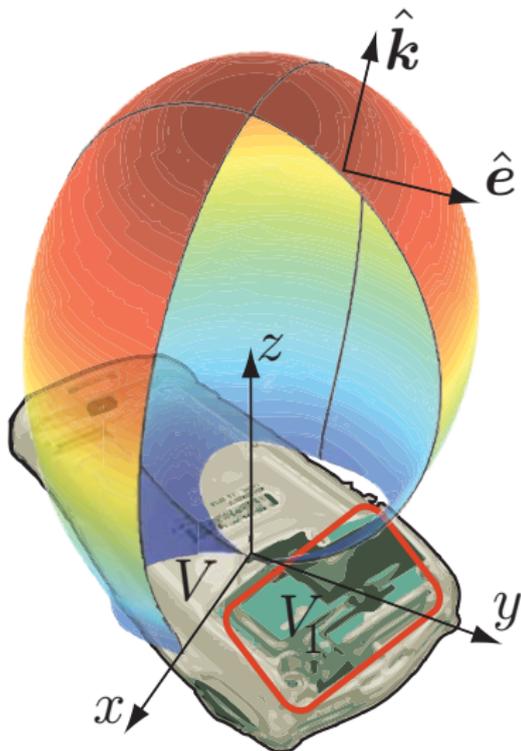
- ▶ There are many advanced methods to design small antennas.
- ▶ Performance often in bandwidth, matching, and efficiency.
- ▶ How can new designs, geometries, and materials improve performance?
- ▶ Here, what is the fundamental tradeoff between performance and size?

Tradeoff between performance and size

- ▶ Radiating (antenna) structure, V .
- ▶ Antenna volume, $V_1 \subset V$.
- ▶ Current density \mathbf{J}_1 in V_1 .
- ▶ Radiated field, $\mathbf{F}(\hat{\mathbf{k}})$, in direction $\hat{\mathbf{k}}$ and polarization $\hat{\mathbf{e}}$.

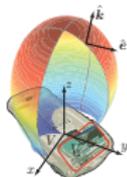
Questions analyzed here, \mathbf{J}_1 for:

- ▶ maximum $G(\hat{\mathbf{k}}, \hat{\mathbf{e}})/Q$.
- ▶ maximum $G(\hat{\mathbf{k}}, \hat{\mathbf{e}})/Q$ for $D(\hat{\mathbf{k}}, \hat{\mathbf{e}}) \geq D_0$ (superdirectivity).
- ▶ embedded antennas.
- ▶ also minimum Q for radiated field approximately $\mathbf{F}(\hat{\mathbf{k}})$ and effects of Ohmic losses.



Background

- ▶ 1947 Wheeler: *Bounds based on circuit models.*
- ▶ 1948 Chu: *Bounds on Q and D/Q for spheres.*
- ▶ 1964 Collin & Rothchild: *Closed form expressions of Q for arbitrary spherical modes, see also Harrington, Collin, Fantes, Maclean, Gayi, Hansen, Hujanen, Sten, Thiele, Best, Yaghjian, Kildal... (most are based on Chu's approach using spherical modes.)*
- ▶ 1999 Foltz & McLean, 2001 Sten, Koivisto, and Hujanen: *Attempts for bounds in spheroidal volumes.*
- ▶ 2006 Thal: *Bounds on Q for small hollow spherical antennas.*
- ▶ 2007 Gustafsson, Sohl & Kristensson: *Bounds on D/Q for arbitrary geometries (and Q for small antennas).*
- ▶ 2010 Yaghjian & Stuart: *Bounds on Q for dipole antennas in the limit $ka \rightarrow 0$.*
- ▶ 2011 Vandenbosch: *Bounds on Q for small (non-magnetic) antennas in the limit $ka \rightarrow 0$.*
- ▶ 2011 Chalas, Sertel & Volakis: *Bounds on Q using characteristic modes.*
- ▶ 2012 Gustafsson, Cismasu, & Jonsson: *Optimal charge and current distributions on antennas.*
- ▶ 2012 Bernland: *Physical Limitations on the Scattering of High Order Electromagnetic Vector Spherical Waves.*
- ▶ 2012 Gustafsson & Nordebo: *Optimal antenna Q , superdirectivity, and radiation patterns using convex optimization.*



