

1/

a
$$E_0 = E_1 = \int_0^{T_s/2} s_i^2(t) dt = \underline{\underline{s_1^2 + s_2^2}}$$

b
$$z_0(t) = s_0(t) * h(t)$$

$$z_1(t) = s_1(t) * h(t) = -z_0(t)$$

$$z_0(t) = s_1 h_1 y_{11}(t) + s_1 h_2 y_{12}(t) + s_1 h_3 y_{13}(t) \\ + s_2 h_1 y_{21}(t) + s_2 h_2 y_{22}(t) + s_2 h_3 y_{23}(t)$$

where

$$y_{mn}(t) = \phi_m(t) * \phi_n(t)$$

$$y_{mn}(t) \neq 0 \quad \text{for} \quad 0 \leq t \leq T_s \quad (\text{in general})$$

Orthogonality knowledge not usable

$$E_{z_0} = \int_0^{T_s} z_0^2(t) dt = s_1^2 h_1^2 E_{1111} + 2s_1^2 h_1 h_2 E_{1112} + 2s_1^2 h_1 h_3 E_{1113}$$

$$+ 2s_1 s_2 h_1^2 E_{1121} + 2s_1 s_2 h_1 h_2 E_{1122} + 2s_1 s_2 h_1 h_3 E_{1123}$$

$$+ s_1^2 h_2^2 E_{1212} + 2s_1^2 h_2 h_3 E_{1213} + 2s_1 s_2 h_2 h_1 E_{1221}$$

$$+ 2s_1 s_2 h_2^2 E_{1222} + 2s_1 s_2 h_2 h_3 E_{1223}$$

$$+ s_1^2 h_3^2 E_{1313} + 2s_1 s_2 h_3 h_1 E_{1321} + 2s_1 s_2 h_3 h_2 E_{1322}$$

$$+ 2s_1 s_2 h_3^2 E_{1323} + s_2^2 h_1^2 E_{2121} + 2s_2^2 h_1 h_2 E_{2122} + 2s_2^2 h_1 h_3 E_{2123}$$

$$+ s_2^2 h_2^2 E_{2222} + 2s_2^2 h_2 h_3 E_{2223} + s_2^2 h_3^2 E_{2323}$$

where
$$E_{mnlk} = \int_0^{T_s} y_{mn}(t) y_{lk}(t) dt \quad (\text{which are unknown})$$

b cont.

collect terms:

$$E_{z_0} = s_1^2 \left[h_1^2 E_{1111} + 2h_1 h_2 E_{1112} + 2h_1 h_3 E_{1113} + 2h_2^2 E_{2212} + 2h_2 h_3 E_{2213} + h_3^2 E_{3313} \right]$$

$$+ s_2^2 \left[h_1^2 E_{2121} + 2h_1 h_2 E_{2122} + 2h_1 h_3 E_{2123} + h_2^2 E_{2222} + 2h_2 h_3 E_{2223} + h_3^2 E_{2323} \right]$$

$$+ s_1 s_2 \left[2h_1^2 E_{1121} + 2h_1 h_2 E_{1122} + 2h_1 h_3 E_{1123} + 2h_2 h_1 E_{1221} + 2h_2^2 E_{1222} + 2h_2 h_3 E_{1223} + 2h_3 h_1 E_{1321} + 2h_3 h_2 E_{1322} + 2h_3^2 E_{1323} \right]$$

$$= s_1^2 A_{11} + s_2^2 A_{22} + 2s_1 s_2 A_{12} \quad \text{with } A_{11} \ A_{22} \ A_{12} \text{ defined from above}$$

