



# EITN90 Radar and Remote Sensing

## Lecture 4: Characteristics of Clutter

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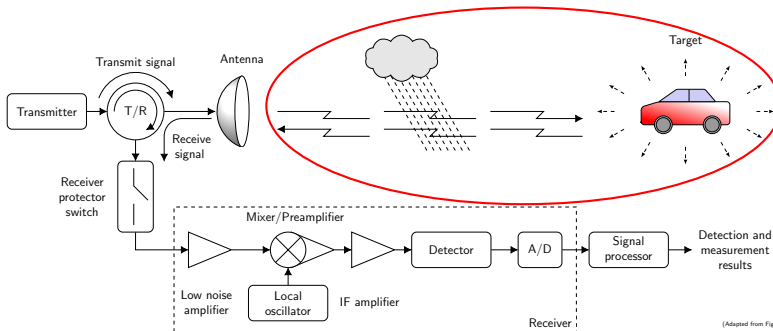
Department of Electrical and Information Technology

- 1 Introduction and definitions**
- 2 General characteristics of clutter**
  - Surface clutter
  - Atmospheric clutter
- 3 Clutter modeling**
  - Surface clutter
  - Atmospheric clutter
  - Summary of clutter results
- 4 Conclusions**
- 5 Lab on Friday**

# Learning outcomes of this lecture

In this lecture we will

- ▶ Characterize the clutter
- ▶ Observe orders of magnitude from different sources
- ▶ Have an initial discussion on clutter suppression
- ▶ See a few empirical models



(Adapted from Fig. 1-1)

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# What is clutter?

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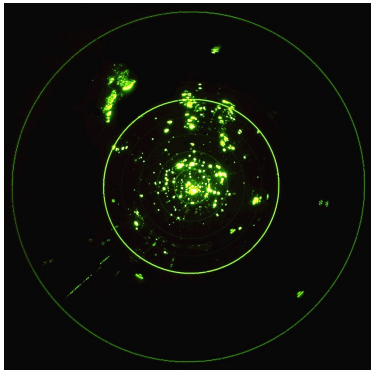
- ▶ Backscattering from natural objects, such as precipitation, vegetation, soil and rocks, or the sea.
- ▶ When trying to detect man-made object, it is considered an unwanted interference, masking the signal.
- ▶ When surveying natural processes (thickness of ice caps, weather etc), it may be the main signal of interest.

## Examples of clutter

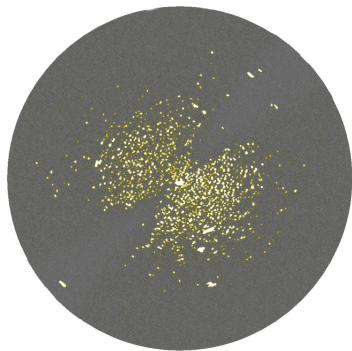
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Images from <http://www.radartutorial.eu/> (CC BY-SA 3.0).

PPI = Plan Position Indicator.



PPI screen of an ATC-radar with targets and clutter.



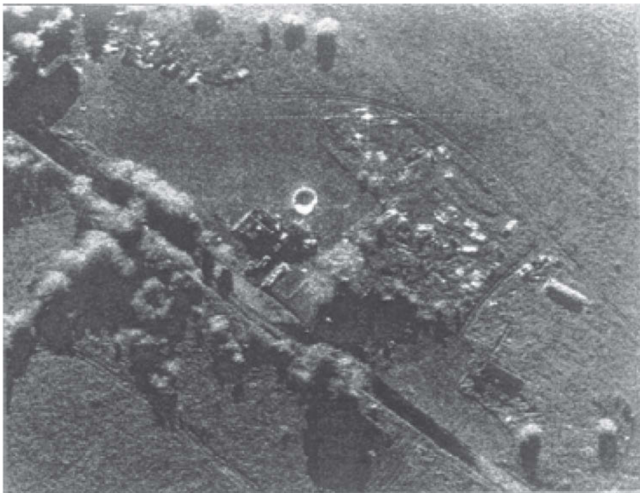
Sea-Clutter on a PPI-Scope.  
Wind from  $310^\circ$  or  $130^\circ$ .

Observing how the image evolves with time gives further information. Clutter can fluctuate and move.

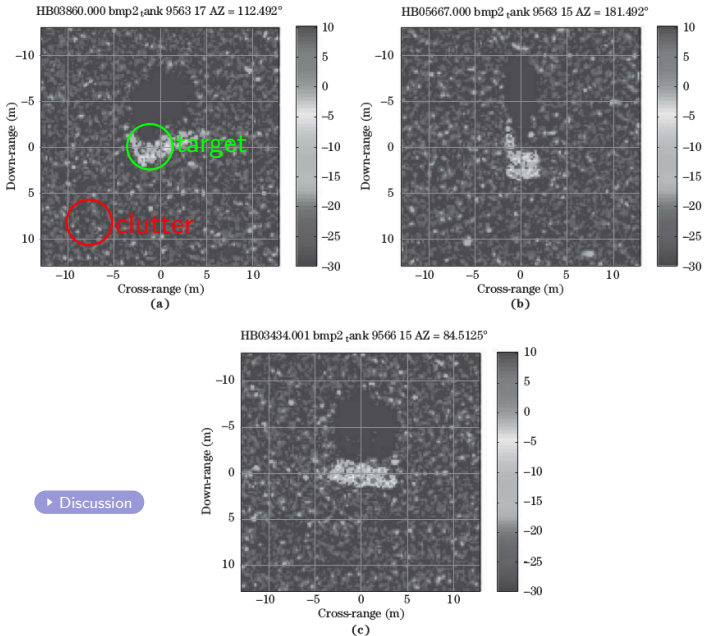
# Radar imaging (35 GHz, 1ft x 1ft res)