G/Q and D/Q

Partial gain expressed in the partial radiation intensity $P(\hat{\mathbf{k}}, \hat{\mathbf{e}})$ and total radiated P_{rad} and dissipated power P_{loss}

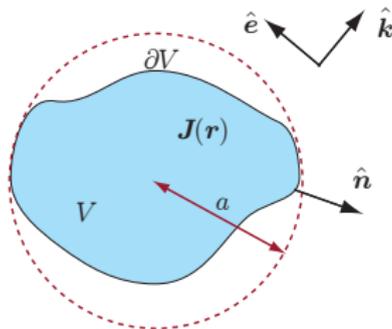
$$G(\hat{\mathbf{k}}, \hat{\mathbf{e}}) = 4\pi \frac{P(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{P_{\text{rad}} + P_{\text{loss}}}$$

Q-factor

$$Q = \frac{2\omega W}{P_{\text{rad}} + P_{\text{loss}}} = \frac{2c_0 k W}{P_{\text{rad}} + P_{\text{loss}}},$$

where $W = \max\{W_e, W_m\}$ denotes the maximum of the stored electric and magnetic energies. The G/Q and (D/Q for lossless) quotient cancels $P_{\text{rad}} + P_{\text{loss}}$

$$\frac{G(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{Q} = \frac{D(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{Q} = \frac{2\pi P(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{c_0 k W}.$$

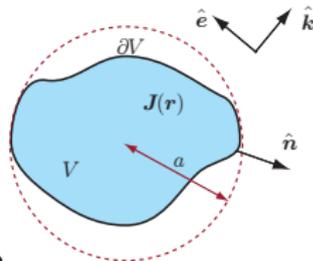


Stored EM energies from current densities \mathbf{J} in V

Use the expressions by Vandenbosch (2010) (and Geyi (2003) for small antennas).

Stored electric energy $\widetilde{W}_{\text{vac}}^{(e)} = \frac{\mu_0}{16\pi k^2} w^{(e)}$

$$w^{(e)} = \int_V \int_V \nabla_1 \cdot \mathbf{J}_1 \nabla_2 \cdot \mathbf{J}_2^* \frac{\cos(kR_{12})}{R_{12}} - \frac{k}{2} (k^2 \mathbf{J}_1 \cdot \mathbf{J}_2^* - \nabla_1 \cdot \mathbf{J}_1 \nabla_2 \cdot \mathbf{J}_2^*) \sin(kR_{12}) dV_1 dV_2,$$



where $\mathbf{J}_1 = \mathbf{J}(\mathbf{r}_1)$,

$\mathbf{J}_2 = \mathbf{J}(\mathbf{r}_2)$, $R_{12} = |\mathbf{r}_1 - \mathbf{r}_2|$. Stored

magnetic energy $\widetilde{W}_{\text{vac}}^{(m)} = \frac{\mu_0}{16\pi k^2} w^{(m)}$, where

$$w^{(m)} = \int_V \int_V k^2 \mathbf{J}_1 \cdot \mathbf{J}_2^* \frac{\cos(kR_{12})}{R_{12}} - \frac{k}{2} (k^2 \mathbf{J}_1 \cdot \mathbf{J}_2^* - \nabla_1 \cdot \mathbf{J}_1 \nabla_2 \cdot \mathbf{J}_2^*) \sin(kR_{12}) dV_1 dV_2.$$

Stored EM energies from current densities \mathbf{J} in V II

Also the total radiated power $P_{\text{rad}} = \frac{\eta_0}{8\pi k} p_{\text{rad}}$ with

$$p_{\text{rad}} = \int_V \int_V (k^2 \mathbf{J}_1 \cdot \mathbf{J}_2^* - \nabla_1 \cdot \mathbf{J}_1 \nabla_2 \cdot \mathbf{J}_2^*) \frac{\sin(kR_{12})}{R_{12}} dV_1 dV_2.$$

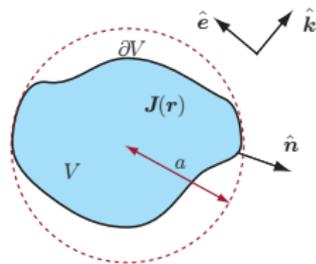
The normalized quantities $w^{(e)}$, $w^{(m)}$, and p_{rad} have dimensions given by volume, m^3 , times the dimension of $|\mathbf{J}|^2$.

