

F11 – Feedback and Stability

Outline

- General feedback structure and systematic analysis
- Feedback topologies
 - Feedback voltage amplifier (series-shunt)
 - Feedback transconductance amplifier (series-series)
 - Feedback transresistance amplifier (shunt-shunt)
 - Feedback current amplifier (shunt-series)
- Stability considerations and Nyquist plot
- Effects of feedback on pole location
- Stability analysis using Bode plots, gain and phase margin
- Frequency compensation (pole splitting)

Reading Guide

Sedra/Smith 7ed int

- Chapter 10.1-4, 10.6 (voltage feedback)
- (Chapter 10.5 (other feedback))
- Chapter 10.7-9 (amplifier stability)
- (Chapter 10.10 (freq. compensation))

Problems

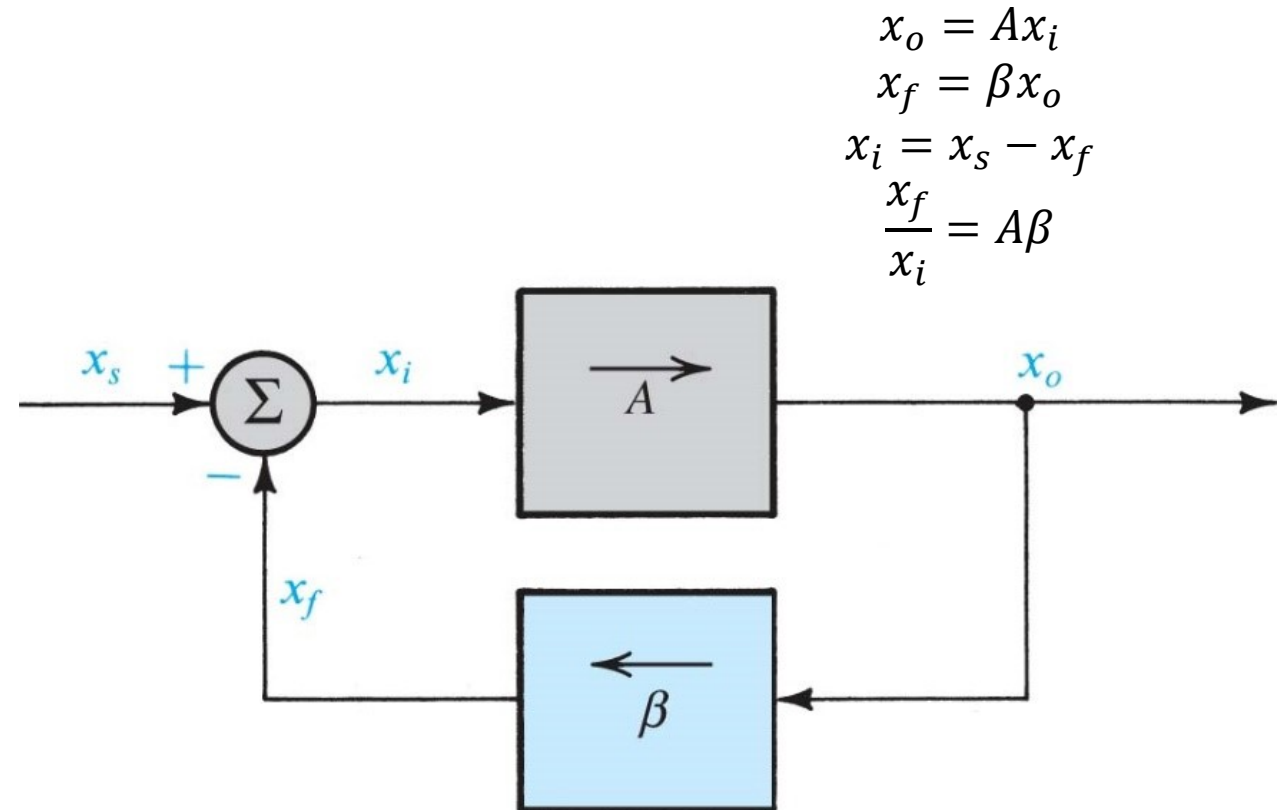
Sedra/Smith 7ed int

- P10.7, 10.8, 10.17, 10.28, 10.30

General Negative Feedback Structure



- Open loop gain, A
- Feedback factor (feedback transfer function), β
- Loop gain (loop transfer function), $A\beta$
 - Signal gain from x_i to x_f
 - Always dimensionless
- Amount of feedback, $1 + A\beta$
- Gain with feedback (closed loop transfer function), $A_f = \frac{x_o}{x_s} = \frac{A}{1+A\beta}$



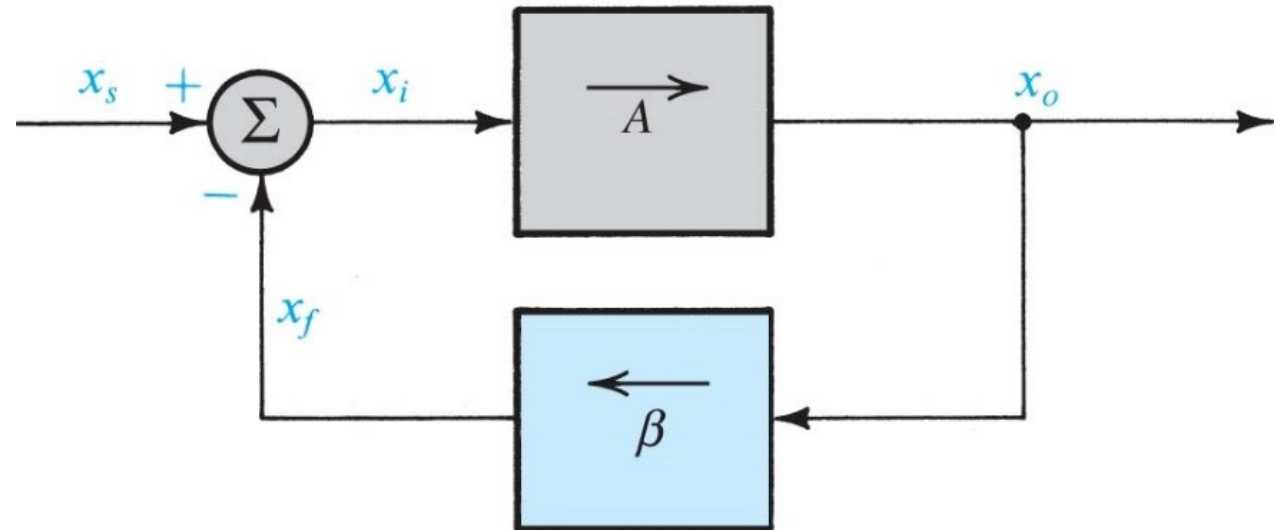
Transfer function is a more general term, non-scalar, for signal gain or factor.

Benefits of Feedback

- Gain with feedback is reduced by the amount of feedback, $1 + A\beta$

$$A_f = \frac{A}{1 + A\beta}$$

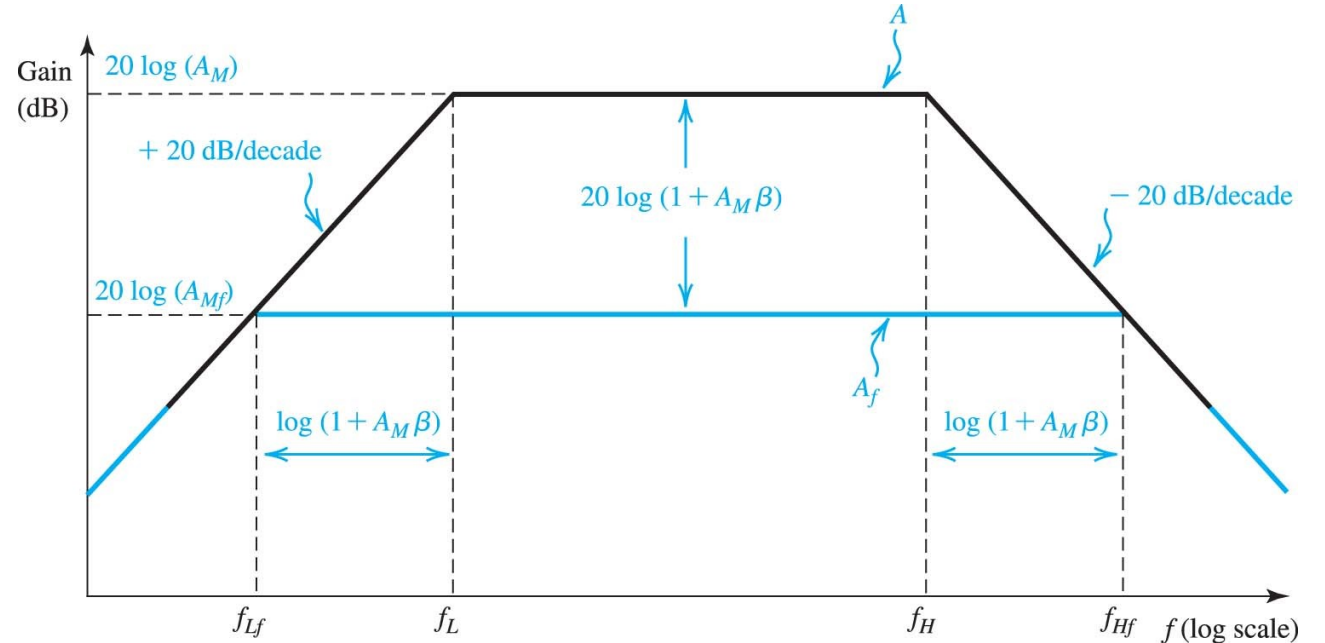
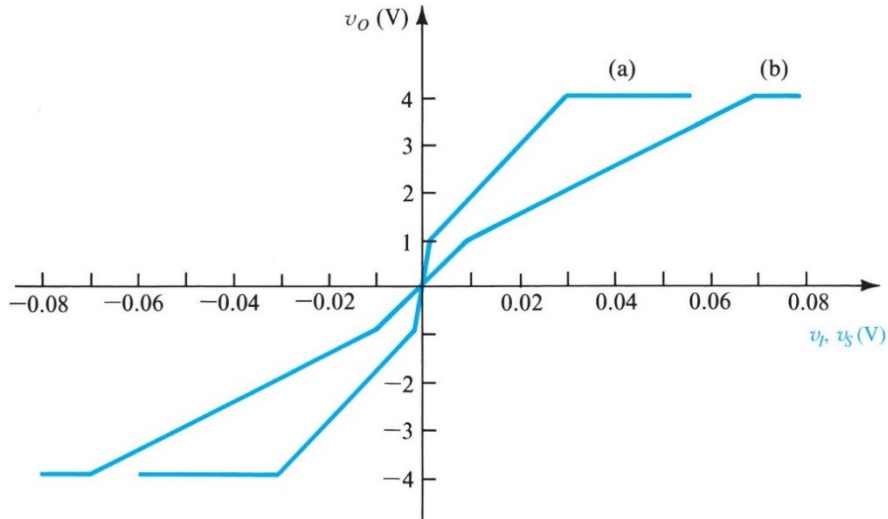
- The amount of feedback also quantifies...
 - Gain desensitivity
 - Bandwidth extension
 - Reduction of nonlinear distortion
 - Input resistance idealisation (increase/ decrease)
 - Output resistance idealisation (increase/ decrease)
 - Interference reduction



Feedback improvements come at the cost of gain, and at the risk of instability.