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**FIGURE 5-1** ■  
Synthetic aperture  
radar image of  
suburban terrain.  
(From Novak and  
Owirka [1]. With  
permission.)



Mix of areas with uniform scattering (grassy lawns) and non-uniform (trees, man-made structures). May look very different for other frequencies.



**FIGURE 21-32** ■ Three SAR images of an armored vehicle with radar at the bottom of each image and the vehicle (a) at a non-cardinal pose angle, (b) broadside to the radar, and (c) end-on to the radar.



# Clutter vs noise

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There are some significant differences between clutter and noise.

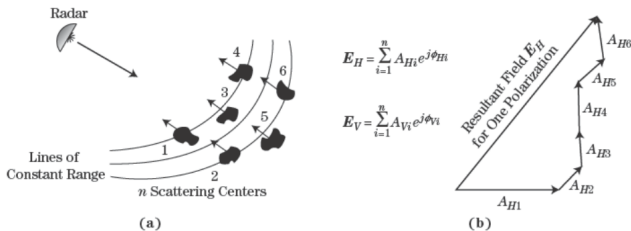
**TABLE 5-1** ■ Clutter Signals versus Noise

Noise Signal	Clutter Signal
Amplitude independent of transmitted radar signal level	Amplitude proportional to transmitted radar signal level
Wide bandwidth (limited by receiver noise bandwidth)	Narrow bandwidth (created by scatterer motion)
Statistically independent between pulses	May be highly correlated between pulses
Amplitude variation described by Rayleigh statistics	Amplitude variation may vary from none to extremely wide (log normal or Weibull statistics)
Average value is constant and independent of spatial position	Time average will differ between spatial samples as the clutter types change
Independent of transmitted frequency	Varies with changing frequency
Independent of environmental parameters	Can vary with changing environmental conditions
No spatial component	Varies with beam position and resolution

Source: Adapted from Long [2]. (© 2006 IEEE. Used with permission.)

# Scattering coefficients

**FIGURE 5-3 ■**  
 Vector summation of scatterers at different positions and ranges.  
 (a) Geometry of multiple scatterers.  
 (b) Vector summation forms resultant E-field amplitude.



The received electric field strength from the  $i$ -th scatterer is proportional to ( $k$  collects factors common to all scatterers)

$$|E_i| \sim \left[ \frac{P_t G^2 \lambda^2 \sigma_i}{(4\pi)^3 L_s R^4} \right]^{1/2} = k \frac{\sqrt{\sigma_i}}{d_i^2}, \quad \arg\{E_i\} = - \left( \theta_i + \frac{4\pi}{\lambda} d_i \right)$$

$$E = \sum_i E_i = \sum_i k \frac{\sqrt{\sigma_i}}{d_i^2} \exp \left[ -j \left( \frac{4\pi}{\lambda} d_i + \theta_i \right) \right] = \frac{k}{d^2} \sqrt{\sigma} e^{j\phi}$$

The complex number  $\sqrt{\sigma} e^{j\phi}$  is the *backscatter coefficient* and  $d$  is the nominal distance to the clutter.

## Clutter polarization scattering matrix

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Taking polarization effects into account, the concept of the backscatter coefficient can be extended to the polarization scattering matrix (PSM).

$$\mathbf{S} = \begin{pmatrix} \sqrt{\sigma_{\text{HH}}}e^{j\phi_{\text{HH}}} & \sqrt{\sigma_{\text{HV}}}e^{j\phi_{\text{HV}}} \\ \sqrt{\sigma_{\text{VH}}}e^{j\phi_{\text{VH}}} & \sqrt{\sigma_{\text{VV}}}e^{j\phi_{\text{VV}}} \end{pmatrix}$$

The PSM could also be expressed in circular polarization (right hand CP and left hand CP). Additional information on the scatterer can be obtained by considering, for instance,

- ▶ Parallel/cross polarization ratio:  $\sqrt{\sigma_{\text{HH}}}/\sqrt{\sigma_{\text{VH}}}$ .
- ▶ Vertical/horizontal polarization ratio:  $\sqrt{\sigma_{\text{VV}}}/\sqrt{\sigma_{\text{HH}}}$ .
- ▶ Polarimetric phase:  $\phi_{\text{HH}} - \phi_{\text{VV}}$ .

These measurements require a radar capable of transmitting and receiving individually in all polarizations, which is expensive.

