

EITG05 – Digital Communications

Lecture 4

Bandwidth of Transmitted Signals

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Fourier transform

$$\begin{aligned} X(f) &= \mathcal{F}\{x(t)\} = \int_{-\infty}^{\infty} x(t) \ e^{-j2\pi f t} \ dt \\ &= X_{Re}(f) + j \ X_{Im}(f) \\ &= |X(f)| \ e^{j \ \varphi(f)} \end{aligned}$$

$$\begin{aligned} x(t) &= \mathcal{F}^{-1}\{X(f)\} = \int_{-\infty}^{\infty} X(f) \ e^{+j2\pi f t} \ df \\ &= \int_{-\infty}^{\infty} |X(f)| \ e^{+j(2\pi f t + \varphi(f))} \ df \end{aligned}$$



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Some useful Fourier transform properties

$$\begin{array}{rcl} g(at) &\leftrightarrow & \frac{1}{|a|} \ G(f/a) & g^*(T-t) &\leftrightarrow \ G^*(f)e^{-j2\pi fT} \\ g(-t) &\leftrightarrow \ G(-f) & \delta(t) &\leftrightarrow \ 1 \\ G(t) &\leftrightarrow \ g(-f) & 1(dc) &\leftrightarrow \ \delta(f) \\ g(t-t_0) &\leftrightarrow \ G(f)e^{-j2\pi ft_0} & e^{j2\pi f_c t} &\leftrightarrow \ \delta(f-f_c) \\ g(t)e^{j2\pi f_c t} &\leftrightarrow \ G(f-f_c) & \cos(2\pi f_c t) &\leftrightarrow \ \frac{1}{2} \ (\delta(f+f_c)+\delta(f-f_c)) \\ \frac{d}{dt} \ g(t) &\leftrightarrow \ j2\pi f \ G(f) & \sin(2\pi f_c t) &\leftrightarrow \ \frac{j}{2} \ (\delta(f+f_c)-\delta(f-f_c)) \\ g^*(t) &\leftrightarrow \ G^*(-f) & \alpha e^{-\pi \alpha^2 t^2} &\leftrightarrow \ e^{-\pi f^2/\alpha^2} \end{array}$$

\rightarrow full list in Appendix C of the compendium



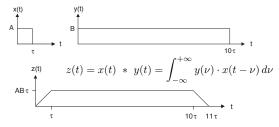
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Some useful Fourier transform properties

• Consider two signals x(t) and y(t) and their Fourier transforms

$$x(t) \longleftrightarrow X(f)$$
, $y(t) \longleftrightarrow Y(f)$

• Recall the convolution operation z(t) = x(t) * y(t):



Filtering:

$$x(t) \ \ast \ y(t) \ \longleftrightarrow \ X(f) \cdot Y(f)$$

Multiplication:

$$x(t) \cdot y(t) \longleftrightarrow X(f) * Y(f)$$



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Spectrum of time-limited signals

- ► Consider some time-limited signal $s_T(t)$ of duration T, with $s_T(t) = 0$ for t < 0 and t > T
- ► Assume that within the interval $0 \le t \le T$, the signal $s_T(t)$ is equal to some signal s(t), i.e.,

$$s_T(t) = s(t) \cdot g_{rec}(t) ,$$

where $g_{rec}(t)$ is the rectangular pulse of amplitude A = 1

Taking the Fourier transform on both sides we get

$$S_T(f) = S(f) * G_{rec}(f) = S(f) * AT \frac{\sin(\pi f T)}{\pi f T} e^{-j\pi f T}$$

► Since G_{rec}(f) is unlimited along the frequency axis, this is the case for S_T(f) as well (convolution increases length)

Time-limited signals can never be strictly band-limited



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Some definitions of bandwidth

Main-lobe definition:

 W_{lobe} is defined by the width of the main-lobe of R(f)This is how we have defined bandwidth in previous examples

- In baseband we use the one-sided width, while in bandpass applications the two-sided width is used (positive frequencies)
- Percentage definition:

W₉₉ is defined according to the location of 99% of the power

▶ For bandpass signals W₉₉ is found as the value that satisfies

$$\int_{f_c - W_{99}/2}^{f_c + W_{99}/2} R(f) \, df = 0.99 \, \int_0^\infty R(f) \, df$$

- Other percentages can be used as well: W₉₀, W_{99.9}
- Nyquist bandwidth

Assuming an ideal pulse with finite bandwidth (see Chapter 6)

$$W_{nyq} = \frac{R_s}{2} [\text{Hz}]$$



Some definitions of bandwidth

Pulse shape	W_{lobe}	% power	W_{90}	W_{99}	$W_{99.9}$	Asymptotic
		in W_{lobe}				decay
rec	2/T	90.3	1.70/T	20.6/T	204/T	f^{-2}
tri	4/T	99.7	1.70/T	2.60/T	6.24/T	f^{-4}
hcs	3/T	99.5	1.56/T	2.36/T	5.48/T	f^{-4}
rc	4/T	99.95	1.90/T	2.82/T	3.46/T	f^{-6}
Nyquist	R_s	100	$0.9R_s$	$0.99R_{s}$	$0.999R_{s}$	ideal