- ▶ Introduced by Vandenbosch in *Reactive energies, impedance, and Q factor of radiating structures*, IEEE-TAP 2010.
- ▶ In the limit $ka \rightarrow 0$ by Geyi in *Physical limitations of antenna*, IEEE-TAP 2003.
- ▶ Validation for wire antennas in Hazdra *etal*, *Radiation Q-factors of thin-wire dipole arrangements*, IEEE-AWPL 2011.
- ▶ Some issues with 'negative stored energy' for large structures in Gustafsson *etal*, IEEE-TAP 2012.

G/Q in the current density \mathbf{J}

The partial radiation intensity $P(\hat{\mathbf{k}}, \hat{\mathbf{e}})$
in direction $\hat{\mathbf{k}}$ and for the polarization $\hat{\mathbf{e}}$ is

$$P(\hat{\mathbf{k}}, \hat{\mathbf{e}}) = \frac{\eta_0 k^2}{32\pi^2} \left| \int_V \hat{\mathbf{e}}^* \cdot \mathbf{J}(\mathbf{r}) e^{jk\hat{\mathbf{k}} \cdot \mathbf{r}} dV \right|^2$$



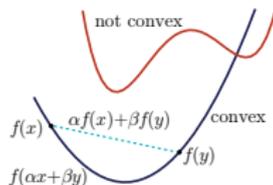
We have the G/Q quotient

$$\begin{aligned} \frac{G(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{Q} &= k^3 \frac{\left| \int_V \hat{\mathbf{e}}^* \cdot \mathbf{J}(\mathbf{r}) e^{jk\hat{\mathbf{k}} \cdot \mathbf{r}} dV \right|^2}{\max\{w^{(e)}(\mathbf{J}), w^{(m)}(\mathbf{J})\}} \\ &\leq \max_{\mathbf{J}} k^3 \frac{\left| \int_V \hat{\mathbf{e}}^* \cdot \mathbf{J}(\mathbf{r}) e^{jk\hat{\mathbf{k}} \cdot \mathbf{r}} dV \right|^2}{\max\{w^{(e)}(\mathbf{J}), w^{(m)}(\mathbf{J})\}} \end{aligned}$$

Solve the optimization problem. Closed form solutions in the limit $ka \rightarrow 0$ and convex optimization for larger (but small) structures.

Convex optimization

$$\begin{aligned} & \text{minimize} && f_0(\mathbf{x}) \\ & \text{subject to} && f_i(\mathbf{x}) \leq 0, \quad i = 1, \dots, N_1 \\ & && \mathbf{Ax} = \mathbf{b} \end{aligned}$$



where $f_i(x)$ are convex, i.e., $f_i(\alpha\mathbf{x} + \beta\mathbf{y}) \leq \alpha f_i(\mathbf{x}) + \beta f_i(\mathbf{y})$ for $\alpha, \beta \in \mathbb{R}$, $\alpha + \beta = 1$, $\alpha, \beta \geq 0$.

Solved with efficient standard algorithms. No risk of getting trapped in a local minimum. A problem is 'solved' if formulated as a convex optimization problem.

Can be used in many convex formulations for antenna performance expressed in the current density \mathbf{J} , e.g.,

- ▶ Radiated field $\mathbf{F}(\hat{\mathbf{k}}) = -\hat{\mathbf{k}} \times \hat{\mathbf{k}} \times \int_V \mathbf{J}(\mathbf{r}) e^{jk\hat{\mathbf{k}} \cdot \mathbf{r}} dV$ is affine.
- ▶ Radiated power, stored electric and magnetic energies, and Ohmic losses are positive semi-definite quadratic forms in \mathbf{J} .

Currents for maximal G/Q

Determine a current density $\mathbf{J}(\mathbf{r})$ in the volume V that maximizes the partial-gain Q-factor quotient $G(\hat{\mathbf{k}}, \hat{\mathbf{e}})/Q$.

