

# Formulas for High Speed Devices

## 2018

### 1 Semiconductor Physics

#### 1.1 3D Energy Bands

Kinetic Energy:

$$E - E_c = \frac{\hbar^2}{2m^*} (k_x^2 + k_y^2 + k_z^2)$$

Effective mass:

$$m^* = \frac{\hbar^2}{\frac{d^2E}{dk^2}}$$

Group Velocity:

$$v_x = \frac{1}{\hbar} \frac{dE_k}{dk_x} = \frac{\hbar}{m^*} k_x$$

Density of states:

$$D_{3D} \frac{(2m^*)^{1.5}}{2\pi^2\hbar^3} \sqrt{E - E_c}$$

#### 1.2 2D Energy Bands

Infinite quantum well energies:

$$E_n \approx \frac{\hbar^2 n^2 \pi^2}{2m^* W^2}$$

Sub-band energy dispersion:

$$E_k = \frac{\hbar}{2m^*} (k_x^2 + k_y^2) + E_n + E_c$$

Density of states:

$$D_{2D} = \sum \frac{m^*}{\pi\hbar^2} \Theta(E - E_n)$$

Effective density of states:

$$N_{2D} = \frac{m^* kT}{\pi \hbar^2} [m^2]$$

$$n_s(E_F) = \int_{E_c}^{\infty} D_{2D} f_0(E - E_n) dE = N_{2D} \sum_n \ln \left[ 1 + e^{\frac{E_F - E_n}{kT}} \right]$$

### 1.3 1D Statistics

Carrier concentration:

$$n_L(E_F - E_C) = N_{1D} F_{-1/2}(\eta_F)$$

Effective density of states:

$$N_{1D} = \frac{\sqrt{2m^* kT}}{\hbar \sqrt{\pi}} m^{-1}$$

### 1.4 Crystal Growth

Lattice mismatch:

$$f = \frac{\Delta a}{a} - 0.014$$

Effective hole mass:

$$m_h^* = \frac{(m_{hh}^*)^{3/2} + (m_{lh}^*)^{3/2}}{(m_{hh}^*)^{1/2} + (m_{lh}^*)^{1/2}}$$

### 1.5 Fermi Level and F/D Statistics

Fermi-Dirac distribution:

$$f_0(E, E_F) = \frac{1}{1 + e^{\frac{E - E_F}{kT}}}$$

Total concentration of free electrons:

$$n = \int_{E_c}^{\infty} D_{3D}(E) f_0(E - E_F) dE$$

Effective density of states:

$$N_c = 2 \left( \frac{2\pi m_e^* kT}{h^2} \right)^{1.5}$$

$$N_v = 2 \left( \frac{2\pi m_h^* kT}{h^2} \right)^{1.5}$$

Electron concentration:

$$\frac{n}{N_C} = \frac{2}{\sqrt{\pi}} \int_0^\infty \frac{\sqrt{\eta}}{1 + e^{\eta - \eta_F}} d\eta = F_{1/2}(\eta_F)$$

$$\eta_F = \frac{E_F - E_n}{kT}$$

Maxwell-Boltzmann statistics, valid if  $n < 0.05N_c$  or  $E_c - E_F \gg 3kT$ :

$$n \approx N_c e^{(E_F - E_C)/kT}$$

$$p \approx N_v e^{(E_v - E_F)/kT}$$

If  $n$  is known:

$$\frac{E_f - E_C}{kT} \approx \ln\left(\frac{n}{N_C}\right) + \frac{n}{N_C} \cdot \frac{1}{(64 + \frac{3.6n}{N_C})^{1/4}}$$

Joyce Dixon approximation:

$$\frac{E_f - E_C}{kT} \approx \ln\left(\frac{n}{N_C}\right) + \frac{1}{\sqrt{8}} \left(\frac{n}{N_C}\right) - 0.00495 \left(\frac{n}{N_C}\right)^2 + \dots$$