Benefits of Feedback

- Gain desensitivity
- Bandwidth extension
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- Input resistance idealisation (increase/ decrease)
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$$f_{Lf} = \frac{f_L}{1 + A_M\beta}$$

$$A_{Mf} = \frac{A_M}{1 + A_M\beta}$$

$$f_{Hf} = f_H(1 + A_M\beta)$$

$$A_f = \frac{A}{1 + A\beta}$$

Feedback improvements come at the cost of gain, and at the risk of instability.



Ideal Feedback Analysis

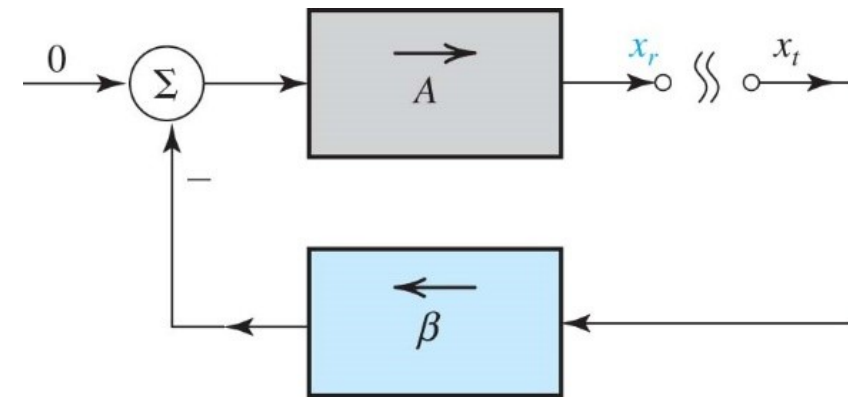
- Quantification method
 - Cancel source, break loop, inject test signal, and measure return
- Sign of the loop gain
 - Negative feedback: $A\beta > 0$
 - Positive feedback: $A\beta < 0$ (reduced stability)

$$\begin{aligned}x_s &= 0 \\x_r &= -A\beta x_t \\A\beta &= \frac{-x_r}{x_t}\end{aligned}$$

- Magnitude of the loop gain, $|A\beta|$
 - Determines amount of feedback, $(1 + A\beta)$, and ideality of closed loop gain

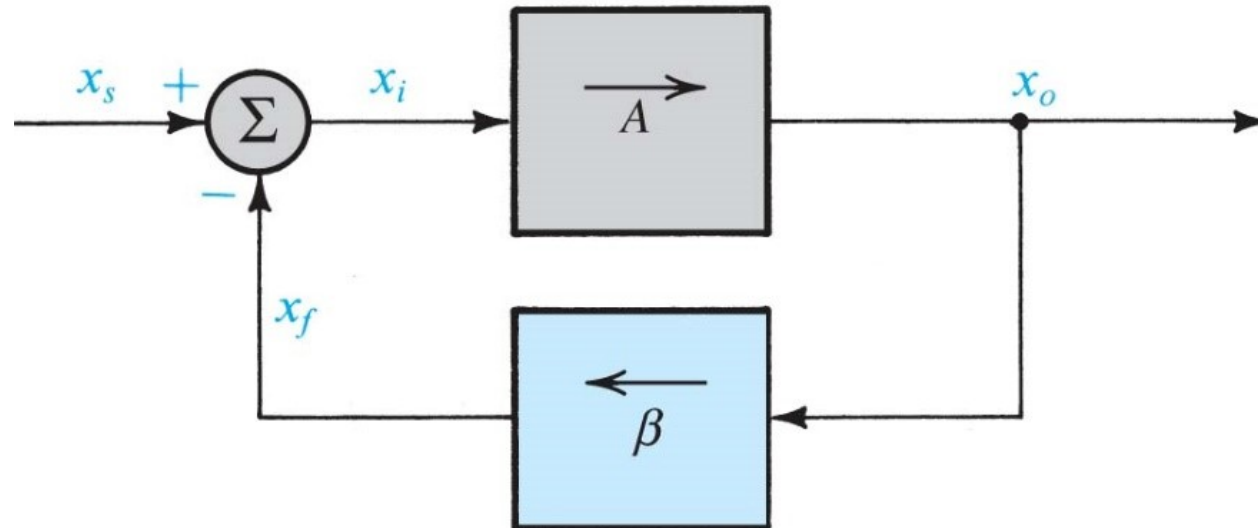
$$A_f = \frac{A}{1 + A\beta}, \quad A_f \Big|_{A\beta \gg 1} \approx \frac{1}{\beta}$$

- Amount of feedback quantifies the benefits of feedback



Feedback loop does not load amplifier, no internal feedback, and unilateral blocks.

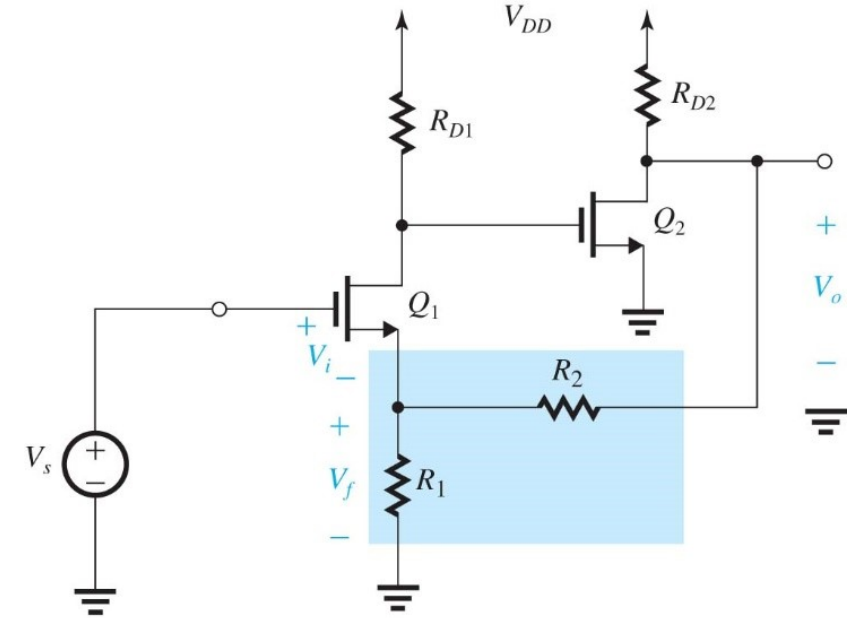
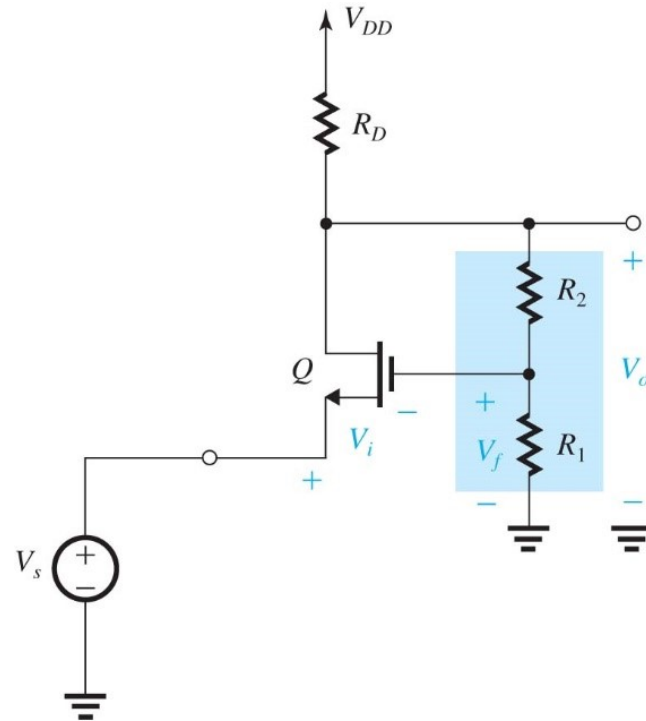
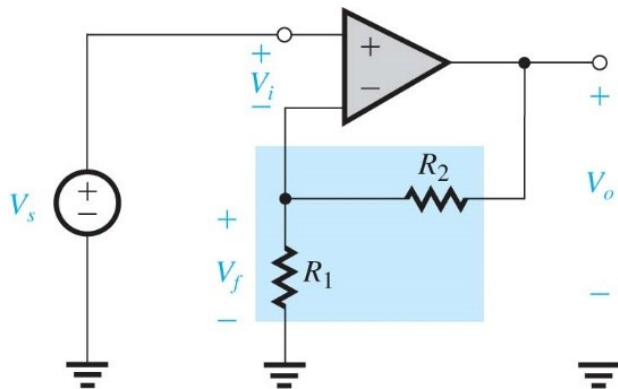
Where did we already encounter feedback?



Think, think, think.