Table 2.1: Double-sided bandwidth results for power spectral densities according to (2.212). The $g_{rec}(t)$, $g_{tri}(t)$, $g_{hcs}(t)$ and $g_{rc}(t)$ pulse shapes are defined in Appendix D, and T denotes the duration of the pulse. The Nyquist pulse shape is not limited in time and it is defined in (D.49) with parameters $\beta = 0$ and $\mathcal{T} = T_s$.

- This table is useful for PAM, PSK, and QAM constellations
- Except bandwidth W, the asymptotic decay is also relevant



Pulse spectrum examples

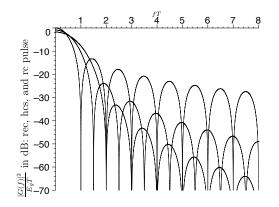


Figure 2.19: $10 \log_{10} \left(\frac{|G(f)|^2}{E_g T} \right)$ for the $g_{rec}(t)$, $g_{hcs}(t)$, and $g_{rc}(t)$ pulse shapes. See also Example 2.26.

From last lecture: R(f) for Binary Signaling

▶ In the general binary case, i.e., M = 2, we have

$$A(f) = P_0 S_0(f) + P_1 S_1(f)$$

This simplifies the expression for the power spectral density to

$$R(f) = R_c(f) + R_d(f)$$

= $\frac{P_0 P_1}{T_b} |S_0(f) - S_1(f)|^2 + \frac{|P_0 S_0(f) + P_1 S_1(f)|^2}{T_b^2} \sum_{n = -\infty}^{\infty} \delta(f - n/T_b)$

(derivation in Ex. 2.20)

We will now consider some examples from the compendium



Assume equally likely antipodal signal alternatives, such that

$$s_1(t) = -s_0(t) = g(t)$$

where $g(t) = g_{rec}(t)$, and $g_{rec}(t)$ is given in (D.1). Assume also that $T \leq T_b$.

- i) Calculate the power spectral density R(f).
- ii) Calculate the bandwidth W defined as the one-sided width of the mainlobe of R(f), if the information bit rate is 10 [kbps], and if T = T_b/2. Calculate also the bandwidth efficiency ρ.
- iii) Estimate the attenuation in dB of the first sidelobe of R(f) compared to R(0).
- ▶ M = 2 with equally likely antipodal signaling $s_1(t) = -s_0(t) = g(t)$
- ▶ With $P_0 = P_1 = 1/2$ and $S_1(f) = -S_0(f) = G(f)$ we get

$$R(f) = R_b |S_1(f)|^2 = R_b |S_0(f)|^2 = R_b |G(f)|^2$$

Details for the pulse in Appendix D



Assume equally likely antipodal signal alternatives below. Assume that $s_1(t) = -s_0(t) = g_{rc}(t)$, where the time raised cosine pulse $g_{rc}(t)$ is defined in (D.18). Assume also that $T = T_b$.

Find an expression for the power spectral density R(f). Calculate the bandwidth W, defined as the one-sided width of the mainlobe of R(f), if R_b is 10 [kbps]. Calculate also the bandwidth efficiency ρ .

- Same as Example 2.21, but with $g_{rc}(t)$ pulse
- Analogously we get

$$R(f) = R_b |G_{rc}(f)|^2$$

From the one-sided main-lobe we get

$$W = 2/T$$
 [Hz]

Bandwidth efficiency ρ = 1/2 [bps/Hz] is the same (why?)



Assume $P_0 = P_1$ and that,

 $s_1(t) = -s_0(t) = g_{rc}(t)\cos(2\pi f_c t)$

with $T = T_b$, and $f_c \gg 1/T$. Hence, a version of binary PSK signaling is considered here (alternatively binary antipodal bandpass PAM). Calculate the bandwidth W, defined as the double-sided width of the mainlobe around the carrier frequency f_c . Assume that the information bit rate is 10 [kbps]. Calculate also the bandwidth

- This corresponds to the bandpass case
- ▶ Let *g*_{hf}(*t*) denote the high-frequency pulse

$$g_{hf}(t) = g_{rc}(t)\cos(2\pi f_c t)$$
 and $R(f) = R_b |G_{hf}(f)|^2$

Using shift operations we get

$$R(f) = R_b \left| \frac{G_{rc}(f+f_c)}{2} + \frac{G_{rc}(f-f_c)}{2} \right|^2$$