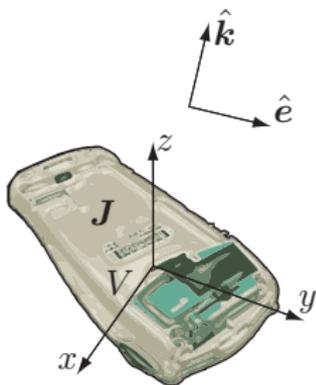
- ▶ Partial radiation intensity $P(\hat{\mathbf{k}}, \hat{\mathbf{e}})$

$$\frac{G(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{Q} = \frac{2\pi P(\hat{\mathbf{k}}, \hat{\mathbf{e}})}{c_0 k \max\{W_e, W_m\}}.$$

- ▶ Scale \mathbf{J} and reformulate $P = 1$ as $\text{Re}\{\hat{\mathbf{e}}^* \cdot \mathbf{F}\} = 1$.
- ▶ Convex optimization problem.

$$\text{minimize} \quad \max\{\mathbf{J}^H \mathbf{W}_e \mathbf{J}, \mathbf{J}^H \mathbf{W}_m \mathbf{J}\}$$

$$\text{subject to} \quad \text{Re}\{\mathbf{F}^H \mathbf{J}\} = 1$$



Determines a current density $\mathbf{J}(\mathbf{r})$ in the volume V with minimal stored EM energy and unit partial radiation intensity in $\{\hat{\mathbf{k}}, \hat{\mathbf{e}}\}$.

Maximal $G(\hat{\mathbf{k}}, \hat{\mathbf{x}})/Q$ for planar rectangles

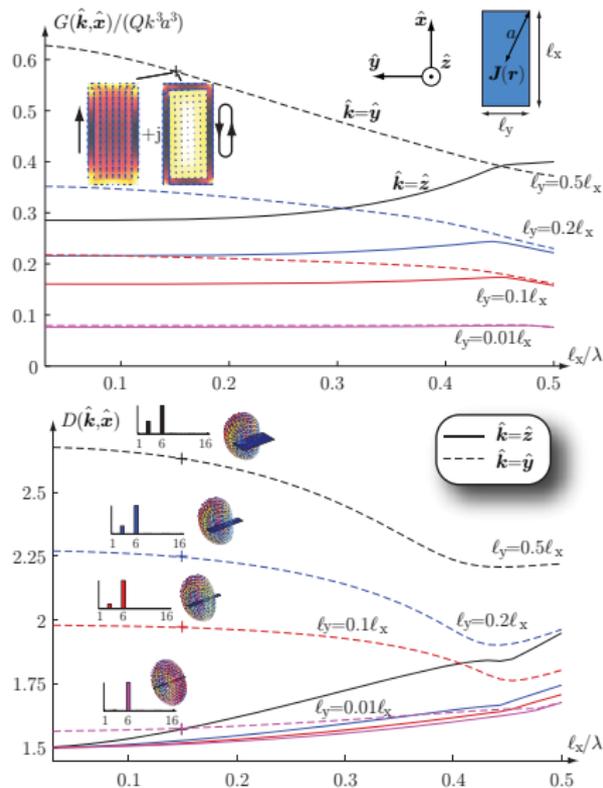
Solution of the convex optimization problem

$$\min. \quad \max\{\mathbf{J}^H \mathbf{W}_e \mathbf{J}, \mathbf{J}^H \mathbf{W}_m \mathbf{J}\}$$

$$\text{s.t.} \quad \text{Re}\{\mathbf{F}^H \mathbf{J}\} = 1$$

for current densities confined to planar rectangles with side lengths ℓ_x and $\ell_y = \{0.01, 0.1, 0.2, 0.5\}\ell_x$.

Note $\ell_x/\lambda = k\ell_x/(2\pi)$, giving $\ell_x = \lambda/2 \rightarrow k\ell_x = \pi \rightarrow ka \geq \pi/2$.



D/Q (or G/Q) bounds

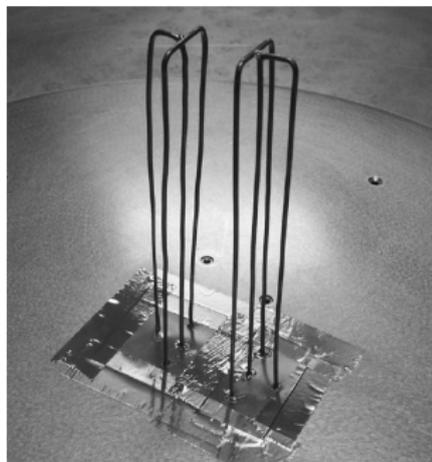
- ▶ Similar to the forward scattering bounds for TM.
- ▶ Can design 'optimal' electric dipole mode (TM) antennas.
- ▶ TE modes and TE+TM are not well understood.
- ▶ Typical matlab code using CVX

```
cvx_begin
    variable J(n) complex;
    dual variables We Wm
    maximize(real(F'*J))
    We: quad_form(J,Ze) <= 1;
    Wm: quad_form(J,Zm) <= 1;
cvx_end
```

We now reformulate the complex optimization problem to analyze superdirectivity, antennas with a prescribed radiation pattern, losses, and antennas embedded in a PEC structure.