## Surface and volume reflectivity

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The absolute square of the complex backscatter coefficient  $\sqrt{\sigma}e^{j\phi}$  is the radar cross section  $\sigma$  of the clutter.

To characterize clutter originating from a surface, use the *surface reflectivity*

$$\sigma^0 = \frac{\sigma}{A} \quad [\sigma^0] = \frac{\text{m}^2}{\text{m}^2} = \text{unitless}$$

where  $A$  is the illuminated clutter area.

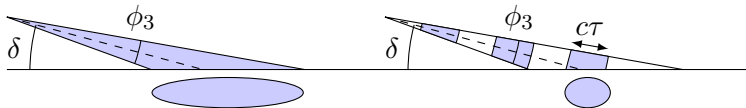
For clutter scatterers in a volume, use the *volume reflectivity*

$$\eta = \frac{\sigma}{V} \quad [\eta] = \frac{\text{m}^2}{\text{m}^3} = \text{m}^{-1}$$

where  $V$  is the illuminated clutter volume.

## Beam limitation vs pulse limitation

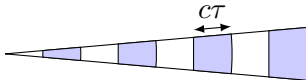
Depending on pulse length  $c\tau$ , the illuminated clutter area is limited by the projected beam or the projected pulse ( $\theta_3$  and  $\phi_3$  are the 3 dB azimuth and elevation beam widths, respectively):



$$A = \frac{\pi R^2 \tan\left(\frac{\theta_3}{2}\right) \tan\left(\frac{\phi_3}{2}\right)}{\sin \delta} \approx \frac{\pi R^2 \theta_3 \phi_3}{4 \sin \delta}$$

$$A = \frac{c\tau R \tan\left(\frac{\theta_3}{2}\right)}{\cos \delta} \approx \frac{c\tau R \theta_3}{2 \cos \delta}$$

The illuminated clutter volume is restricted by the pulse length



$$V = \frac{\pi R^2 \theta_3 \phi_3 c\tau}{4 \cdot 2}$$

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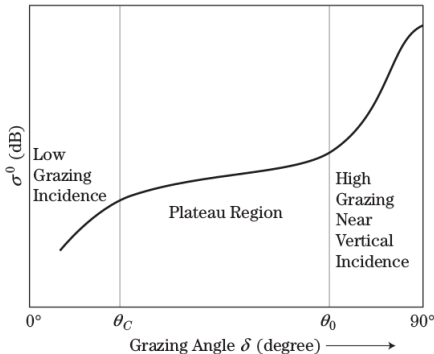
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## Dependence on grazing angle

The surface reflectivity depends on the grazing angle.



**FIGURE 5-4** ■  
General dependence of  $\sigma^0$  on grazing angle. (Adapted from [6]. With permission.)

Based on theory and measured data for land and sea. The behavior at low grazing angles is motivated by the surface becoming smoother (less backscattering). Rayleigh's definition of a smooth surface is

$$\sigma_h \sin \delta < \frac{\lambda}{8}$$



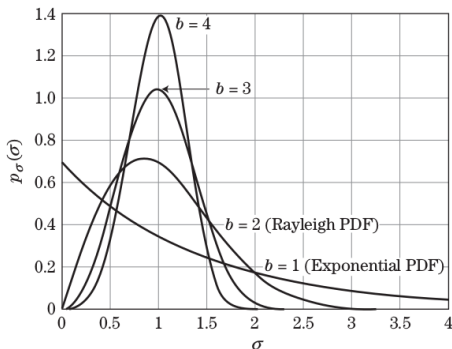
## Random nature of clutter

The clutter response varies with time and space due to motion of the radar or the scatterers, for instance due to wind. A statistical approach is necessary, for instance using the Weibull distribution

$$p_{\sigma} = \begin{cases} \frac{b\sigma^{b-1}}{\alpha} \exp\left(-\frac{\sigma^b}{\alpha}\right) & \sigma \geq 0 \\ 0 & \sigma < 0 \end{cases}$$

where  $\alpha = \sigma_m^b / \ln 2$  and  $\sigma_m$  is the median of the distribution.

**FIGURE 5-7** ■  
Weibull distributions  
for  $\sigma_m = 1$  and  
several values of  $b$ .



# Spatial statistics for ground clutter

**TABLE 5-7** ■ Spatial Statistical Attributes for X-Band Ground Clutter

Terrain Type	Depression Angle (deg)	Weibull Parameters			Ensemble Mean Clutter Strength $\sigma^0$ (dB)	Percent of Samples above Radar Noise Floor	Number of Patches
		$a$	$\sigma_m$ (dB)	$\sigma_w^0$ (dB)			
Rural/ Low-Relief	0.00–0.25	4.8	–60	–33	–32.0	36	413
	0.25–0.50	4.1	–53	–32	–30.7	46	448
	0.50–0.75	3.7	–50	–32	–29.9	55	223
	0.75–1.00	3.4	–46	–31	–28.5	62	128
	1.00–1.25	3.2	–44	–30	–28.5	66	92
	1.25–1.50	2.8	–40	–29	–27.0	69	48
	1.50–4.00	2.2	–34	–27	–25.6	75	75
Rural/ High-Relief	0–1	2.7	–39	–28	–26.7	58	176
	1–2	2.4	–35	–26	–25.9	61	107
	2–3	2.2	–32	–25	–24.1	70	44
	3–4	1.9	–29	–23	–23.3	66	31
	4–5	1.7	–26	–21	–22.2	74	16
	5–6	1.4	–25	–21	–21.5	78	9
	6–8	1.3	–22	–19	–19.1	86	8
Urban	0.00–0.25	5.6	–54	–20	–18.7	57	25
	0.25–0.70	4.3	–42	–19	–17.0	69	31
	0.70–4.00	3.3	–37	–22	–24.0	73	53