From the two-sided main-lobe we get

$$W = 4/T [Hz]$$



Example: discrete frequencies in R(f)

- Assume M = 2
- Let $s_0(t) = 0$ and $s_1(t) = 5$ with a pulse duration $T = T_b/2$
- With this the average signal becomes

$$a(t) = \frac{s_0(t) + s_1(t)}{2} = 2.5$$
, $0 \le t \le T$

We can then write (within the pulse duration T)

$$s_0(t) = -2.5 + a(t)$$
, $s_1(t) = +2.5 + a(t)$

Observe:

- **1.** this method is a waste of signal energy since a(t) does not carry any information
- repetition of *a*(*t*) in every symbol interval creates some periodic signal component in the time domain, which leads to discrete frequencies in the frequency domain



From last lecture: general R(f)

► The power spectral density R(f) can be divided into a continuous part R_c(f) and a discrete part R_d(f)

 $R(f) = R_c(f) + R_d(f)$

The general expression for the continuous part is

$$R_{c}(f) = \frac{1}{T_{s}} \sum_{n=0}^{M-1} P_{n} |S_{n}(f) - A(f)|^{2}$$
$$= \left(\frac{1}{T_{s}} \sum_{n=0}^{M-1} P_{n} |S_{n}(f)|^{2}\right) - \frac{|A(f)|^{2}}{T_{s}}$$

For the discrete part we have

$$R_d(f) = \frac{|A(f)|^2}{T_s^2} \sum_{n=-\infty}^{\infty} \delta(f - n/T_s)$$



R(*f*): *M*-ary PAM signals

With M-ary PAM signaling we have

$$s_{\ell} = A_{\ell} g(t) , \quad \ell = 0, 1, \dots, M-1$$

Then

$$S_{\ell}(f) = A_{\ell} G(f)$$
, and $A(f) = \sum_{\ell=0}^{M-1} P_{\ell} A_{\ell} G(f)$

With this we obtain the simplified expression

$$R(f) = \frac{\sigma_A^2}{T_s} |G(f)|^2 + \frac{m_A^2}{T_s^2} |G(f)|^2 \sum_{n=-\infty}^{\infty} \delta(f - n/T_s) ,$$

where m_A denotes the mean and $\sigma_A^2 = \overline{E}_s / E_g - m_A^2$ the variance of the amplitudes A_ℓ

► Assuming zero average amplitude $m_A = 0$ and using $\overline{P} = \sigma_A^2 E_g R_s$ this reduces to

$$R(f) = R_c(f) = \frac{\sigma_A^2}{T_s} |G(f)|^2 = \frac{\overline{P}}{E_g} |G(f)|^2$$



Assume the bit rate $R_b = 9600$ [bps], M-ary PAM transmission and that $m_A = 0$. Determine the (baseband) bandwidth W, defined as the one-sided width of the mainlobe of the power spectral density R(f), if M = 2, M = 4 and M = 8, respectively. Furthermore, assume a rectangular pulse shape with amplitude A_g , and duration $T = T_s$. Calculate also the bandwidth efficiency ρ .

- What is W for a given pulse shape and different M?
- Using $T = T_s$, $m_A = 0$ and $g(t) = g_{rec}(t)$, we have

$$R(f) = \frac{\sigma_A^2}{T_s} |G_{rec}(f)|^2$$

For the given pulse we get $W = 1/T_s$, where $T_s = k T_b$

k = 1	\Rightarrow	M = 2	\Rightarrow	W = 9600[Hz]
k = 2	\Rightarrow	M = 4	\Rightarrow	W = 4800[Hz]
k = 3	\Rightarrow	M = 8	\Rightarrow	W = 3200 [Hz]

► Bandwidth efficiency: $\rho = R_b/W = k T_b/T_b = k$



What does bandwidth efficiency tell us?

In the previous example we had a bandwidth efficiency of

$$\rho = \frac{R_b}{W} = k$$

Saving bandwidth

- ► The previous example showed that the bandwidth *W* can be reduced by increasing *M*
- $T = T_s = k T_b$ increases with M
- $W = 1/T = R_b/k$ decreases accordingly

Improving bit rate

- Assume instead that the bandwidth W is fixed in the same example, i.e., the symbol duration $T_s = T$ is fixed
- Then $R_b = k W$ increases with M
- Assume for example W = 1 MHz:

$$R_b = 1$$
 Mbps if $M = 2$ ($k = 1$)

$$R_b = 10 \text{ Mbps if } M = 1024 \ (k = 10)$$

R(f): *M*-ary QAM signals

With M-ary QAM signaling the signal alternatives are

$$s_{\ell}(t) = A_{\ell} g(t) \cos(2\pi f_c t) - B_{\ell} g(t) \sin(2\pi f_c t), \quad \ell = 0, 1, \dots, M - 1$$