## 1.6 Intrinsic Semiconductors

Carrier concentration, only valid if  $n < N_c$  and  $p < N_V$ :

$$n = p = n_i = \sqrt{N_V N_C} \cdot e^{-\frac{E_G}{2kT}}$$

## 1.7 Doped Semiconductors

n-doping ( $N_d \gg n_i$ ):

$$n = \frac{\sqrt{N_d^2 + 4n_i^2} + N_d}{2} \approx N_d$$

p-doping ( $N_a \gg n_i$ ):

$$p = \frac{\sqrt{N_a^2 + 4n_i^2} + N_a}{2} \approx N_a$$

Law of mass action:

$$np = n_i^2$$

For n-type material:

$$n_n \approx N_d \gg n_i$$

$$p_n \approx \frac{n_i^2}{N_d} \ll n_i$$

## 1.8 Electrostatics

Poisson's equation:

$$\frac{d^2}{dx^2}v(x) = -\frac{q}{\epsilon_r \epsilon_0}(p(x) - n(x) + N_d(x) - N_a(x)) \quad (\text{1D})$$

$$\Delta V(x, y, z) = \frac{\rho(x, y, z)}{\epsilon_r \epsilon_0} \quad (\text{3D})$$

Relations between  $\mathcal{E}$ ,  $V$  and  $\rho$ :

$$\begin{aligned}\mathcal{E}(x) &= -\nabla V \\ \frac{q}{\epsilon_s} \rho(x) &= \nabla \mathcal{E}\end{aligned}$$

Potential energy of an electron:

$$E_p = -qV(x) + E_C$$

Potential energy of a hole:

$$E_p = (+)qV(x) + E_V$$

## 1.9 Drift and Diffusion

**Long Devices** - accurate for low  $\mathcal{E}$ -fields, low carrier concentrations and long devices.

Electron current density:

$$J = q\mu_n n \epsilon + qD_n \frac{dn}{dx}$$

Hole Current Density:

$$J = q\mu_p p \epsilon - qD_p \frac{dp}{dx}$$

Einstiens relation:

$$D_n = \frac{kT}{q} \cdot \mu_n$$

Drift velocity:

$$v_n = \mu_n \cdot \mathcal{E}$$

**Short (hot) Devices** - accurate for short (hot) devices and for high  $\mathcal{E}$ -fields.

Velocity saturation:

$$v_{el} \approx \frac{\mu_n \cdot \mathcal{E}}{1 + \mathcal{E}/\mathcal{E}_{crit}}$$

Critical  $\mathcal{E}$ -field around 3-4 kV/cm

**Ballistic Devices** - accurate for nanoscale devices.  $\lambda > L$ .

$$v_x = \frac{\hbar k_x}{m^*}$$

## 2 Transistor Fundamentals

### 2.1 n-type FET

On-resistance:

$$R_{on} = \left( \frac{dI}{dV_{ds}} \right)^{-1} \Big|_{V_{DS} \rightarrow 0V} [\Omega \mu m]$$

Output conductance:

$$g_d = \frac{dI_D}{dV_{DS}} \Big|_{V_{DS}, V_{GS}}$$

Transconductance:

$$g_m = \frac{dI_D}{dV_{GS}} \Big|_{V_{DS}, V_{GS}}$$

Geometric length scale:

$$\lambda = t_s + 2t_i$$

$$L > 2\lambda$$

where  $t_i$  is the thickness of the insulator, and  $t_s$  is the thickness of the channel.

## 3 2D FET Electrostatics

### 3.1 Charge Density FET

On-state:

$$qn_s = C_G(V_{GS} - V_T)$$

Off-state:

$$qn_s \approx N_{2D} e^{\frac{q}{kT}(V_{GS} - V_T)} \approx 0$$

### 3.2 Gate Capacitance

Quantum capacitance:

$$C_q = \frac{q^2 m^*}{\pi \hbar^2}$$

Quantum well charge:

$$\begin{aligned} n_s &= N_{2D} F_0(\eta_F) \approx \frac{m^*}{\pi \hbar^2} (E_F - E_1) \\ qn_s &\approx \frac{q^2 m^*}{\pi \hbar^2} \Psi_s = C_q \Psi_s \end{aligned}$$