Thus, $\underline{E_{b,r} = s_1^2 A_{11} + s_2^2 A_{22} + 2s_1 s_2 A_{12}}$

c/ received signal $z_0(t) = z(t)$

$$z_1(t) = -z(t)$$

antipodal

$$r(t) \rightarrow \left[\int_0^{T_b} r(t) z(t) dt \right] \rightarrow \boxed{z_0}$$

d/ P_b for antipodal signaling: $Q\left(\sqrt{2 \frac{E_{b,r}}{N_0}}\right)$

$$\rightarrow P_b = Q\left(\sqrt{2 \frac{s_1^2 A_{11} + s_2^2 A_{22} + 2s_1 s_2 A_{12}}{N_0}}\right)$$

e/ $P_b = Q\left(\sqrt{2 \frac{E_{b,r}}{N_0}}\right)$ Antipodal signaling with received $E_{b,r}$

g/ optimize $E_{b,r}$

$$E_{b,r} = E \rightarrow s_1^2 + s_2^2 = E$$

Method 1 (direct): $s_2 = \pm \sqrt{E - s_1^2}$

$$\frac{\partial}{\partial s_1} s_1^2 A_{11} + (E - s_1^2) A_{22} \pm 2s_1 \sqrt{E - s_1^2} A_{12} = 0$$

+ if $A_{12} > 0$

- if $A_{12} < 0$

Method 2 $s_1 = \cos(x) \sqrt{E}$

$$s_2 = \sin(x) \sqrt{E}$$

$$f(x) = A_{11} E \cos^2(x) + A_{22} E \sin^2(x) + 2A_{12} E \sin(x) \cos(x)$$

$$\frac{\partial}{\partial x} f(x) = -2A_{11} E \cos(x) \sin(x) + 2A_{22} E \cos(x) \sin(x) + 2A_{12} E \cos(2x) = 0$$

$$\sin(2x) [A_{22} - A_{11}] + 2A_{12} \cos(2x) = 0$$

$$\sqrt{[A_{22} - A_{11}]^2 + 4A_{12}^2} \sin(2x + \varphi) \quad \varphi = \tan^{-1} \left(\frac{A_{22} - A_{11}}{2A_{12}} \right)$$

$$2x + \varphi = 0 \rightarrow$$

$$x = -\frac{1}{2} \tan^{-1} \left(\frac{A_{22} - A_{11}}{2A_{12}} \right)$$

2

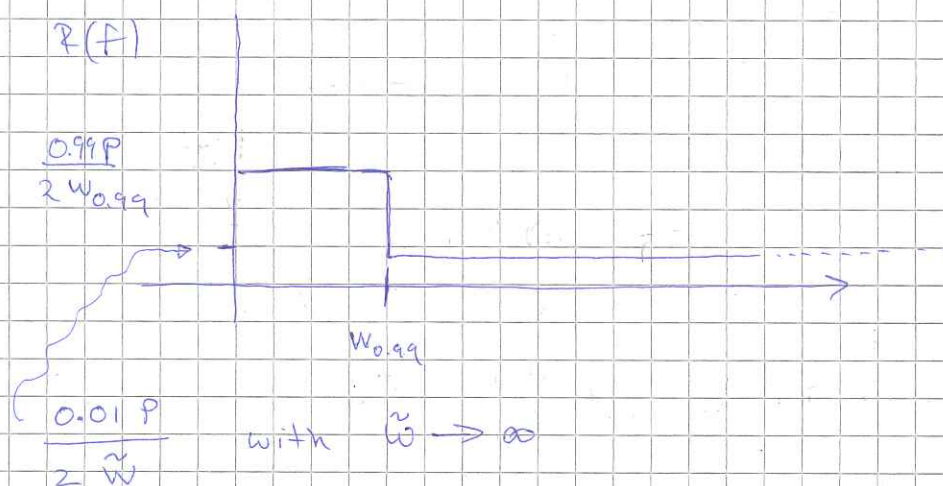
a) $W \log_2 \left(1 + \frac{P}{N_0 W} \right)$

b) Power inside $W_{0.99} = 0.99P \rightarrow$

$$C = W_{0.99} \log_2 \left(1 + \frac{0.99P}{N_0 W_{0.99}} \right)$$

c) ONLY constraint: $0.99P$ inside $W_{0.99}$

$\rightarrow$ unlimited bandwidth $\rightarrow$



d) $C_{\text{inside}} = W_{0.99} \log_2 \left(1 + \frac{0.99P}{N_0 W_{0.99}} \right)$

$$C_{\text{outside}} = \lim_{\tilde{W} \rightarrow \infty} \tilde{W} \log_2 \left(1 + \frac{0.01P}{N_0 \tilde{W}} \right) = \frac{0.01P}{N_0 \ln(2)}$$

$$C = W_{0.99} \log_2 \left(1 + \frac{0.99P}{N_0 W_{0.99}} \right) + \frac{0.01P}{N_0 \ln(2)}$$