Superdirectivity

- ▶ A superdirective antenna has a directivity that is much larger than for a typical reference antenna.
- ▶ Often low efficiency (low gain) and narrow bandwidth.
- ▶ There is an interest in small superdirective antennas, e.g., Best *etal.* 2008 and Arceo & Balanis 2011,



Best, *etal.*, An Impedance-Matched 2-Element Superdirective Array, IEEE-TAP, 2008

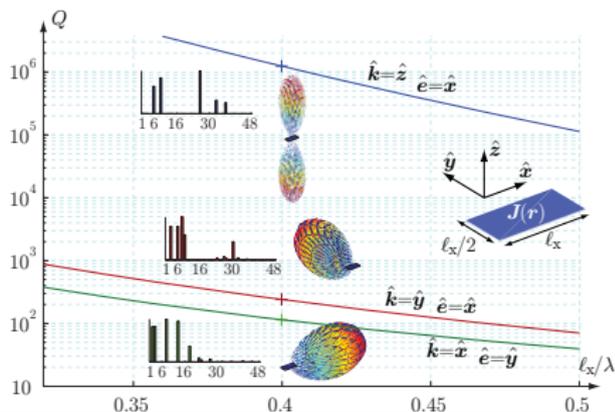
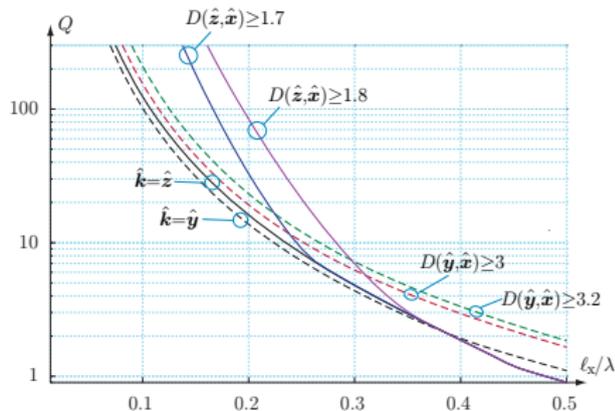
Here, we add the constraint $D \geq D_0$ to the convex optimization problem for G/Q to determine the minimum Q for superdirective lossless antennas. We can also add constraints on the losses.

Superdirectivity

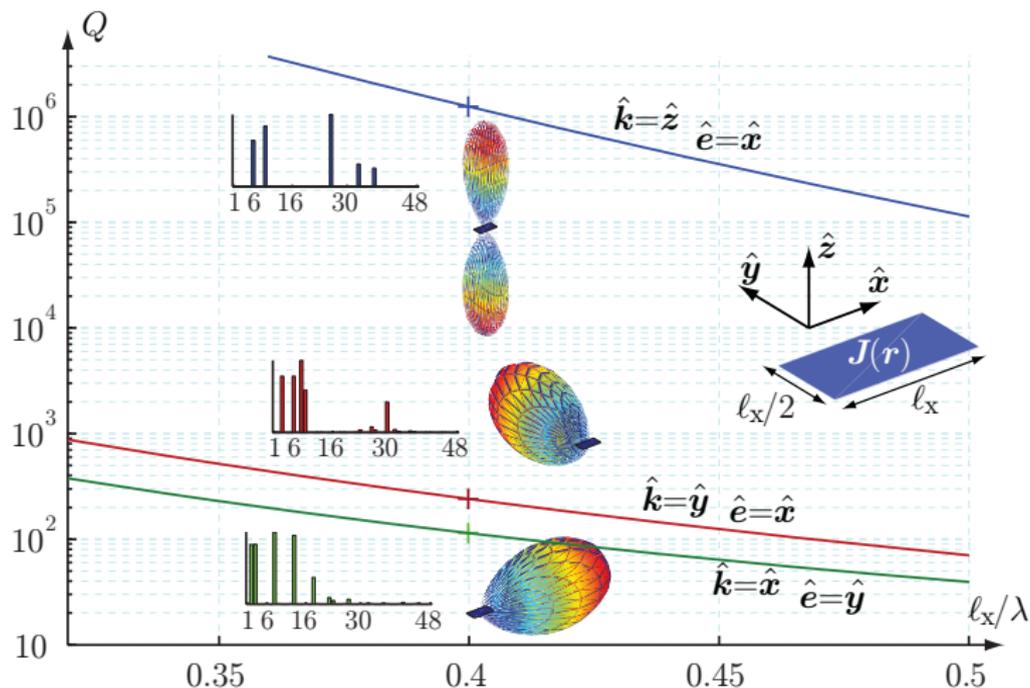
Add the constraint
 $P_{\text{rad}} \leq 4\pi D_0^{-1}$ then get the
 convex optimization problem