Oxide capacitance:

$$C_{ox} = \frac{\epsilon_{ox} \epsilon_0}{t_{ox}}$$

Centroid Capacitance:

$$C_c = \frac{\epsilon_r \epsilon_0}{0.36 t_w}$$

Gate Capacitance:

$$\frac{1}{C_G} = \frac{1}{C_q} + \frac{1}{C_{ox}} + \frac{1}{C_c}$$

Gate-Source Voltage:

$$V_{GS} = \frac{qn_s}{C_{ox}} + \frac{qn_s}{C_q} + \frac{qn_s}{C_c}$$

### 3.3 Threshold Voltage

Ideal MOS:

$$V_T = \phi_m - \chi + \frac{E_q}{q}$$

Ideal HEMT:

$$V_T = \phi_b - \Delta E_c + \frac{E_1}{q} - \phi_{00}$$

where

$$\phi_{00} = \frac{qN_D}{2\epsilon_r \epsilon_0} (t_b - \delta)^2$$

## 4 Ideal Ballistic FETs

Drain current in saturation:

$$I^+ \approx \frac{qW2\sqrt{2m^*}}{2\pi^2\hbar^2} \left( \frac{q \cdot C'_{ox}}{C'_{ox} + \frac{C_q}{2}} \right)^{3/2} (V_{GS} - V_T)^{3/2}$$

Drain voltage in saturation:

$$V_{ds} \approx \frac{V_{GS} - V_T}{1 + \frac{C_q}{2C_{ox}}}$$

where  $C'_{ox} = C_{ox} || C_c$

## 5 Real Ballistic devices

Mean free path:

$$\lambda_0 \approx v_T \cdot \tau$$

Transmission probability:

$$T = \frac{\lambda_0}{\lambda_0 + L_{eff}}$$

Scattering current:

$$I_{scattering} = T \cdot I_{ballistic}$$

## 6 Resistance

### 6.1 3D

$$\begin{aligned} R &= \rho \cdot \frac{l}{A} \\ \rho_n &= \frac{1}{qn\mu_n} \\ \rho_p &= \frac{1}{qp\mu_p} \end{aligned}$$

### 6.2 2D

$$\begin{aligned} R &= \frac{\rho L}{tW} = R_{SH} \frac{L}{W} \\ n_s &= \int_0^t n(x) dx \\ R_{SH} &= \frac{1}{qn_s \mu_n} \end{aligned}$$

### 6.3 Semiconductor Contacts

Contact Resistance:

$$R_C = \frac{\sqrt{R_{SH}\rho_\sigma}}{W} \coth\left(L_c \sqrt{\frac{R_{SH}}{\rho_\sigma}}\right)$$

$$\coth(x) = \frac{\cosh(x)}{\sinh(x)}$$

Access resistance:

$$R_{lead} = \frac{R_{SH}L_{gs,gd}}{W}$$

Transfer length:

$$L_T = \sqrt{\frac{\rho_\sigma}{R_{SH}}}$$

Drain and Source resistance:

$$R_D = R_C + R_{lead,d}$$

$$R_S = R_C + R_{lead,s}$$

## 7 FET AC properties

### 7.1 Quasi-Static Operation

= The charging time of the inversion layer is ignored.

Gate current:

$$i_g = \frac{d}{dt}Q_G(t)$$

Drain Current:

$$i_D(t) = I_D(t) + \frac{d}{dt}Q_D(t) = I_D(t) + i_d(t)$$

Source current:

$$i_S = -I_D(t) + \frac{d}{dt}Q_S(t) = I_S(t) + i_s(t)$$

Charge neutrality:

$$Q_G(t) + Q_{CH}(t) = 0$$

$$Q_{CH}(t) = Q_D(t) + Q_S(t)$$

$$Q_G + Q_S + Q_D = 0$$

$$Q_S + Q_D = Q_G$$

Gate charge in saturation:

$$C'_G = \left( \frac{1}{C_{ox}} + \frac{2}{C_q} + \frac{1}{C_c} \right)^{-1}$$

$$Q_G = WLC'_G(v_{GS} - V_T)$$

## 7.2 Non Quasi-Static Operation

= It takes a finite time to charge the inversion layer due to finite velocity of the carriers. Introduces lag (resistors to  $C_{gg}$  and  $C_{gd}$ ).