(eq. 5.63)



Set $W_{0.99} = 1$ Hz (More rigorously: plot $C/W_{0.99}$)

against ~~E_b/N_0~~

$\frac{P}{N_0}$ dB	C
0	1
10	3.6
15	5.47
20	8.09
25	12.86

Shown with •

f/

$\frac{P}{N_0}$ dB	C
0	1
10	3.46
15	5.03
20	6.66
25	8.31

99% BW makes sense up to about 15-20 dB $\frac{P}{N_0}$

Shown with x

g/ by repeating for other ϵ , we can see a large gap around $\frac{P}{N_0} \approx \frac{1}{1-\epsilon}$
(linear scale)

3)

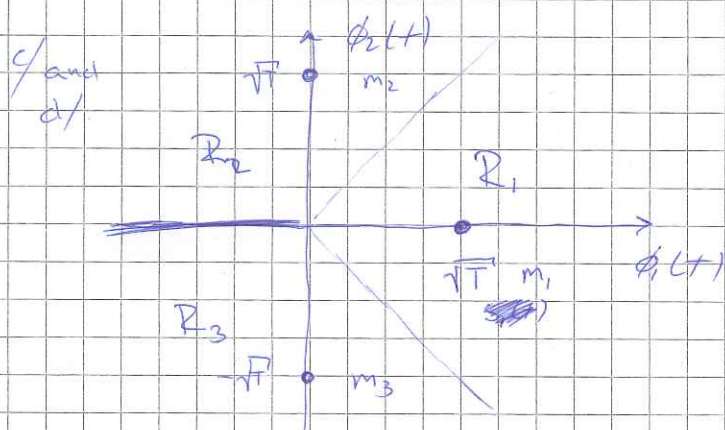
a) 2 since $\int_0^T s_1(t) s_2(t) dt = 0$

$s_1(t)$ and $s_2(t)$ clearly live in the same dimension

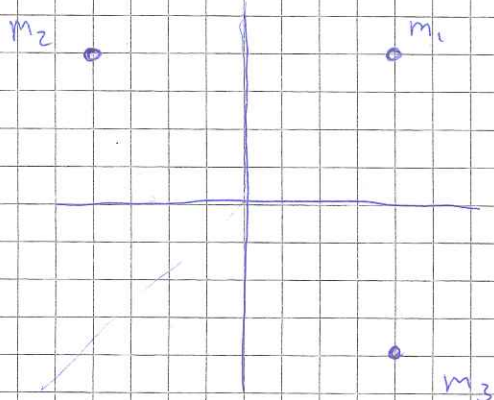
b) since $\int_0^T s_1(t) s_2(t) dt = 0 \rightarrow$

$$\phi_1(t) = \frac{s_1(t)}{\sqrt{E_1}} \quad \phi_2(t) = \frac{s_2(t)}{\sqrt{E_2}}$$

$$E_1 = E_2 = T$$



e/ rotate signal space 45°



$$P(\text{error} | m_2) = P(\text{error} | m_3) = 1 - \iint_{(n_1, n_2) \in S} p(n_1, n_2) dn_1 dn_2$$

$$P(\text{error} | m_1) = 1 - \iint_{\tilde{S}} p(n_1, n_2) dn_1 dn_2 \quad \tilde{S} \subset S \rightarrow P(\text{error} | m_1) > P(\text{error} | m_2)$$

f/

$$\text{Let } E_y = \int_0^T s_y^2(t) dt$$

$$\text{Let } a_1 = \int_0^T s_y(t) \phi_1(t) dt$$

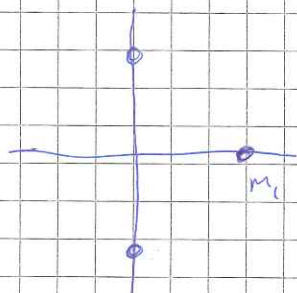
$$a_2 = \int_0^T s_y(t) \phi_2(t) dt$$

if $a_1^2 + a_2^2 = E \rightarrow s_y(t)$ is in the same space

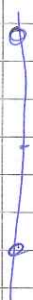
g/

exactly the same situation as the original problem:

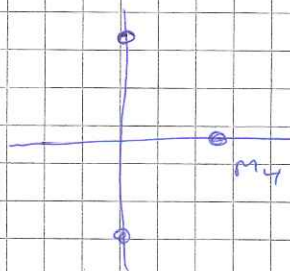
original



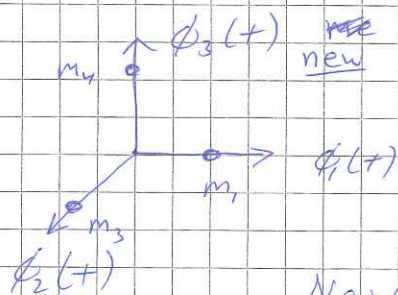
original
remove s_1



add $s_y(t)$



h/



New situation! eq. to 3-FSK

all signals orthogonal, $P(\text{error} | m_i)$ equal for all i

④

a)

$$P_b \text{ for Rayleigh fading} \approx \frac{1}{2d^2 \frac{E_b}{N_0}} \quad (\text{eq. 9.46})$$

$$d^2 \text{ for M-PAM: } \frac{6 \log_2(M)}{M^2 - 1}$$

$$P = R_b E_b \rightarrow$$

$$P_b \approx \frac{(M^2 - 1) R_b \cdot N_0}{12 \log_2(M) \cdot P} = \frac{(M^2 - 1)}{12 \log_2(M)} \frac{1}{P} = 10^{-5}$$

$$\rightarrow P = 10^{-5} \cdot \frac{(M^2 - 1)}{12 \log_2(M)}$$

function decays with $M \rightarrow$ choose M as small as possible.

But slow fading, freq-nonselective $\rightarrow$

$$R_s \gg \frac{1}{t_{coh}} \quad \text{and} \quad R_s \ll \frac{1}{2T_m} \quad (\text{eq. 9.32 with } k_w=2)$$

$$R_s \gg 2000$$

$$R_s \ll 10000$$

$$\rightarrow 2000 \ll R_s \ll 10000$$

R_s as a function of M ?

$$R_s = \frac{R_b}{\log_2(M)} \quad M=2 \text{ does not work}$$

$\rightarrow$ choose $M=4$

M	R_s	OK?
2	10000	X
4	5000	✓
8	3333	✓?
16	2500	✓??
32	2000	X

b/ Bandwidth = $2R_s$

Spectral broadening = $B_p = \frac{1}{T_{\text{coh}}} = 2000 \text{ Hz}$

total need $2R_s + 2000$

$R_s = \frac{R_b}{\log_2(M)} \rightarrow$

$$BW = \frac{20000}{\log_2(M)} + 2000$$

d/ $P_b = \frac{1}{2P(R) \frac{\log_2(M)}{M^2-1} \frac{E_b}{N_0}}$

$P = E_b R_b$ even with coding

$$\rightarrow P = 10^{-5} \frac{(M^2-1)}{2P(R) \log_2(M)}$$

$R_s = \frac{R_b}{R \log_2(M)}$

$2000 \leq R_s \leq 10000$

M Range of R to satisfy

2 $1 \leq R \leq 5$ ~~Not possible~~ Not possible

4 $\frac{1}{2} \leq R \leq 2.5$

8 $\frac{1}{3} \leq R \leq 1.67$

16 $\frac{1}{4} \leq R \leq 1.25$

32 $\frac{1}{8} \leq R \leq 1$

etc

wide range of possibilities.

optimal choice depends on $P(R)$

if $P(\frac{1}{3}) \gg P(\frac{1}{2})$ $M=8$ may be better than $M=4$

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a) since $T_{\text{obs}f_A} = 1$

$$p = \frac{\log_2(M)}{\frac{N_{\text{FFT}} + N_{\text{CP}}}{N_{\text{FFT}}}}$$