$\sigma_m$  = median reflectivity

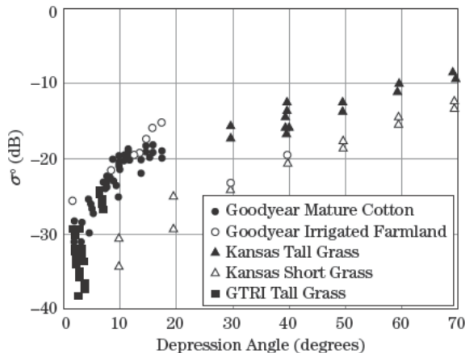
$\sigma_w^0$  = mean reflectivity

$F$  = propagation factor (see Chapter 4)

Source: Adapted from Billingsley [11] (with permission).

Example of how measurements are fitted to theoretical models.

## Land reflectivity: grass and crops

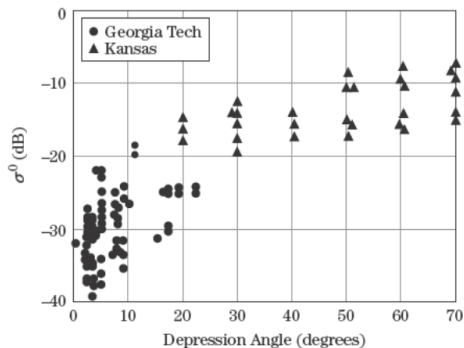


**FIGURE 5-9** ■  $\sigma^0$  data for grass and crops from several sources at X-band. (Data from [16–18]. With permission.)

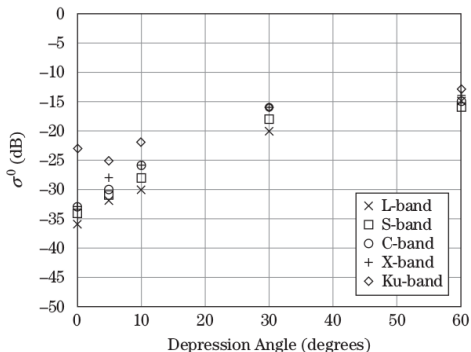
Follows the general trend shown before. Depression angle is an angle relative to the radar system, same as grazing angle for level, horizontal surface. This angle is easier to control in an experiment.

# Land reflectivity: trees

**FIGURE 5-10** ■  $\sigma^0$   
data for trees from  
two sources for  
X-band. (Data from  
[16,18]. With  
permission.)



## Land reflectivity: frequency



**FIGURE 5-12** ■ Averaged reflectivity data for rural farmland as a function of frequency. (Adapted from Nathanson [15]. With permission.)

Higher frequency implies higher reflectivity.

# Sea reflectivity: affecting factors

**TABLE 5-2** ■ Parameters Affecting Sea Return

PARAMETER	COMMENTS
Wave height	Strong proportional dependence
Wind speed	Dependence increases with increasing frequency
Wind/wave look direction	Significant difference between up-wave and down-wave
Polarization	Dependence decreases with increasing frequency
Grazing angle	Strong dependence at low angles, weaker dependence in the plateau region
Frequency band	Proportional to frequency in the microwave region

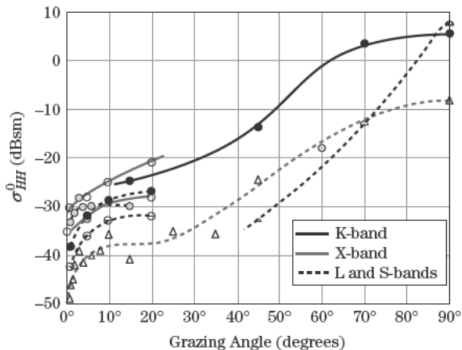
**TABLE 5-3** ■ Douglas Sea State versus Wave Height and Wind Speed for a Fully Developed Sea

Sea State	Significant Wave Height (ft)	Wind Speed (Kts)
0	0 to 0.5	0 to 2
1	0.5 to 1	2 to 7
2	1 to 3	7 to 12
3	3 to 5	12 to 16
4	5 to 8	16 to 20
5	8 to 12	20 to 25
6	12 to 20	25 to 32
7	20 to 40	32 to 45
8	40+	45+

Source: Adapted from Long [6] (with permission).