$$\begin{aligned} \min. \quad & \max\{\mathbf{J}^H \mathbf{W}_e \mathbf{J}, \mathbf{J}^H \mathbf{W}_m \mathbf{J}\} \\ \text{s.t.} \quad & \text{Re}\{\mathbf{F}^H \mathbf{J}\} = 1 \\ & \mathbf{J}^H \mathbf{P} \mathbf{J} \leq k^3 D_0^{-1} \end{aligned}$$

Example for current densities
 confined to planar rectangles
 with side lengths ℓ_x and
 $\ell_y = 0.5\ell_x$.



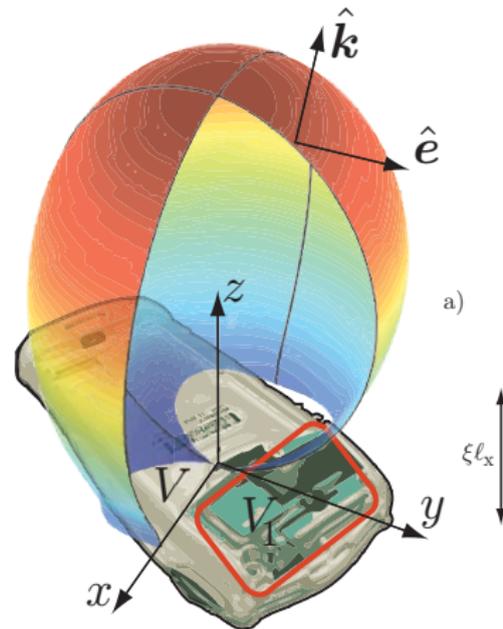
Superdirectivity with $D \geq D_0 = 10$



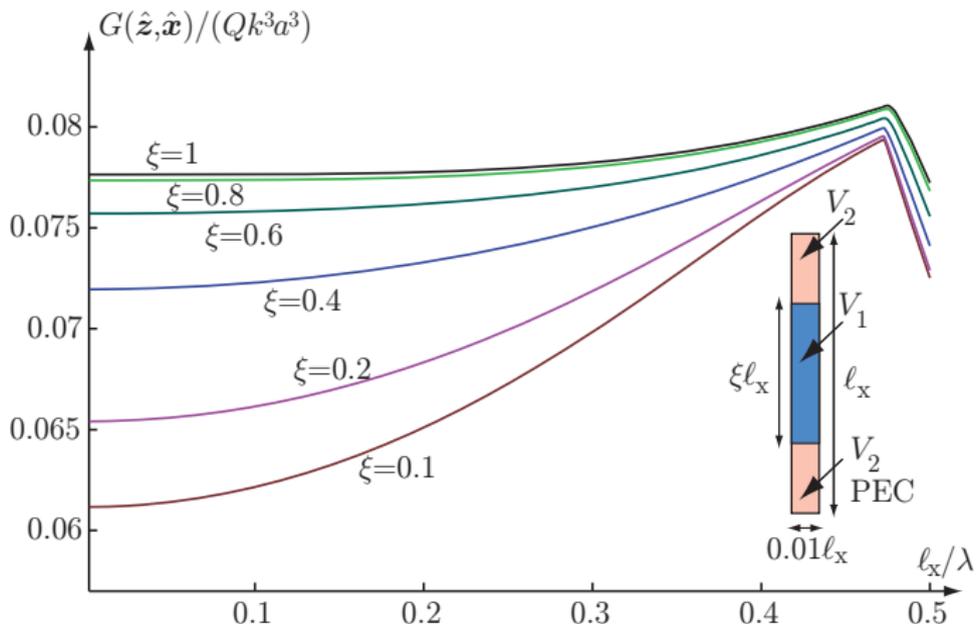
Note, it gives a bound on Q as D is known.