Channel resistance (resistive  $C_{gs}$ ):

$$R_i = \frac{1}{2 \cdot 0.7WC_{gs}v^+} = \frac{1}{1.4g_m}$$

$$t_{1/2} \approx \frac{L_G}{2v^+}$$

# 8 Hybrid Pi Model

## 8.1 Large/Small Signal

$$i_G = I_{GS} + i_{gs} = I_{GS} + y_{11}v_{gs} + y_{12}v_{ds}$$

$$i_D = I_{DS} + i_{ds} = I_{DS} + y_{21}v_{gs} + y_{22}v_{ds}$$

$y$ -parameters:

$$y_{11} = \left. \frac{i_1}{v_1} \right|_{v_2=0}$$

$$y_{12} = \left. \frac{i_1}{v_2} \right|_{v_1=0}$$

$$y_{21} = \left. \frac{i_2}{v_1} \right|_{v_2=0}$$

$$y_{22} = \left. \frac{i_2}{v_2} \right|_{v_1=0}$$

Common source FET  $y$ -parameters:

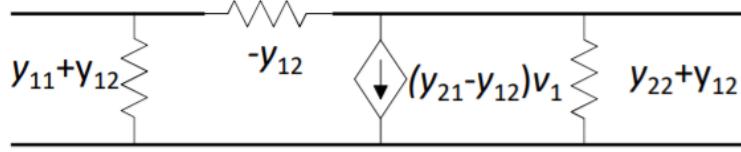
$$y_{11} = j\omega C_{gg,t}$$

$$y_{12} = -j\omega C_{gd,t}$$

$$y_{21} = g_m - j\omega C_{dg,t}$$

$$y_{22} = g_d + j\omega C_{dd,t}$$

General hybrid-Pi:



Capacitances:

$$C_{gs} = C_{gg} - C_{gd}$$

$$C_{sd} = C_{dd} - C_{dg}$$

$$C_m = C_{dg} - C_{gd}$$

In saturation :

$$C_{gg} = C_{gs}$$

$$C_{dd} \approx 0$$

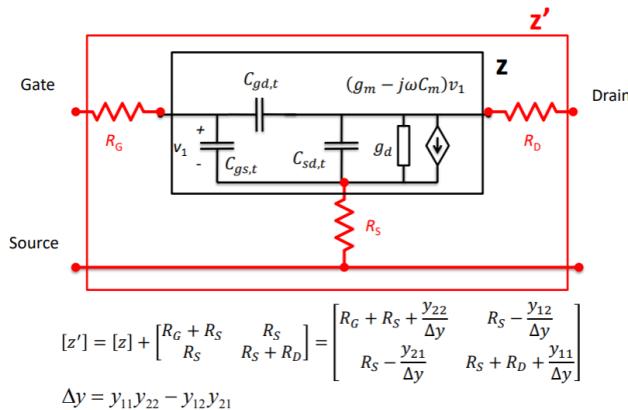
$$C_{dg} \approx 0$$

Parasitic drain and source resistance:

$$R_S = R_C + R_{lead,s}$$

$$R_D = R_C + R_{lead,d}$$

Complete small signal MOSFET model:



## 9 Gain and Stability

### 9.1 Current Gain

No parasitic resistances ( $R_S = R_D = 0$ ):

$$h_{21} = -\frac{z_{21}}{z_{22}} = \frac{g_m - j\omega C_{dg,t}}{j\omega C_{gg,t}} \approx \frac{g_m}{j\omega C_{gg,t}}$$

$$f_T = \frac{g_m}{2\pi C_{gg,t}}$$

With parasitic resistances ( $R_S$  &  $R_D > 0$ ):

$$h'_{21} = \frac{g_m}{j\omega [C_{gg,t} + (R_S + R_D)C_{gg,t}g_d + (R_D + R_D)C_{gd,t}g_m]}$$

$$f_T = \frac{1}{2\pi} \left( \frac{C_{gg,t}}{g_m} + \frac{C_{gg,t}}{g_m} (R_S + R_D)g_d + (R_S + R_D)C_{gd,t} \right)^{-1} \approx \frac{g_m}{2\pi C_{gg,t}}$$

where  $C_{gg,t} = C_{gg}(L)$  (*intrinsic*) +  $C_{gg,p}$  (*parasitic*)