Examples of Series-Shunt (Voltage) Feedback Amplifiers

- Amplifier circuit
 - Some kind of circuit with gain, preferably voltage amplifier
- Voltage feedback network
 - Series voltage mixing on input
 - Shunt voltage sampling over output



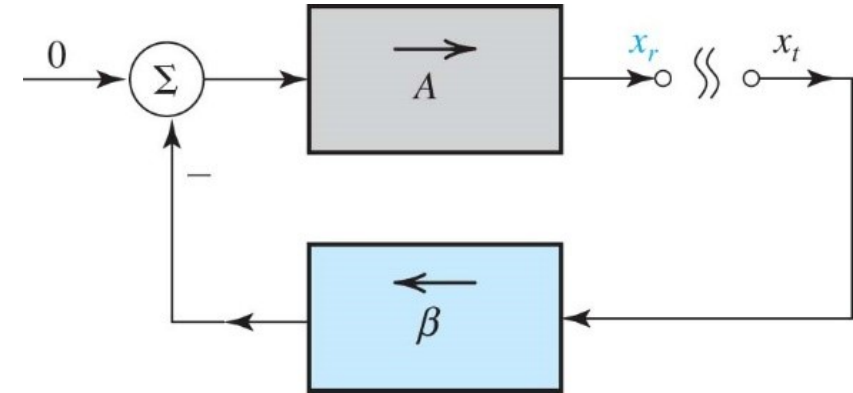
The feedback network is treated as an add-on to the amplifier.



Loop (Voltage) Gain Analysis

- Identify feedback network
 - Determine feedback factor, β
 - Determine ideal gain with feedback (closed loop gain)

$$A_f = \frac{A}{1 + A\beta} \approx \frac{1}{\beta}$$

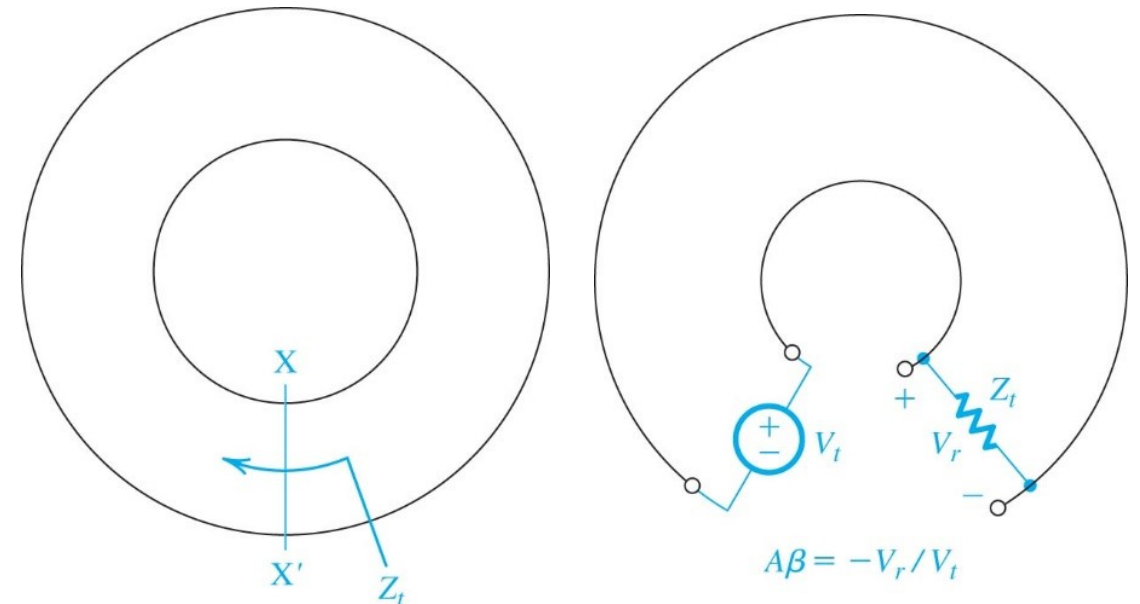


- Determine loop gain
 - Cancel source signal
 - Break loop (ideally at infinite impedance)
 - Terminate return path (as required)
 - Apply a test voltage to the feedback loop
 - Measure the returned termination voltage

$$A\beta = -\frac{V_r}{V_t}$$

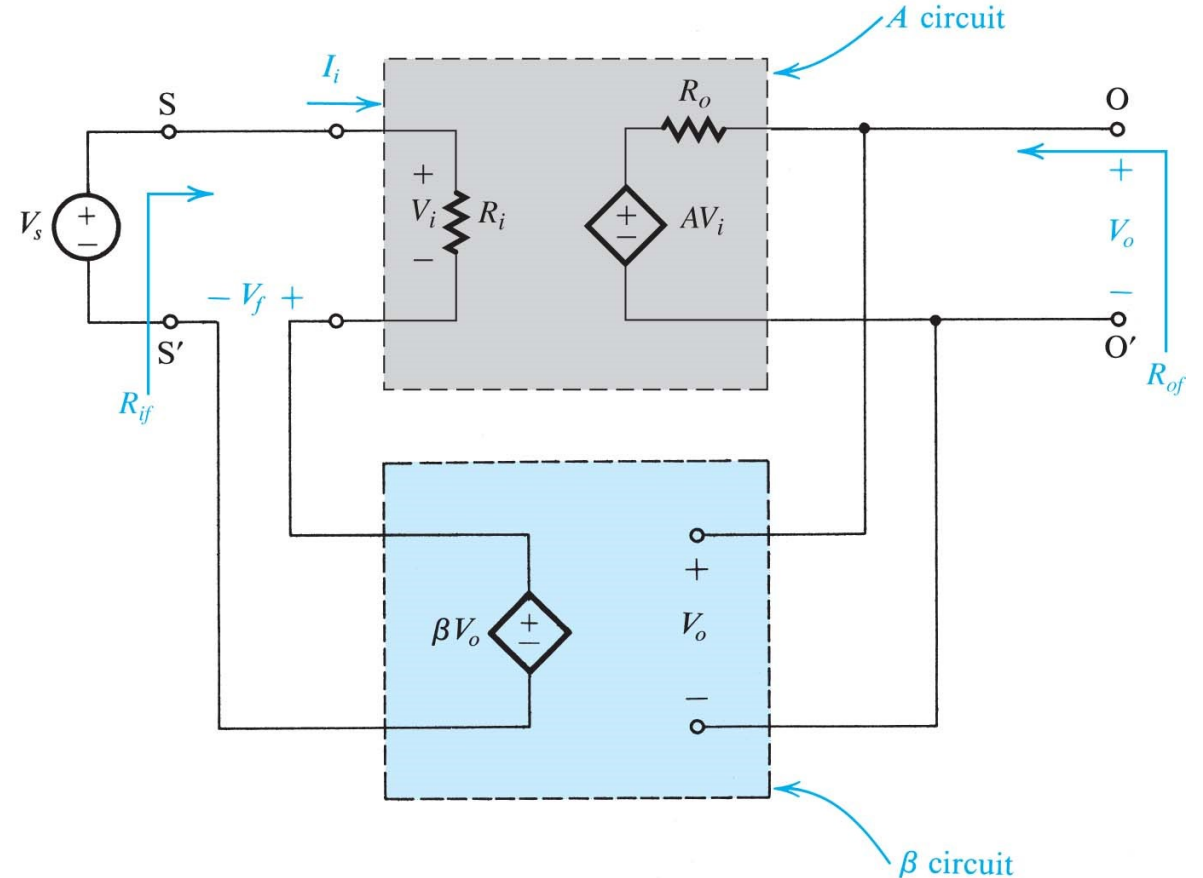
- Determine the open loop gain from feedback factor and loop gain

$$A = \frac{A\beta}{\beta}$$



Sensing, Mixing, and Feedback Topology

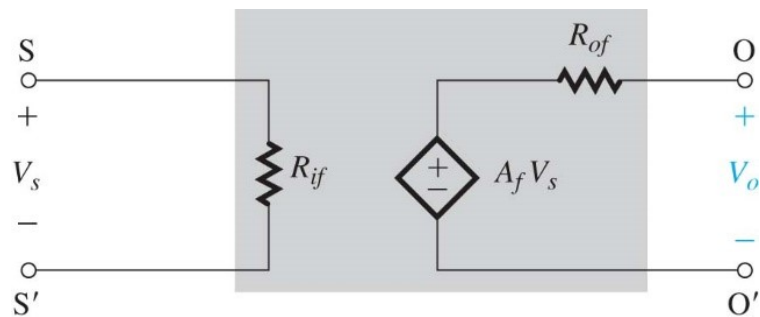
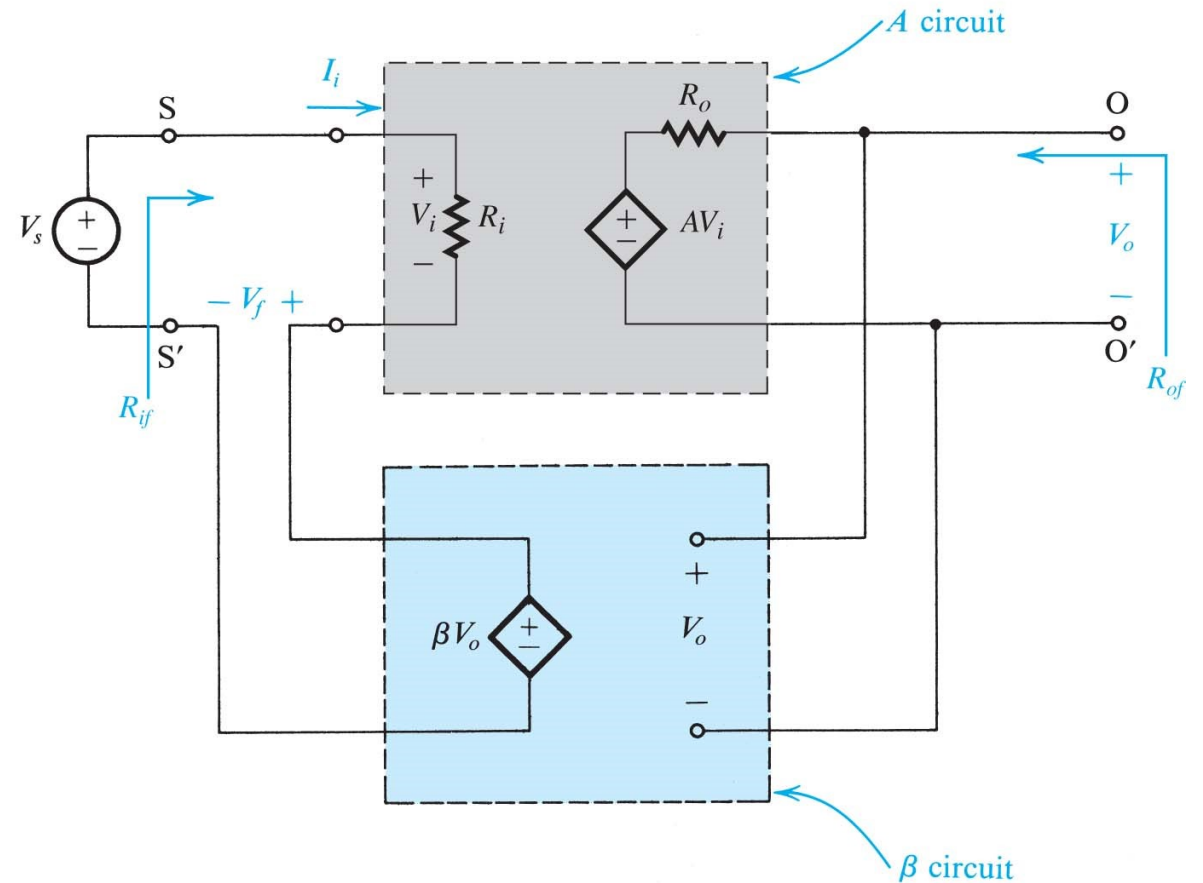
- Mixing on the input
 - Voltage (series) or current (shunt)
- Sensing on the output
 - Voltage (shunt) or current (series)
- Feedback topologies
 - Series-shunt (voltage)
 - Series-series (transconductance)
 - Shunt-shunt (transresistance)
 - Shunt-shunt (current)
- Feedback network typically loads circuit (not ideal probe and source)