Optimal performance for embedded antennas

- ▶ It is common with antennas embedded in metallic structures.
- ▶ The induced currents radiate but they are not arbitrary.
- ▶ Linear map from the antenna region adds a (convex) constraint.
- ▶ Here, we assume that the surrounding structure is PEC and add a constraint to account for the induced currents on the surrounding structure in the G/Q formulation.

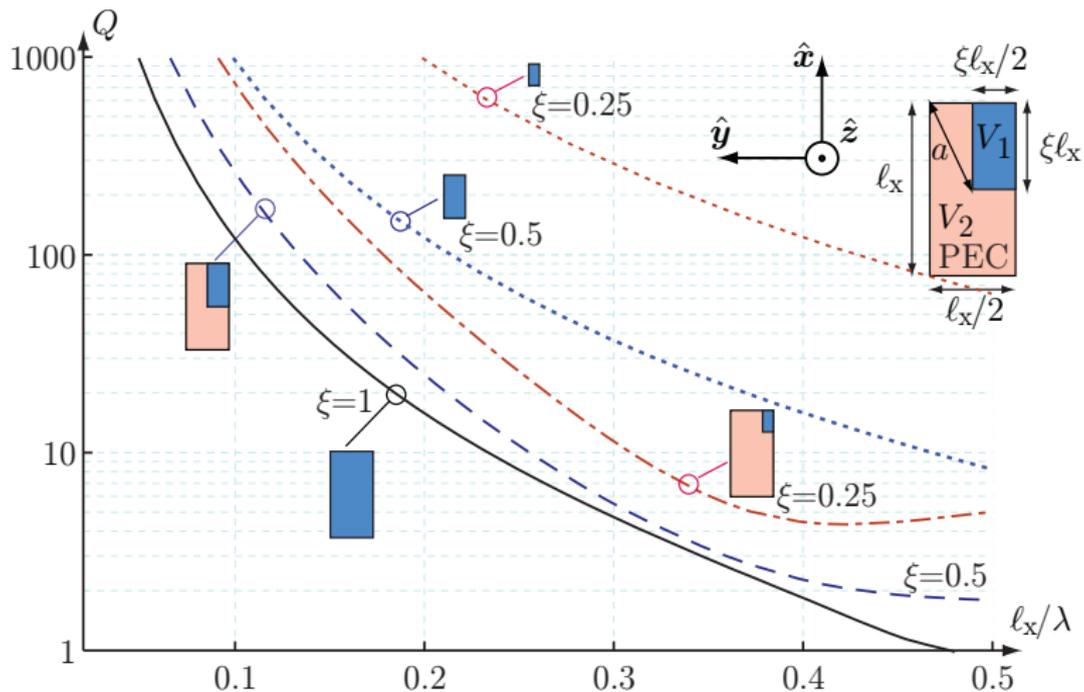


Center fed strip dipole



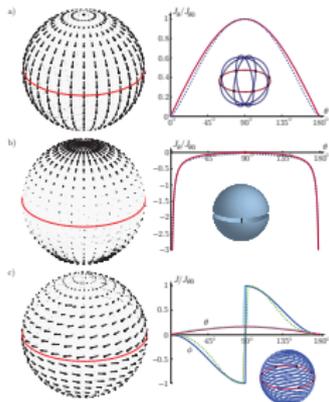
Almost independent of the feed width at the resonance just below $l_x = 0.5\lambda$.

Embedded antennas in a planar rectangle



Conclusions

- ▶ Closed form solution for small antennas.
 - ▶ Optimal current distributions. Spherical dipole, capped dipole, and folded spherical helix. More in IF46, *Small Antennas: Designs and Applications* on Thursday.
- ▶ Convex optimization to determine bounds and optimal currents for larger structures:
 - ▶ D/Q and G/Q .
 - ▶ Q for superdirective antennas.
 - ▶ Embedded antennas in PEC structures.
 - ▶ Q for antennas with prescribed far fields.



See also *Physical bounds and optimal currents on antennas* IEEE TAP, 60, 6, pp. 2672-2681, 2012 and *Antenna currents for optimal Q , superdirectivity, and radiation patterns using convex optimization* (www.eit.lth.se/staff/mats.gustafsson)