# Sea reflectivity: measurements

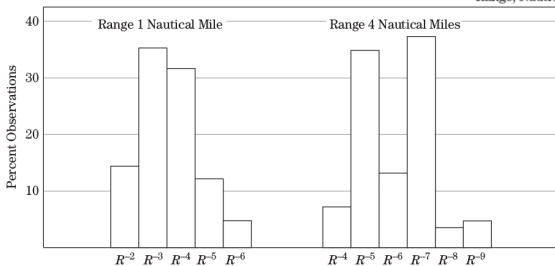
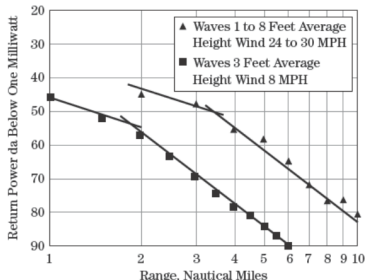
**FIGURE 5-17** ■ Sea return as a function of grazing angle for four radar bands. (From Long [6]. With permission.)



- Wiltse Et Al. [1957] 26 Knot Wind 24 GHz
- Schooley [1956] 30 Knot Wind-upwind 10 GHz
- ◻ Schooley [1956] 30 Knot Wind-downwind 10 GHz
- ◊ Macdonald [1956] 12 Knot Wind 9.3 GHz
- ◌ Campbell [1959] 10-20 Knot Wind 8.8 GHz
- Schooley [1956] 30 Knot Wind-upwind 3 GHz
- ◊ Schooley [1956] 30 Knot Wind-downwind 3 GHz
- △ Macdonald [1956] 30 Knot Wind 1.2 GHz

# Sea reflectivity: range dependence

**FIGURE 5-21 ■**  
Range dependence of sea return for two wave conditions, X-band, HH polarization. (From Dyer and Currie [19]. With permission.)



**FIGURE 5-23 ■**  
Measured range dependencies above and below the critical grazing angle as a percentage of total measurements. (From Dyer and Currie [19]. With permission.)

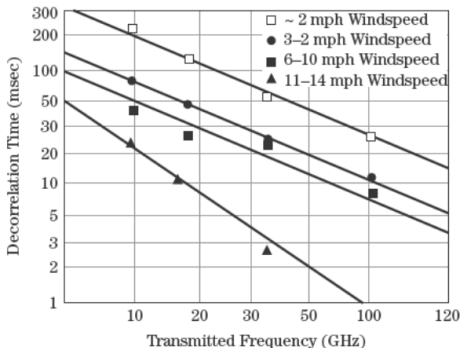
Theoretically, sea clutter should decrease as  $R^{-3}$ , but may decrease faster. [▶ Discussion](#)



## Clutter suppression, decorrelation time

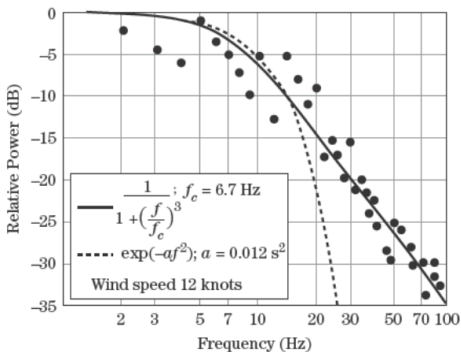
- ▶ The clutter decorrelation time  $\tau_0$ , is the time over which the clutter response is coherent (stable phase and amplitude). This is frequency dependent.
- ▶ If the target signal is stable over longer time than  $\tau_0$ , the signal-to-clutter ratio can be improved by averaging.
- ▶ If  $\text{PRI} > \tau_0$ , each clutter sample is uncorrelated.

**FIGURE 5-27** ■  
Decorrelation time  
for windblown trees  
as a function of wind  
speed. (From Currie  
et al. [21]. With  
permission.)



# Clutter frequency spectra

**FIGURE 5-28** ■  
Spectral data from trees at X-band with Gaussian and power function curve fits.  
(From Fishbein et al. [22]. With permission.)



Theory predicts Gaussian-shaped spectra, but actual measurements often result in a slower roll-off with frequency. This may be due to imperfections in the systems, since a very well-controlled experiment (Billingsley, ref [11]) was well modeled by a Gaussian distribution.

# Outline

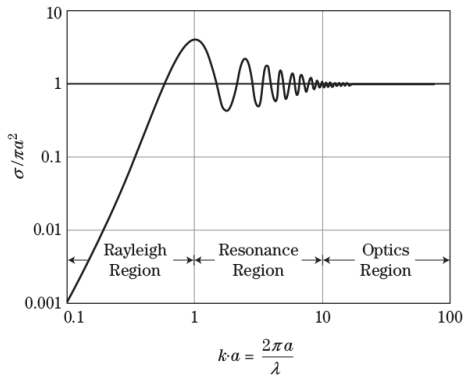
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# Atmospheric clutter

Most volumetric (atmospheric) clutter is due to rain or other precipitation. It depends on rain rate, and the drop-size (typically 0.5–4 mm) in relation to the wavelength  $\lambda$ .