## 9.2 Gain Expressions

Available gain:

$$G_A = \frac{P_{out}}{P_{AVS}}$$

Operating gain:

$$G_P = \frac{P_L}{P_{in}}$$

Transducer gain:

$$G_T = \frac{P_L}{P_{AVS}}$$

## 9.3 Stability

Sterns Stability factor, stable if  $k > 1$ :

$$k = \frac{2Re(y_{11}) \cdot Re(y_{22}) - Re(y_{12}) \cdot Re(y_{21})}{|y_{12} \cdot y_{21}|}$$

Stability factor, S-parameters:

$$K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2}{2|S_{21}S_{12}|}$$

$$\Delta = S_{11}S_{22} - S_{12}S_{21}$$

## 9.4 Power Gain Definitions

Maximum Available Gain:

$$MAG = \left| \frac{y_{21}}{y_{12}} \right| \cdot (k - \sqrt{k^2 - 1})$$

Maximum Stable Gain:

$$MSG = \left| \frac{y_{21}}{y_{12}} \right|$$

Unilateral Gain:

$$U = \frac{|\theta_{21} - \theta_{12}|^2}{4[Re(\theta_{11}) \cdot Re(\theta_{22}) - Re(\theta_{12}) \cdot Re(\theta_{21})]}$$

where  $\theta_{ij}$  is y, z, h, ...

$$f_{max} = \sqrt{\frac{f_T}{8\pi R_G C_{gd,t} \left[ 1 + \frac{2\pi f_T}{C_{gd,t}} \Psi \right]}}$$

$$\Psi = (R_D + R_S) \frac{C_{gg,t}^2 \cdot g_d^2}{g_m^2} + (R_D + R_S) \frac{C_{gg,t} \cdot C_{gd,t} \cdot g_d}{g_m} + \frac{C_{gg,t} \cdot g_d}{g_m^2}$$

## 10 Noise

### 10.1 Thermal Noise

*In all resistors.*

$$\overline{v^2} = 4kT R \Delta f$$

$$\overline{i^2} = \frac{4kT}{R} \Delta f$$

Total noise power:

$$P = \frac{\overline{v^2}}{R} = 4kT \Delta f$$

### 10.2 Shot Noise

*Discrete nature of electron charge.*

$$\overline{i^2} = 2qI_D \Delta f$$

### 10.3 1/f Noise

*Semiconductor defects cause trapping of electrons.*

$$\overline{i^2} = K_1 \frac{I^a}{f} \Delta f$$

$a \approx 0.5 - 2$

#### 10.4 Noise In a Diffusive FET

$$\overline{i^2} = 4kT\gamma g_0 \approx 4kT \frac{2}{3}g_m\Delta f$$

where  $\frac{2}{3} < \gamma < 5$ .

$$\overline{v^2} = 4kTR_{gs}\Delta f$$

#### 10.5 Signal to Noise Ratio

$$P_{signal} = \frac{v_{signal}^2}{4R_S}$$

$$P_{g,noise} = kT$$

$$P_{amp,noise} = \frac{\overline{V_{total}^2}}{4R_S}$$

$$SNR_1 = \frac{P_{signal}}{P_{g,noise}}$$

$$SNR_2 = \frac{P_{signal}}{P_{g,noise} + P_{amp,noise}}$$

Noise factor:

$$F = \frac{SNR_1}{SNR_2} = \frac{P_{g,noise} + P_{amp,noise}}{P_{g,noise}} = 1 + \frac{P_{amp,noise}}{kT}$$

Noise figure:

$$NF = 10\log(F)$$

#### 10.6 Minimum NF and Optimal $Z_S$

$$F_{min} = 1 + \frac{1}{4kT} \left[ 2\sqrt{v_n^2 i_n^2 - (Im(\overline{v_n i_n^*}))^2} + 2Re(\overline{v_n i_n^*}) \right]$$

$$Z_{opt} = R_{opt} + jX_{opt} = \sqrt{\frac{v_n^2}{i_n^2} - \left( \frac{Im(\overline{v_n i_n^*})}{i_n^2} \right)^2} - j \frac{Im(\overline{v_n i_n^*})}{i_n^2}$$