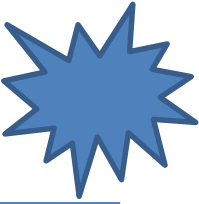
The appropriate feedback topology depends on amplifier type.

Series-Shunt Feedback Voltage Amplifier

- Series-shunt feedback
 - Input
 - Voltage mixing
 - Increased input resistance
 - Output
 - Voltage sampling
 - Reduced output resistance



BREAK



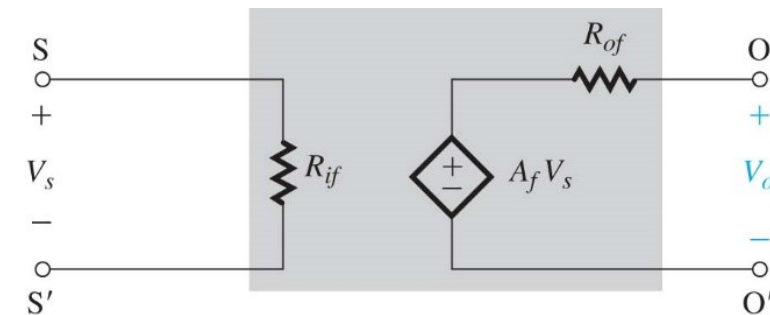
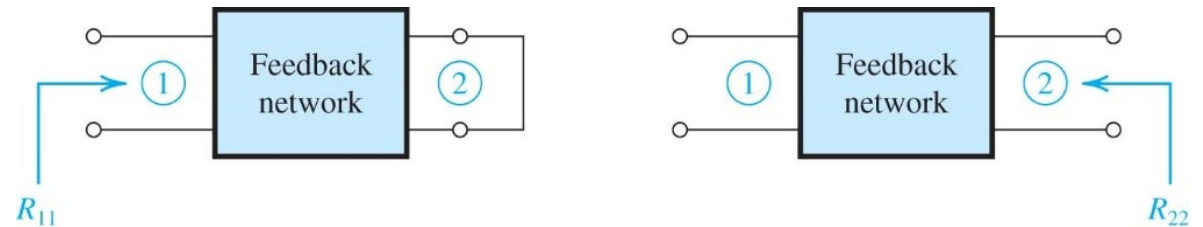
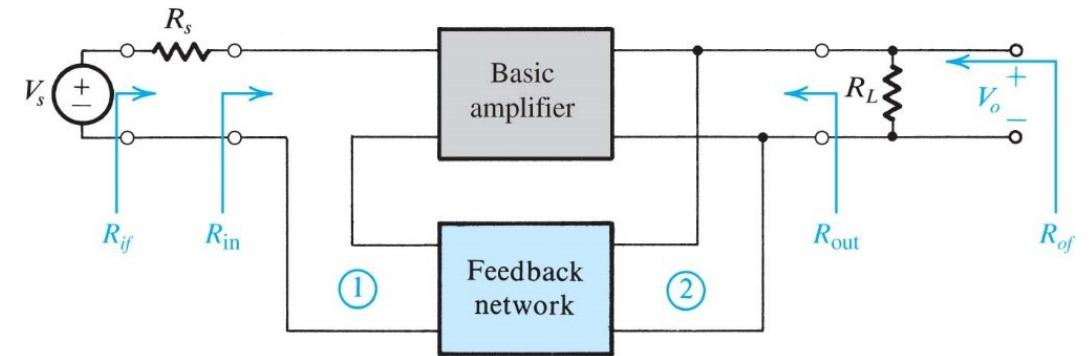
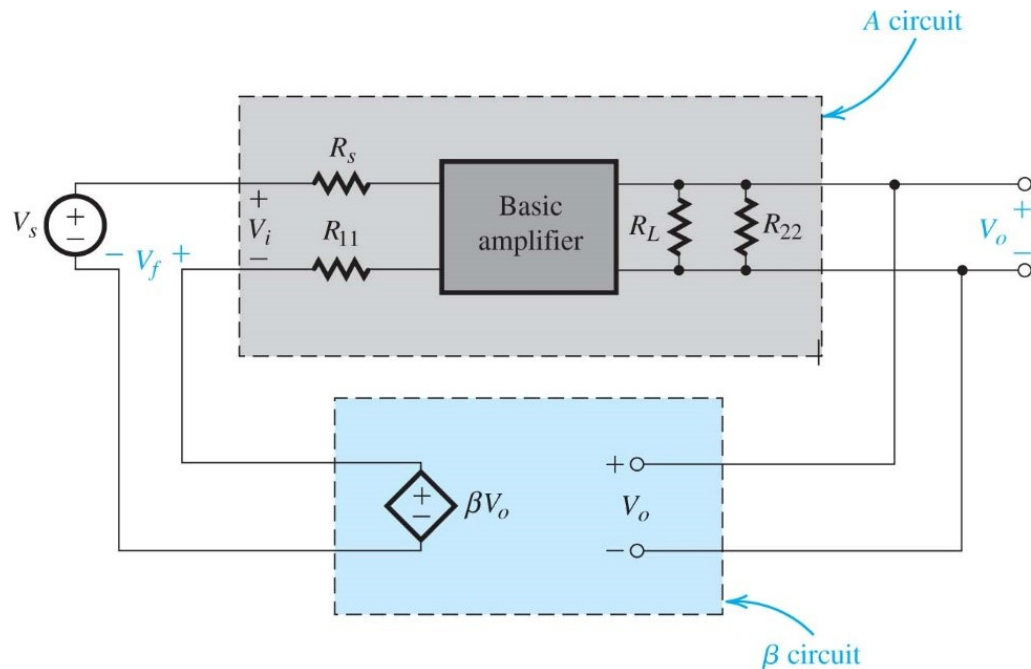
Series-Shunt Feedback Voltage Amplifier Analysis

- Include source, load and feedback loading

$$R_{if} = R_{S1}(1 + A\beta), \quad R_{of} = R_{L2}/(1 + A\beta)$$

$$R_i = R_{if} - R_S, \quad R_o = 1/\left(\frac{1}{R_{of}} - \frac{1}{R_L}\right)$$

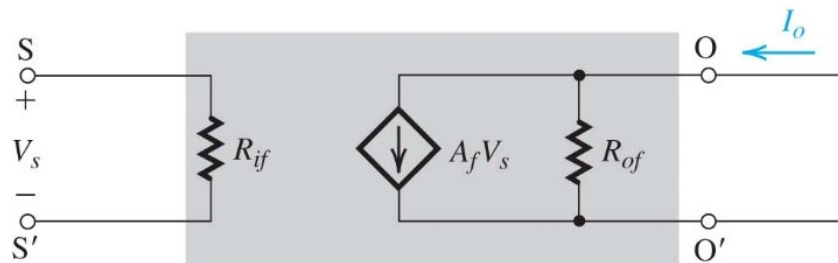
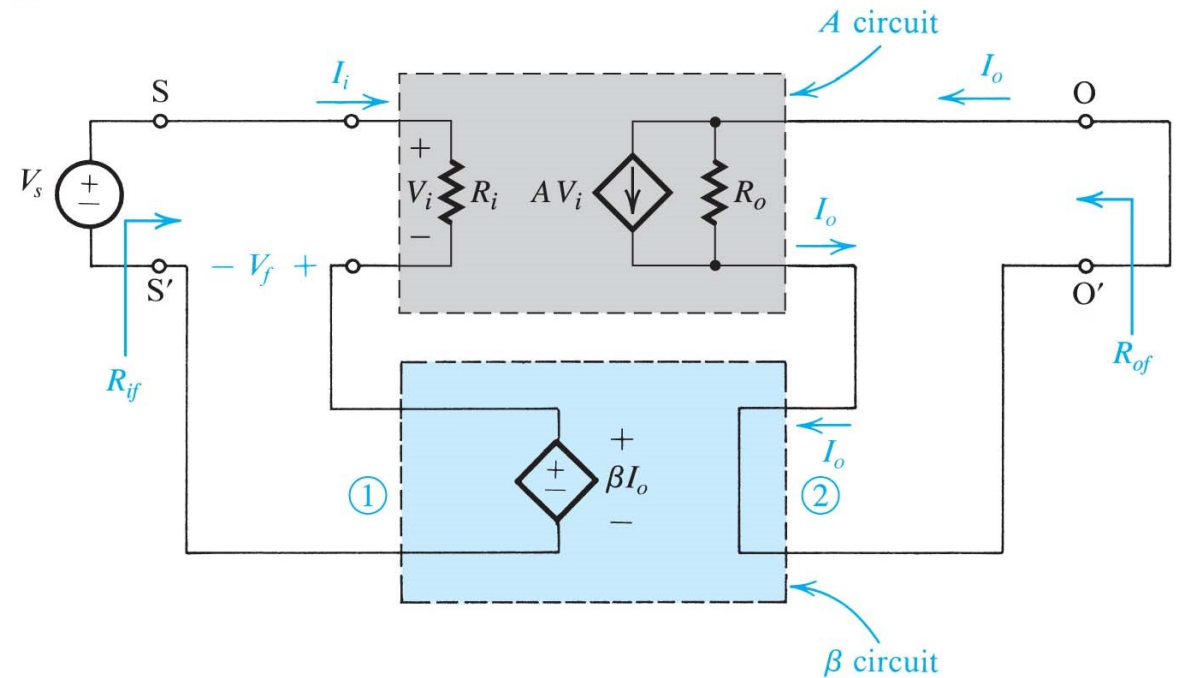
- Determine β , R_{11} , R_{22} , A_f , R_i , and R_o



Shunt short; series sever.