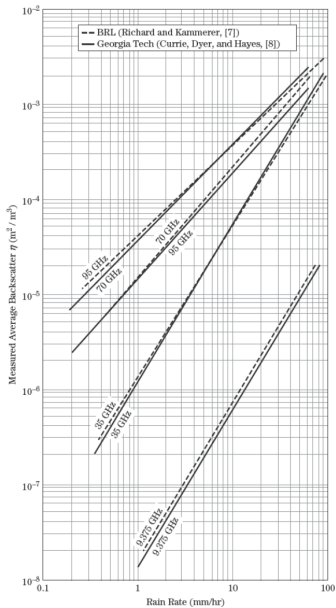
**FIGURE 5-5** ■  
Dependence of the  
RCS of a sphere on  
wavelength.



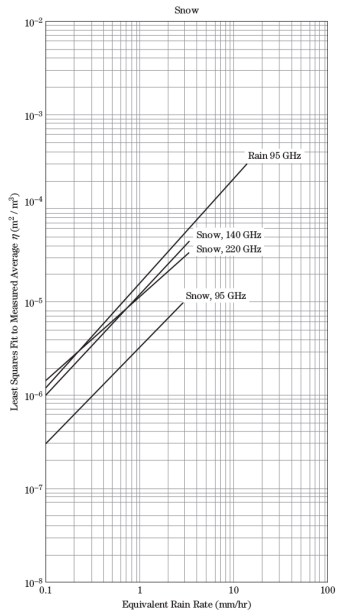
Strongest response around  $ka \approx 1$ , radius  $a \approx \lambda/(2\pi)$ , or a diameter around  $\lambda/3$ .

# Rain data

**FIGURE 5-33** ■  
Least squares fit to  
rain data at four  
frequency bands.  
(From Currie [32].  
With permission.)



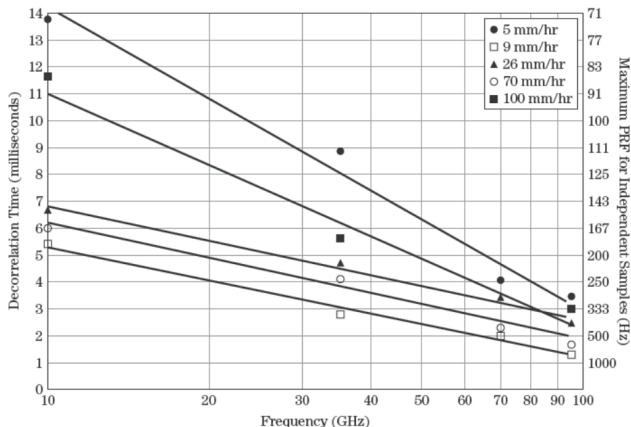
# Snow data



**FIGURE 5-34** ■  
Least squares fit to  
snow data at two  
frequency bands  
compared with rain  
data. (From Currie et  
al. [34]. With  
permission.)

## Rain decorrelation time

**FIGURE 5-35** ■  
Decorrelation time for rain backscatter as a function of frequency. (From Currie et al. [8]. With permission.)



Decorrelation time in the order of milliseconds. This corresponds to a limit for maximum PRF in order to have uncorrelated clutter responses in each pulse ( $\text{PRF}_{\text{max}} = 1/\tau_0$ ).

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## General remarks

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Clutter is notoriously difficult to model, due to the complexity of the real world phenomena it represents. But still, explicit models may provide useful approximations when evaluating the radar scenario.

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## GTRI empirical model

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The following model was developed in the late 1970's by GTRI = Georgia Tech Research Institute.

$$\sigma^0 = A(\delta + C)^B \exp \left[ \frac{-D}{1 + \frac{0.1\sigma_h}{\lambda}} \right]$$

- ▶  $\delta$  is the grazing angle in radians
- ▶  $\sigma_h$  is the rms surface roughness
- ▶  $\lambda$  is the wavelength
- ▶  $A$ ,  $B$ ,  $C$ , and  $D$  are empirically derived constants

▶ Discussion

# GTRI coefficients

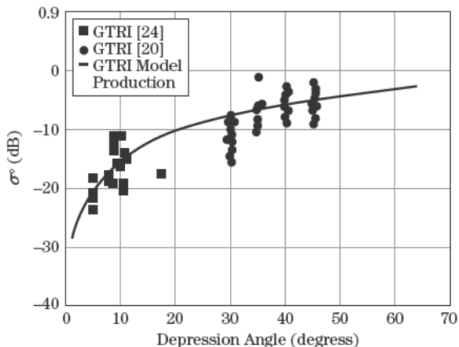
**TABLE 5-10** ■ Coefficients for GTRI Empirical Model