## 10.7 Simple Transistor Noise Model

$$\begin{aligned}\overline{v_n^2} &= 4kT \left( R + \frac{\gamma}{g_m} (1 + (\omega RC)^2) \right) \\ \overline{i_n^2} &= \frac{4kT\gamma}{g_m} (\omega C)^2 \\ \overline{v_n i_n^*} &= 4kT\gamma g_m \left[ \frac{1 + j\omega CR}{g_m} \right] \left[ \frac{-j\omega C}{g_m} \right]\end{aligned}$$

$$F_{min} \approx 1 + 2\sqrt{\gamma} \frac{\omega}{\omega_T}$$

where  $\omega \ll \omega_T$  and  $\omega_T = \frac{g_m}{C_{gs}}$ .

$$\begin{aligned}X_{opt} &= \frac{1}{\omega C} \\ R_{opt} &= \sqrt{R^2 + \frac{R}{\gamma g_m} \left( \frac{\omega_T}{\omega} \right)^2} \neq R_i + R_G\end{aligned}$$

Noise Resistance:

$$\begin{aligned}R_n &= \frac{\overline{v_n^2}}{4kT} = R + \frac{\gamma}{g_m} (1 + (\omega RC)^2) \\ F &= F_{min} + \frac{4R_n}{Z_0} \frac{|\Gamma_s - \Gamma_{s,opt}|^2}{(1 - |\Gamma_s|^2)|1 + \Gamma_{s,opt}|^2}\end{aligned}$$

## 11 Transmission Lines

Velocity:

$$v = \frac{c}{\epsilon_{eff}} = \frac{1}{\sqrt{LC}}$$

Characteristic Impedance:

$$Z_0 = \sqrt{\frac{L}{C}}$$

Voltage traveling wave (lossless):

$$V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{j\beta z}$$

Phase propagation constant:

$$\beta = \frac{\omega}{v_p} = \frac{2\pi}{\lambda}$$

## 11.1 Reflection Coefficients

Reflection at load:

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Reflection at source:

$$\Gamma_S = \frac{Z_S - Z_0}{Z_S + Z_0}$$

Input impedance:

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l}$$

Power reflection:

$$|\Gamma|^2 = \frac{|Z_{in} - Z_0|^2}{|Z_{in} + Z_0|^2}$$

$$P_r = |\Gamma|^2 P_{AVS}$$

## 11.2 Bounce Diagram

$$v_n^- = v_n^+ \cdot \Gamma_L$$

$$v_{n+1}^+ = v_n^- \cdot \Gamma_S$$

Steady state:

$$V_{ss} = V_0 \frac{R_L}{R_L + R_S}$$

Total voltage:

$$V_{tot} = \sum v_i$$

## 11.3 Lossy Transmission Line

$$V(z) = V_0^+ e^{-\gamma z} = V_0^+ e^{-\alpha z} e^{-j\beta z}$$

## 12 S-Parameters and Smith Chart

### 12.1 S-Parameters

$$\begin{aligned}s_{11} &= \left. \frac{b_1}{a_1} \right|_{a_2=0} = \Gamma_{in} \\ s_{12} &= \left. \frac{b_1}{a_2} \right|_{a_1=0} = \frac{2v_1}{v_s} = \text{reverse gain} \\ s_{21} &= \left. \frac{b_2}{a_1} \right|_{a_2=0} = \frac{2v_2}{v_s} = \text{gain} \\ s_{22} &= \left. \frac{b_2}{a_2} \right|_{a_1=0} = \Gamma_{out}\end{aligned}$$

## 13 Low Noise Amplifier

### 13.1 Conjugate Match

$$\begin{aligned}y_{in} &= y_{11} - \frac{y_{12} \cdot y_{21}}{y_{22} + y_L} = [y_{12} = 0] = y_{11} \\ y_{out} &= y_{22} - \frac{y_{12} \cdot y_{21}}{y_{11} + y_S} = [y_{12} = 0] = y_{22}\end{aligned}$$

Optimal power transfer from source to load:

$$\begin{aligned}y_S &= y_{11}^* \\ y_L &= y_{22}^*\end{aligned}$$

### 13.2 Stubs

Phase propagation constant:

$$\beta = \frac{\omega}{v_p} = \frac{2\pi f \sqrt{\epsilon_r}}{c}$$