(Series-Series Feedback Transconductance Amplifier)

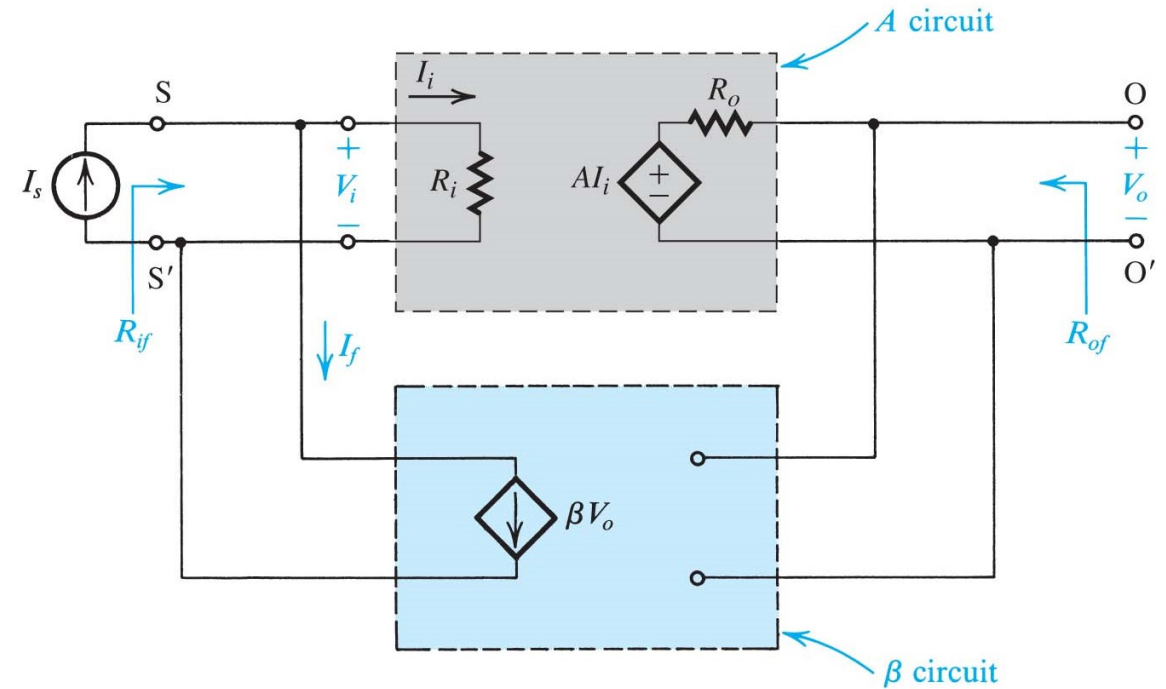
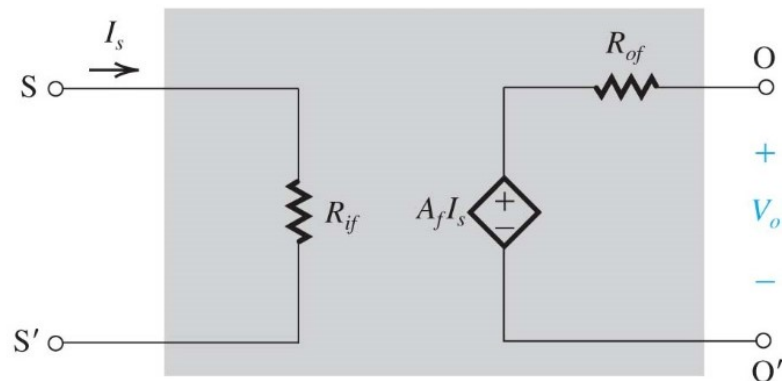
- Series-series feedback
 - Input
 - Voltage mixing
 - Increased input resistance
 - Output
 - Current sampling
 - Increased output resistance



Shunt short; series sever.

(Shunt-Shunt Feedback Transresistance Amplifier)

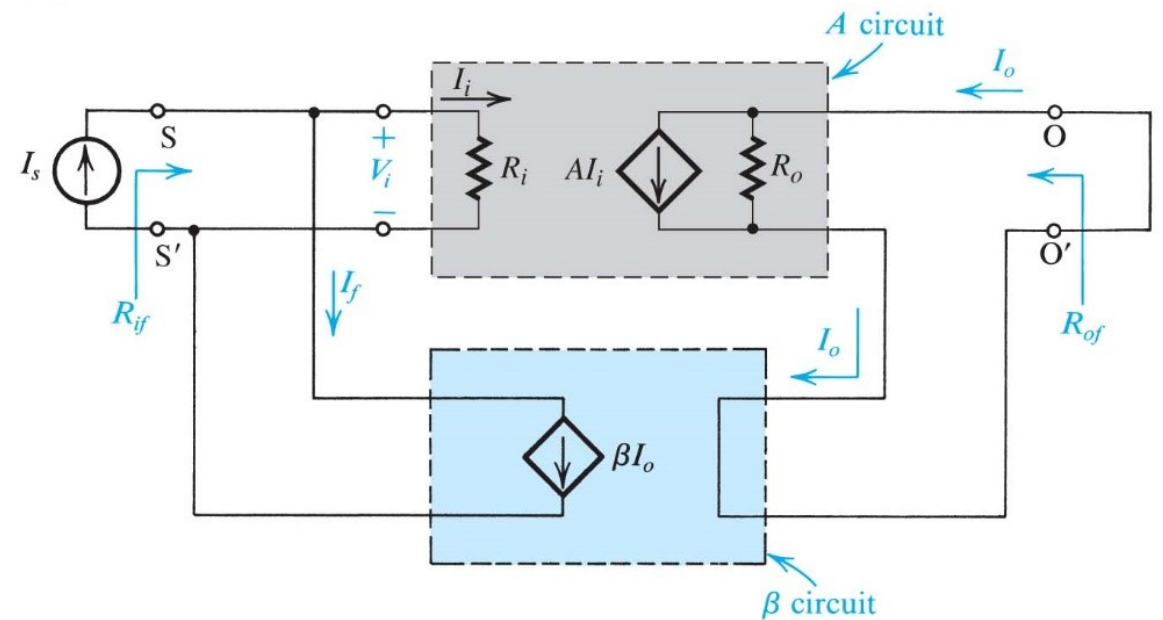
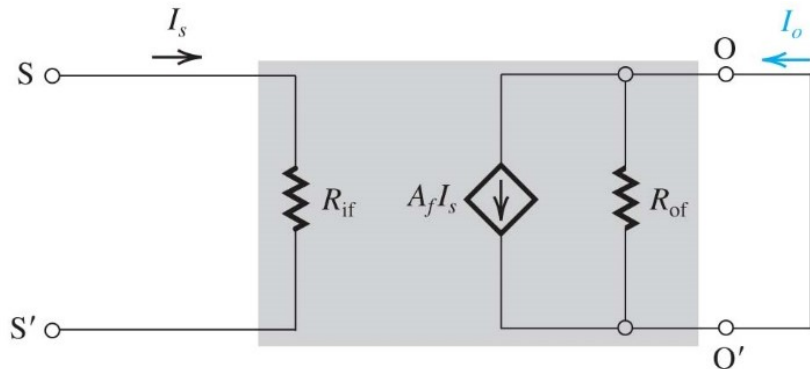
- Shunt-shunt feedback
 - Input
 - Current mixing
 - Reduced input resistance
 - Output
 - Voltage sampling
 - Reduced output resistance



Shunt short; series sever.

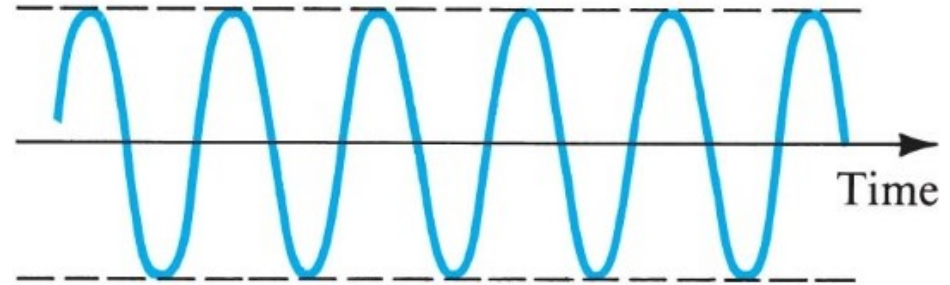
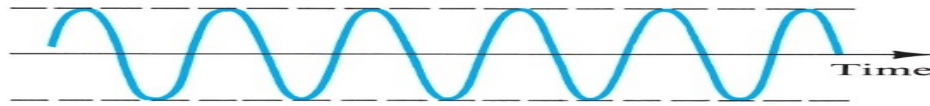
(Shunt-Series Feedback Current Amplifier)

- Shunt-series feedback
 - Input
 - Current mixing
 - Reduced input resistance
 - Output
 - Current sampling
 - Increased output resistance