Constant	Frequency	Soil/ Sand	Grass	Tall Grass Crops	Trees	Urban	Wet Snow	Dry Snow
<i>A</i>	3	0.0045	0.0071	0.0071	0.00054	0.362	—	—
	5	0.0096	0.015	0.015	0.0012	0.779	—	—
	10	0.25	0.023	0.006	0.002	2.0	0.0246	0.195
	15	0.05	0.079	0.079	0.019	2.0	—	—
	35	—	0.125	0.301	0.036	—	0.195	2.45
	95	—	—	—	3.6	—	1.138	3.6
<i>B</i>	3	0.83	1.5	1.5	0.64	1.8	—	—
	5	0.83	1.5	1.5	0.64	1.8	—	—
	10	0.83	1.5	1.5	0.64	1.8	1.7	1.7
	15	0.83	1.5	1.5	0.64	1.8	—	—
	35	—	1.5	1.5	0.64	—	1.7	1.7
	95	—	1.5	1.5	0.64	—	0.83	0.83
<i>C</i>	3	0.0013	0.012	0.012	0.002	0.015	—	—
	5	0.0013	0.012	0.012	0.002	0.015	—	—
	10	0.0013	0.012	0.012	0.002	0.015	0.0016	0.0016
	15	0.0013	0.012	0.012	0.002	0.015	—	—
	35	—	0.012	0.012	0.012	—	0.008	0.0016
	95	—	0.012	0.012	0.012	—	0.008	0.0016
<i>D</i>	3	2.3	0.0	0.0	0.0	0.0	—	—
	5	2.3	0.0	0.0	0.0	0.0	—	—
	10	2.3	0.0	0.0	0.0	0.0	0.0	0.0
	15	2.3	0.0	0.0	0.0	0.0	—	—
	35	—	0.0	0.0	0.0	—	0.0	0.0
	95	—	0.0	0.0	0.0	—	0.0	0.0

Source: From Currie [32] (with permission).

# Comparison of GTRI model with measured data

**FIGURE 5-38 ■**  
Comparison of GTRI  
model output with  
data for deciduous  
trees at X-band.  
(From Currie [32].  
With permission.)



# GTRI sea clutter model

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**TABLE 5-11** ■ GTRI Sea Clutter Model Equations

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$$\sigma_{HH}^0 = 10 \log[3.9 \times 10^{-6} \lambda \delta^{0.4} A_i A_u A_w]$$

For 1 to 3 GHz

$$\sigma_{VV}^0 = \sigma_{HH}^0 - 1.73 \ln(h_{av} + 0.015) + 3.76 \ln(\lambda) + 2.46 \ln(\delta + 0.0001) + 22.2$$

For 3 to 10 GHz

$$\sigma_{VV}^0 = \sigma_{HH}^0 - 1.05 \ln(h_{av} + 0.015) + 1.09 \ln(\lambda) + 1.27 \ln(\delta + 0.0001) + 9.70$$

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$$\sigma_\phi = (14.4\lambda + 5.5)\delta h_{av}/\lambda$$

$$A_i = \sigma_\phi^4 / (1 + \sigma_\phi^4)$$

$$A_u = \exp [0.2 \cos \phi (1 - 2.8\delta)(\lambda + 0.015)^{-0.4}]$$

$$q_w = 1.1 / (\lambda + 0.015)^{0.4}$$

$$V_w = 8.67 h_{av}^{0.4}$$

$$A_w = [1.94 V_w / (1 + V_w / 15.4)]^{q_w}$$

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Note: Values for  $h_{av}$  and  $\lambda$  are given in meters,  $\delta$  and  $\phi$  are in radians.

Source: From Horst et al. [39] (with permission).

# Outline

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- 1 Introduction and definitions
- 2 General characteristics of clutter
  - Surface clutter
  - Atmospheric clutter
- 3 Clutter modeling**
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## Rain clutter

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The model parameters  $A$  and  $B$  below can be fitted to the rain data in Figure 5-33 (where  $R$  is the rain rate in mm/hr):

$$\eta = AR^B [\text{m}^{-1}]$$

**TABLE 5-12** ■ Model Coefficients for Rain

Frequency (GHz)	$A$	$B$
9.4	$1.3 \times 10^{-8}$	1.6
35	$1.2 \times 10^{-6}$	1.6
70	$4.2 \times 10^{-5}$	1.1
95	$1.5 \times 10^{-5}$	1.0

*Source:* From Currie et al. [34] (with permission).



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# Land reflectivity

**TABLE 5-13** ■ Summary of Averaged Land Reflectivity ( $\sigma^0$  in db)

Clutter Type	Frequency Band	Grazing Angle (Deg.)			
		1.5	10	30	60
Desert	L	-45	-38	-28	-21
	S	-46	-36	-25	-17
	C	-40	-33	-23	-16
	X	-40	-30	-21	-14
	K <sub>u</sub>		-28	-19	-13
Farmland	L	-36	-30	-20	-15
	S	-34	-28	-18	-16
	C	-33	-26	-16	-15
	X	-33	-26	-16	-14
	K <sub>u</sub>	-23	-22	-16	-13
Woods	L	-28	-26	-18	-19
	S	-28	-24	-16	-15
	C	-27	-23	-16	-15
	X	-26	-23	-14	-14
	K <sub>u</sub>	-13	-20	-14	-12
Urban	L	-25	-18	-15	-12
	S	-23	-18	-13	-11
	C	-21	-18	-11	-10
	X	-20	-16	-10	-10
	K <sub>u</sub>				