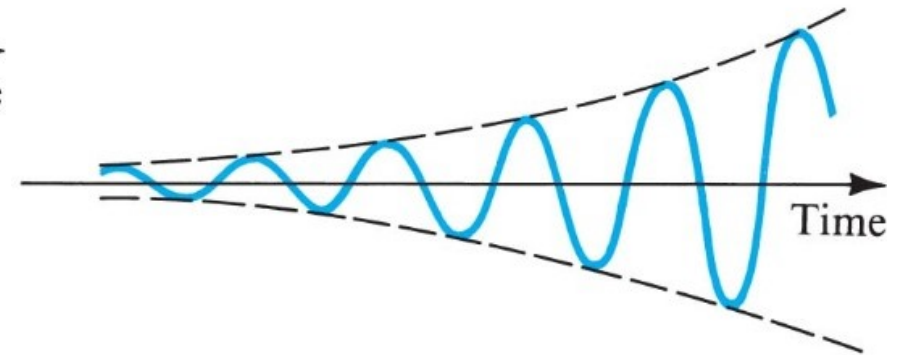
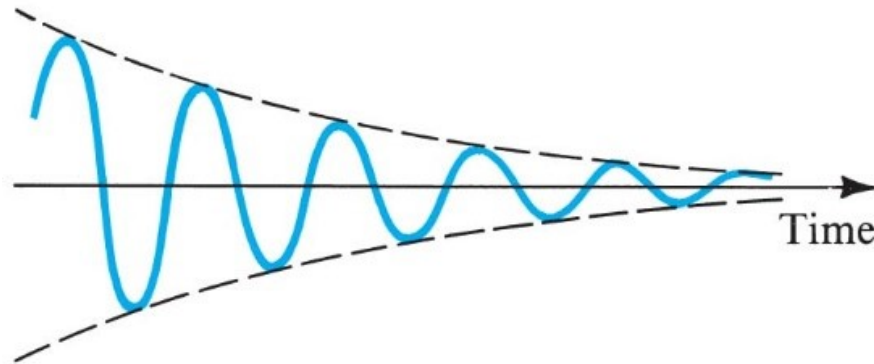


Shunt short; series sever.

An amplifier must be stable; why?

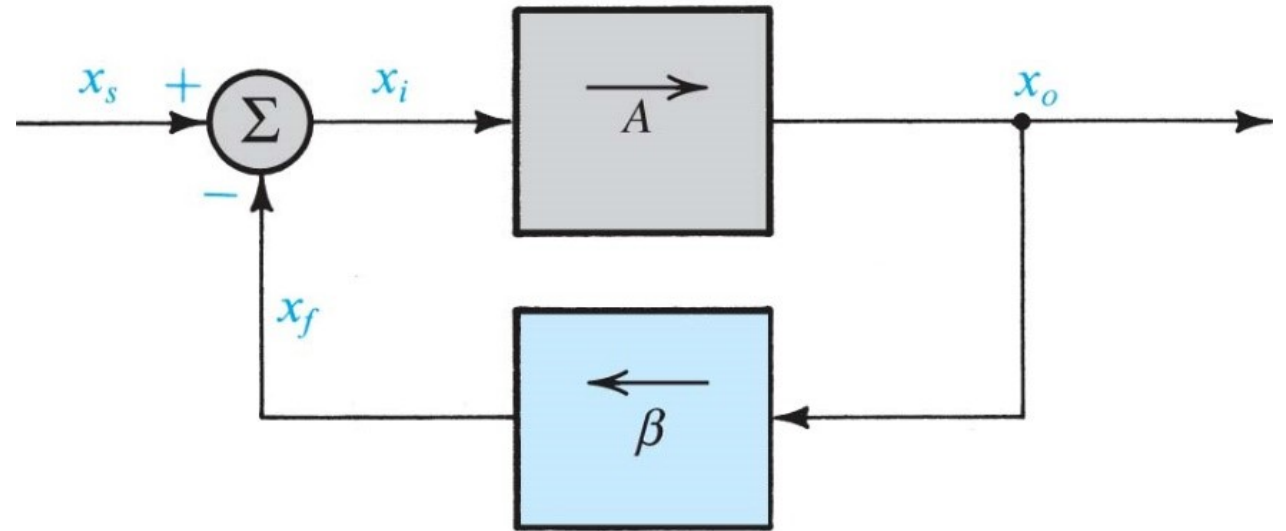


Think, think, think.



Stability

- Negative feedback stabilises the amplifier
 - Input signal is reduced ($x_i = x_s - x_f$)
- Positive feedback risks instability
 - Input signal is boosted ($x_i = x_s + x_f$)
 - Stable oscillations if $A\beta = -1$
 - Regenerative oscillations if $A\beta < -1$

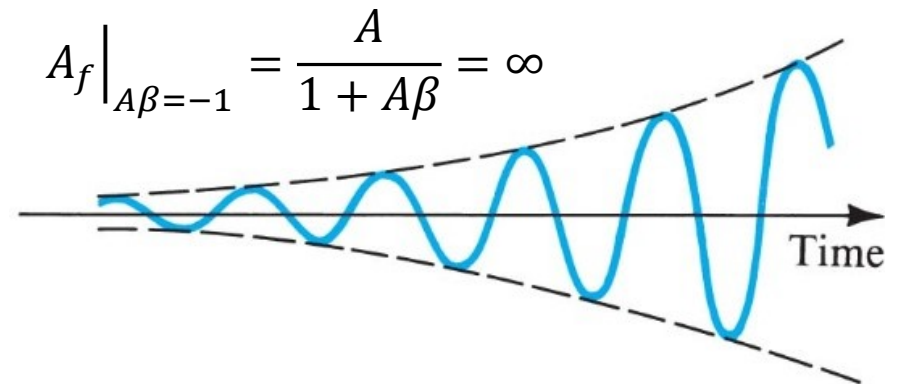


- Loop gain is frequency dependent

$$A_f(j\omega) = \frac{A(j\omega)}{1 + A(j\omega)\beta(j\omega)} = \frac{A(j\omega)}{D(j\omega)}$$

- Characteristic equation of feedback poles

$$D(j\omega) = 1 + A(j\omega)\beta(j\omega) = 0$$



Nyquist Plot

- Loop gain, $A(j\omega)\beta(j\omega)$, plotted in complex plane

- Complex function (polar format)

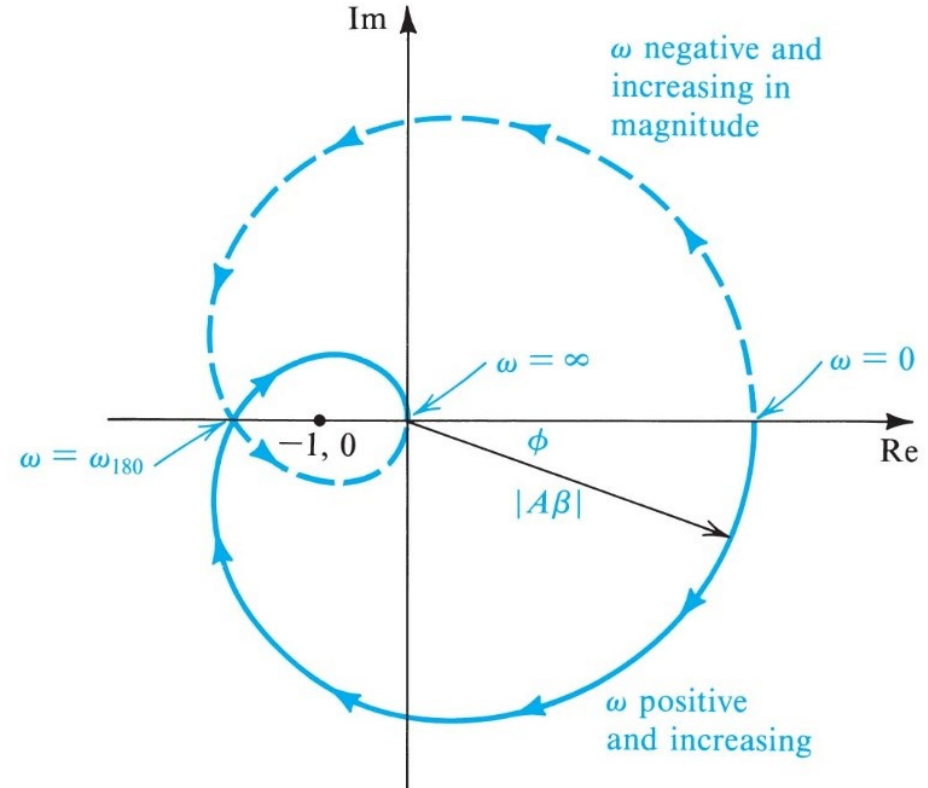
$$A(j\omega)\beta(j\omega) = |A(j\omega)\beta(j\omega)| \exp[j\Phi(j\omega)]$$

- Phase inversion frequency, ω_{180}

$$\Phi(j\omega_{180}) = 180^\circ$$

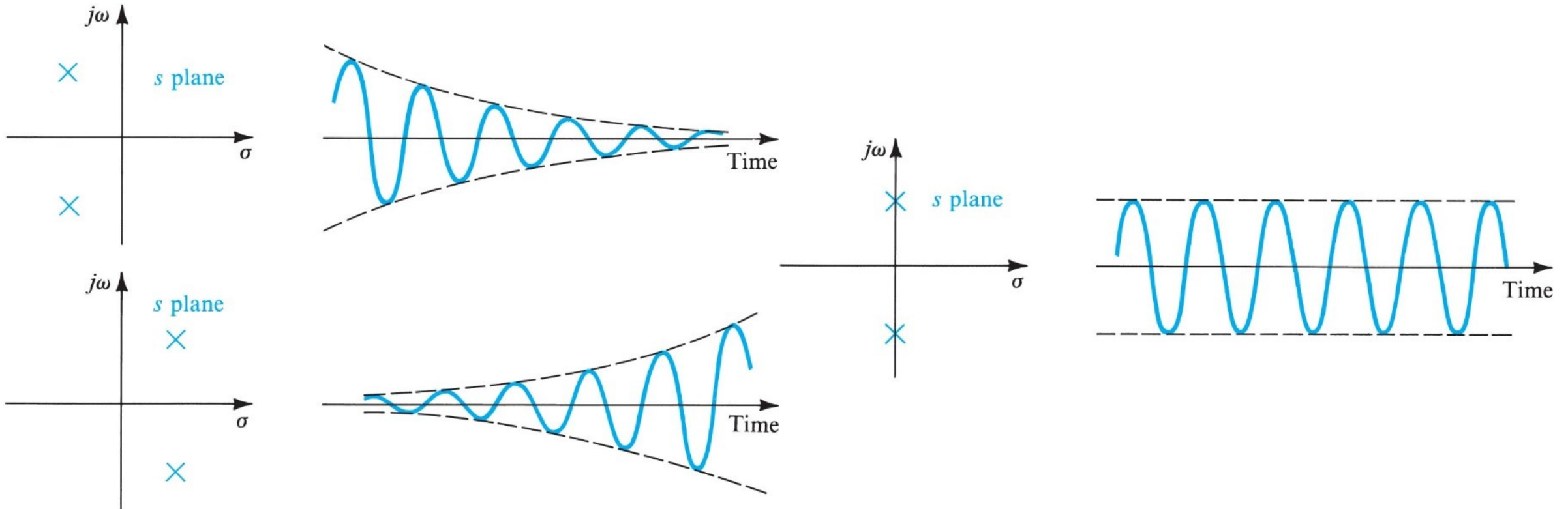
- Feedback amplifier must be stable if NOT encircling point (-1,0)

$$|A(j\omega)\beta(j\omega)|_{\omega=\omega_{180}} < 1$$



$$A_f(j\omega) = \frac{A(j\omega)}{1 + A(j\omega)\beta(j\omega)} = \frac{A(j\omega)}{D(j\omega)}$$

Stability and Pole Location

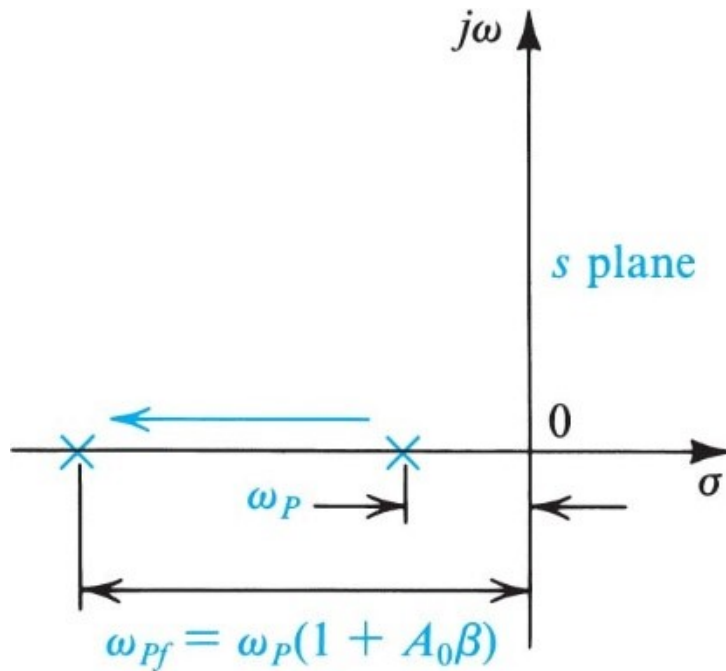


Poles must be kept in negative (left) half-plane.

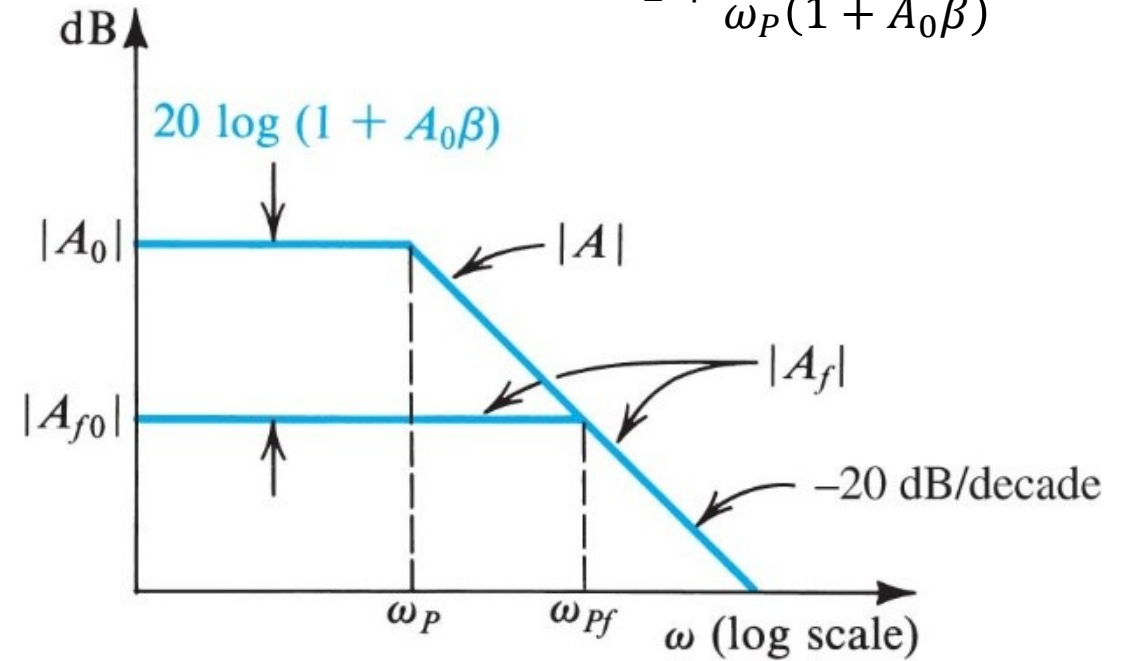


Single Pole Feedback Amplifier

- Feedback moves pole
- Root locus diagram visualises effects on poles
 - Feedback moves pole to higher frequency



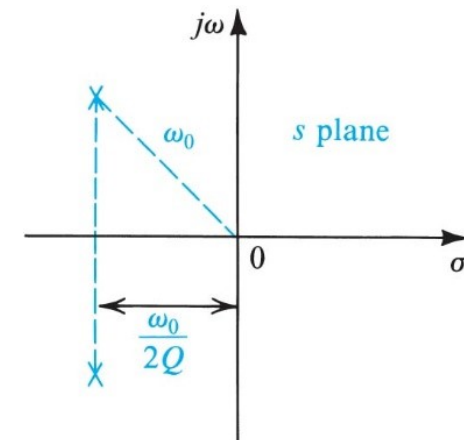
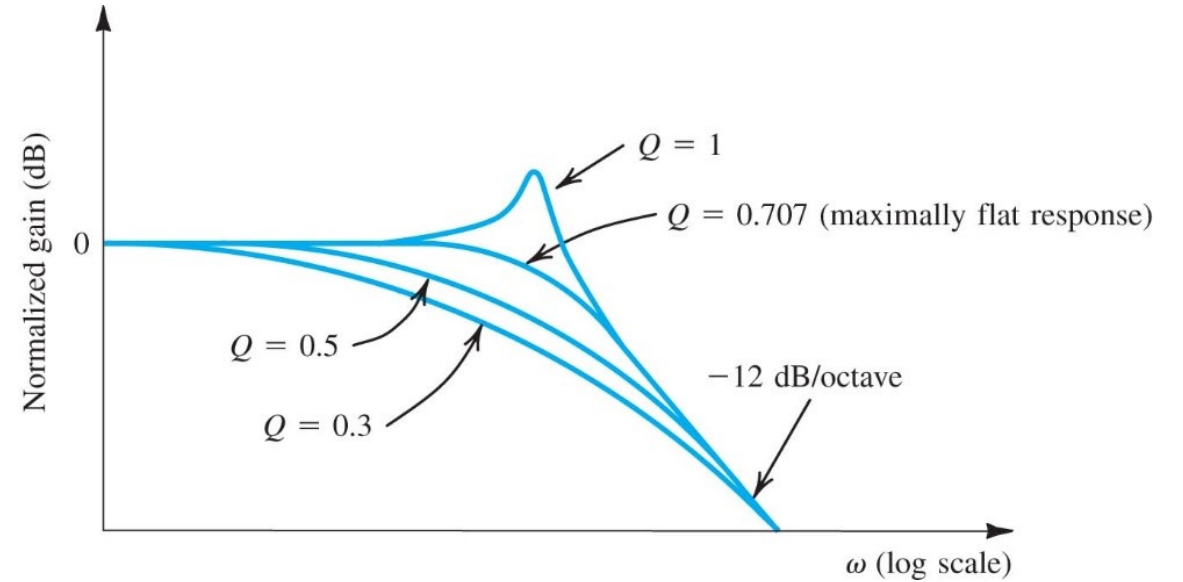
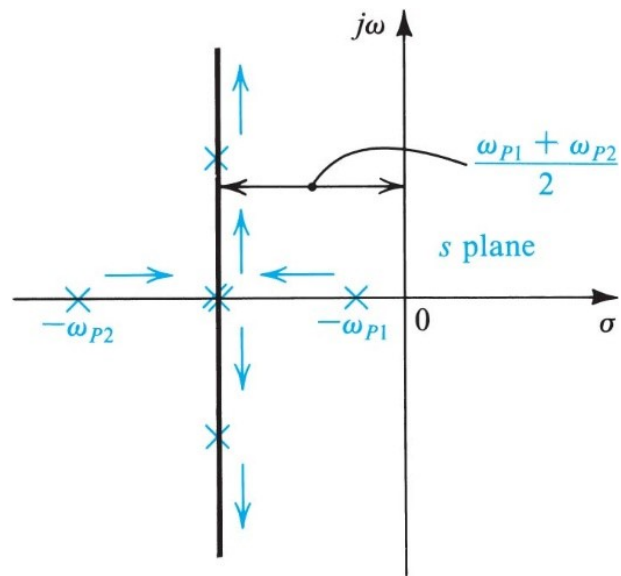
$$A(j\omega) = A_0 \frac{1}{1 + \frac{j\omega}{\omega_P}}$$
$$A_f(j\omega) = \frac{A_0 / (1 + A_0\beta)}{1 + \frac{j\omega}{\omega_P (1 + A_0\beta)}}$$



Bandwidth extension from another perspective.