# Sea reflectivity

**TABLE 5-14** ■ Summary of Averaged Sea Reflectivity ( $\sigma^0$  in db)

Sea State	Frequency Band	Polarization	Grazing Angle (Deg.)			
			0.1	10	30	60
1	L	VV		-39	-38	-22
	L	HH		-56	-46	-24
	S	VV	-80	-40	-40	-24
	S	HH	-80			-25
	C	VV	-72	-41	-42	-24
	C	HH	-75	-53	-48	-26
	X	VV	-65	-42	-36	-24
	X	HH	-71	-51	-44	-24
	K <sub>u</sub>	VV		-40	-31	-20
	K <sub>u</sub>	HH			-38	-20
	3	L	VV	-82	-34	-30
L		HH	-82	-48	-39	-20
S		VV	-75	-34	-29	-19
S		HH	-68	-46	-38	-20
C		VV	-60	-34	-28	-18
C		HH	-69	-40	-37	-20
X		VV	-51	-32	-26	-16
X		HH	-53	-37	-34	-21
K <sub>u</sub>		VV		-31	-23	-14
K <sub>u</sub>		HH		-32	-28	-16

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# Conclusions

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- ▶ Characterization of clutter: backscatter coefficient, surface reflectivity  $\sigma^0$ , volume reflectivity  $\eta$ .
- ▶ Illuminated area/volume determines the clutter RCS.
- ▶ Clutter decorrelation time needs to be considered for clutter suppression.
- ▶ Some empirical models exist for estimating the reflectivity for different contexts.

# Outline

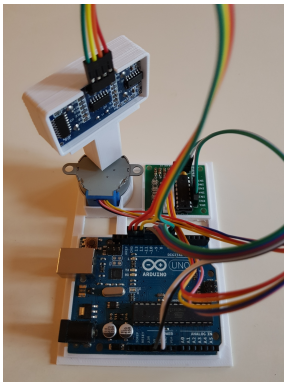
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## About the lab

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- ▶ The lab will take place in the same room as the exercises.  
**Note the time: 8–12!**
- ▶ The lab is based around a simple ultrasonic sensor placed on a stepper motor, controlled by an Arduino unit.
- ▶ **Read the lab instructions carefully before the lab!** They are available on the course web site, under “Lectures”.



## A practical problem: interference!

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Since several units will be operating at the same time, they may interfere with each other, meaning one unit may receive both its own echo (intended) and the direct signal of another unit (not intended).

- ▶ We can use two rooms in order to reduce problems.
- ▶ In each room, make sure to spread out, and try not to point your radar in the direction of others (remember signals will also reflect in walls, but the range is only a couple of meters).

The lab is done in pairs of two. Ask your lab leader Sebastian if you get strange results, or if there are any other questions.

**Before you leave the lab, demonstrate your findings to the lab leader in order to be approved on the lab!**



# Discussion

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Why is there a shadow behind the targets?

◀ Go back

# Discussion

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Why is there a shadow behind the targets?

Answer:

- ▶ Only diffracted signals reach what is directly behind the targets, leading to significantly reduced illumination and less clutter.

[◀ Go back](#)

# Discussion

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Why is the pulse limited volume estimated with a range of  $c\tau/2$  rather than  $c\tau$ ?

◀ Go back

## Discussion

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Why is the pulse limited volume estimated with a range of  $c\tau/2$  rather than  $c\tau$ ?

Answer:

- ▶ This is the range when the last reflection of the initial pulse overlaps with the first reflection of the end of the pulse.

[◀ Go back](#)

## Discussion

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Give a suggestion why sea clutter tends to decay slower than anticipated by theory. (No uniquely true answer!)

◀ Go back

## Discussion

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Give a suggestion why sea clutter tends to decay slower than anticipated by theory. (No uniquely true answer!)

Answer:

- ▶ The book suggests a ducting phenomenon, with waves trapped close to sea surface, leading to a slower decay of the excitation of clutter. Open case!

◀ Go back

## Discussion

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In the expression (where  $\delta$  is the grazing angle,  $\sigma_h$  is the rms surface roughness, and  $\lambda$  is the wavelength)

$$\sigma^0 = A(\delta + C)^B \exp \left[ \frac{-D}{1 + \frac{0.1\sigma_h}{\lambda}} \right]$$

which parameters  $A$ ,  $B$ ,  $C$ , or  $D$  would you say have the strongest connection to angle of incidence and surface roughness?

## Discussion

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In the expression (where  $\delta$  is the grazing angle,  $\sigma_h$  is the rms surface roughness, and  $\lambda$  is the wavelength)

$$\sigma^0 = A(\delta + C)^B \exp \left[ \frac{-D}{1 + \frac{0.1\sigma_h}{\lambda}} \right]$$

which parameters  $A$ ,  $B$ ,  $C$ , or  $D$  would you say have the strongest connection to angle of incidence and surface roughness?

Answer:

- ▶  $C$  (and to some extent  $B$ ) gives an offset to the angle of incidence, and  $D$  gives a weighting to the surface roughness.