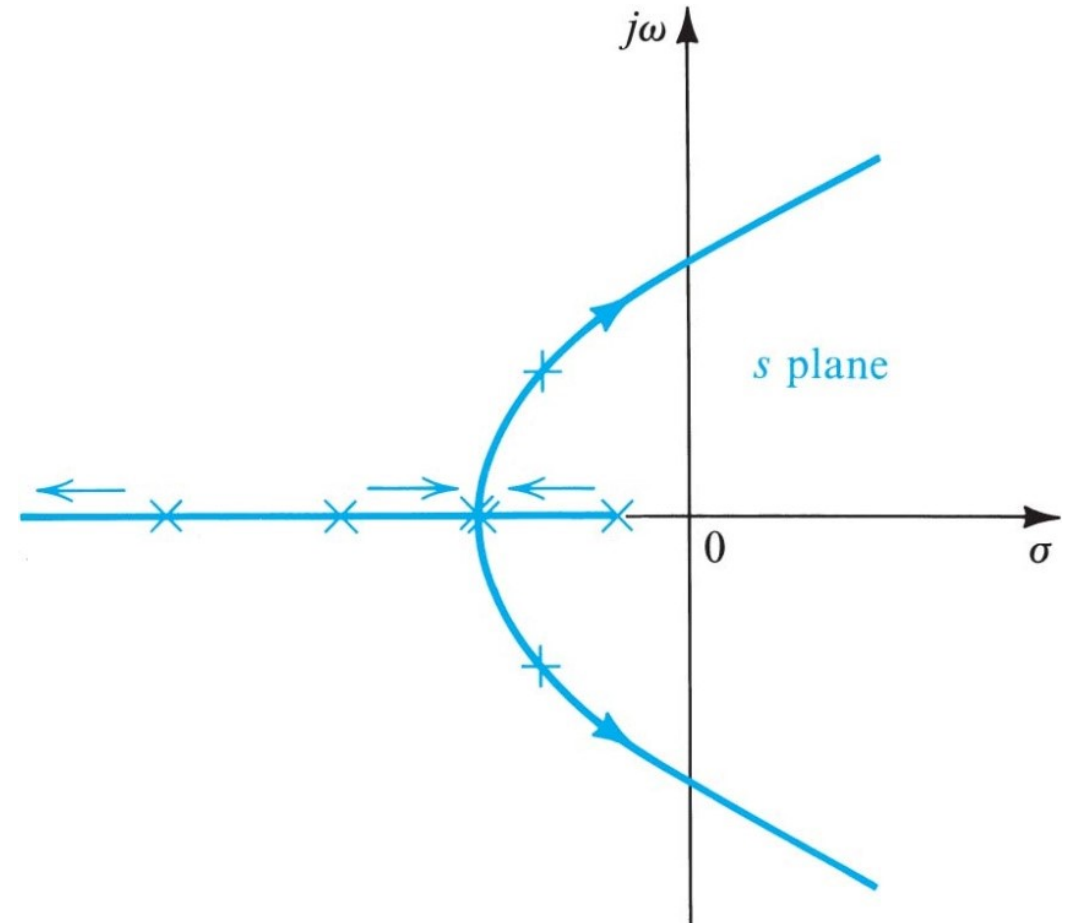
Two Pole Feedback Amplifier

- Feedback merges poles into a resonance
- Root locus diagram visualises effects on (two) poles
 - Feedback first brings poles together, then poles split into conjugate pair



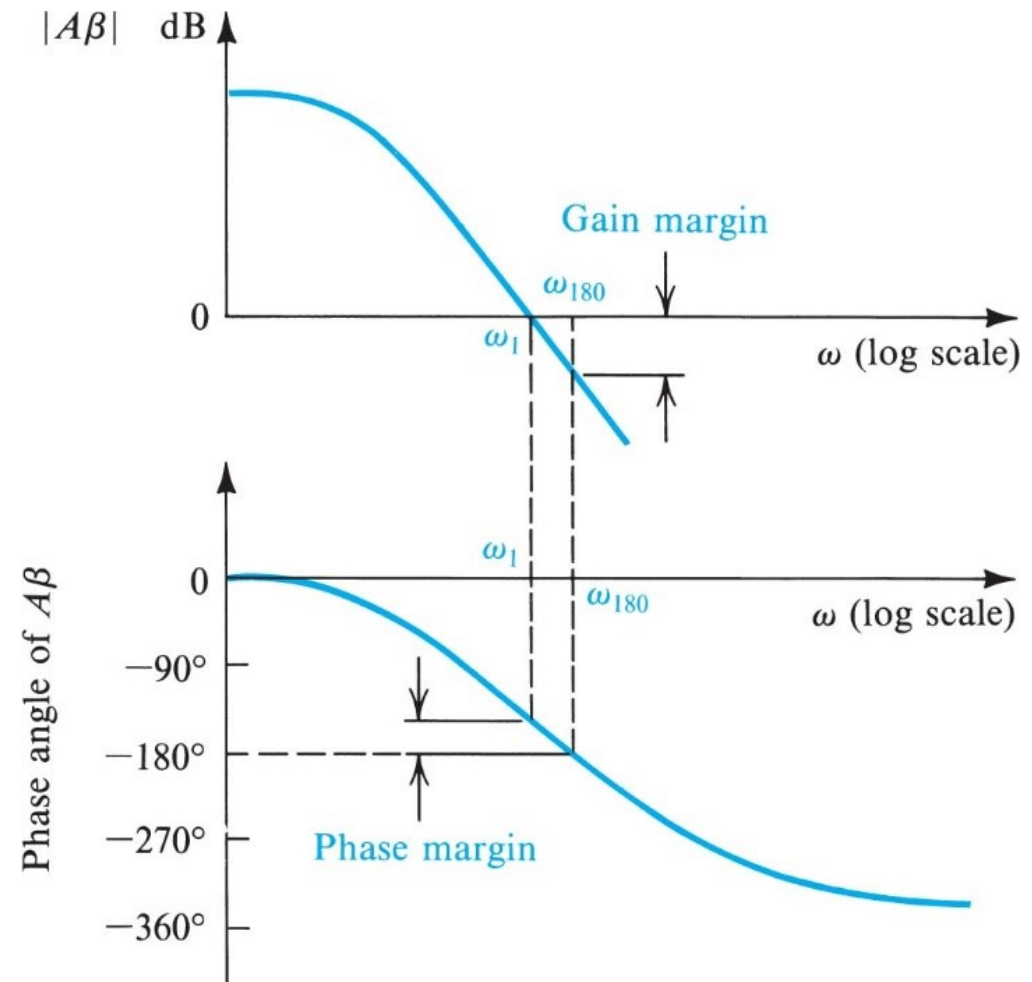
Three (or More) Pole Feedback Amplifier

- Feedback potentially creates instability
- Root locus diagram visualises effects on (three) poles
 - One pole moved to high frequency
 - Feedback brings low poles together, then poles split into conjugate pair
 - Conjugate pair approaches positive half-plane



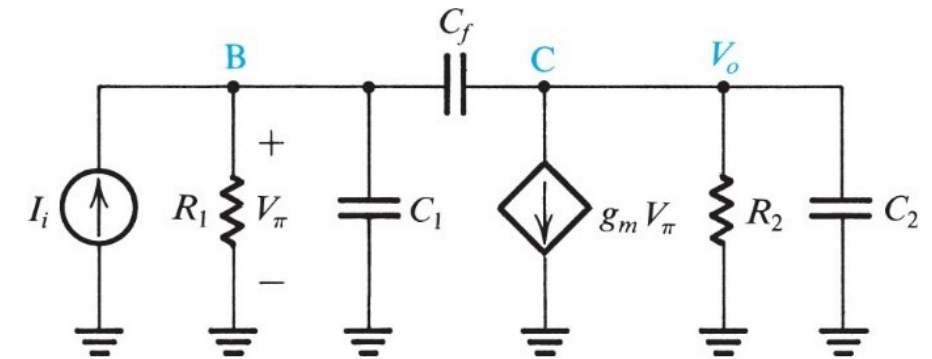
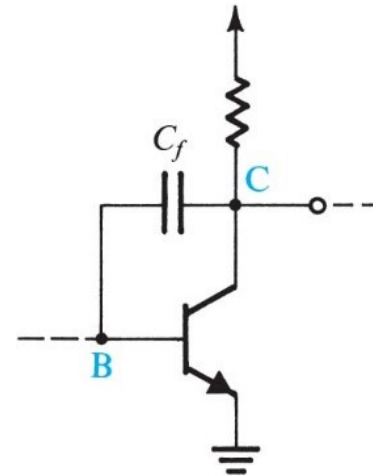
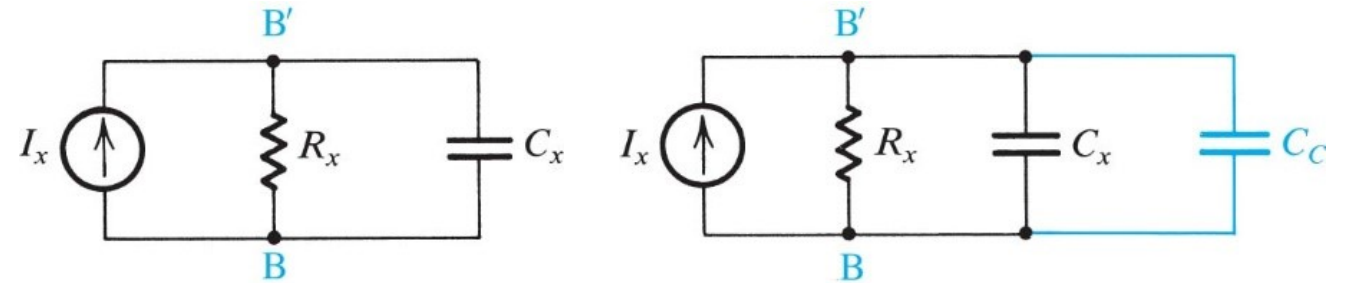
Gain and Phase Margin

- “Destructive” positive feedback
 - Loop gain with phase inversion
 - Risk of oscillation (not an amplifier)
- Gain margin
 - Evaluated at phase inversion
- Phase margin
 - Evaluated at unity gain



Frequency Compensation and Pole Splitting

- Compensate feedback pole movement
 - Poles split by added capacitance
 - Increased stability
- Frequency compensation
 - Compensate at in-/ output
- Miller compensation
 - Use the Miller effect to magnify effect of capacitor in feedback configuration



Force gain cutoff before phase inversion.