Then the Fourier transform becomes

$$S_{\ell}(f) = A_{\ell} \frac{G(f+f_c) + G(f-f_c)}{2} - j B_{\ell} \frac{G(f+f_c) - G(f-f_c)}{2}$$
$$= (A_{\ell} - jB_{\ell}) \frac{G(f+f_c)}{2} + (A_{\ell} + jB_{\ell}) \frac{G(f-f_c)}{2}$$

► Assuming a zero average signal a(t) = 0 and f_c T ≥ 1 this simplifies to

$$R(f) = R_c(f) = \overline{P} \; \frac{|G(f+f_c)|^2 + |G(f-f_c)|^2}{2E_g}$$



R(f): *M*-ary QAM signals

Remember that *M*-ary QAM signals contain *M*-ary PSK and *M*-ary bandpass PAM signals as special cases:

> BP-PAM: $B_{\ell} = 0$ PSK: $A_{\ell} = \cos(v_{\ell})$, $B_{\ell} = \sin(v_{\ell})$

- ▶ \Rightarrow our results for R(f) of *M*-ary QAM signals include these cases
- ► For symmetric constellations, such that *a*(*t*) = 0, the simplified version applies
- ► The bandwidth *W* is determined by $|G(f f_c)|^2$ and hence the two-sided main-lobe of $|G(f)|^2$

 \Rightarrow if the same pulse g(t) is used then *M*-ary QAM, *M*-ary bandpass PAM and *M*-ary PSK have the same bandwidth *W*



Example

Bandwidth consumption for BPSK, QPSK and 16-QAM assuming equal R_b and $f_c = 100R_b$

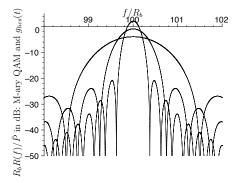


Figure 2.20: The power spectral density for binary QAM (BPSK, widest mainlobe), 4-ary QAM (QPSK), and 16-ary QAM (smallest mainlobe). The figure shows $10 \log_{10}(R_b R(f)/\bar{P})$ [dB] in the frequency interval $98R_b \leq f \leq 102R_b$. The carrier frequency is $f_c = 100R_b$ [Hz], and a $T_s = kT_b \log g_{hcs}(t)$ pulse is assumed. See also (2.227) and (2.230).



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R(*f*): *M*-ary FSK signals

With *M*-ary frequency shift keying (FSK) signaling the signal alternatives are

$$s_{\ell}(t) = A \cos(2\pi f_{\ell} t + v), \quad 0 \le t \le T_s$$

• Choosing $v = -\pi/2$ this can be written as

 $s_\ell(t) = g_{rec}(t) \sin(2\pi f_\ell t)$, with $T = T_s$,

since $s_{\ell}(t) = 0$ outside the symbol interval

The Fourier transform is then

$$S_{\ell}(f) = j \; \frac{G_{rec}(f+f_{\ell}) - G_{rec}(f-f_{\ell})}{2}$$

The exact power spectral density R(f) can now be computed by the general formula (2.202)–(2.204)

R(*f*): *M*-ary FSK signals

- Let us find an approximate expression for the FSK bandwidth W
- Assume that

$$f_{\ell} = f_0 + \ell f_{\Delta}, \quad \ell = 0, \dots, M - 1$$

Then the bandwidth W can be approximated by

$$W \approx R_s + f_{M-1} - f_0 + R_s = (M-1)f_{\Delta} + 2R_s$$

- Consider now orthogonal FSK with $f_{\Delta} = I \cdot R_s/2$ for some I > 0
- The bandwidth efficiency is then

$$\rho = \frac{R_b}{W} \approx \frac{R_b}{(M-1)f_{\Delta} + 2R_s} = \frac{R_b}{((M-1)I/2 + 2)R_s} = \frac{\log_2 M}{(M-1)I/2 + 2}$$

Observe: the bandwidth efficiency of orthogonal *M*-ary FSK gets small if *M* is large Last week we saw: *M*-ary FSK has good energy and Euclidean distance properties \Rightarrow trade-off

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Assume that orthogonal M-ary FSK is used to communicate digital information in the frequency band $1.1 \le f \le 1.2$ [MHz].

For each M below, find the largest bit rate that can be used (use bandwidth approximations):

i) M = 2 ii) M = 4 iii) M = 8 iv) M = 16 v) M = 32

Which of the M-values above give a higher bit rate than the M = 2 case?

Solution:

It is given that $W_{M-FSK} = 100$ [kHz]. From (2.245), the largest bit rate is obtained with I = 1:

$$R_b \approx 10^5 \cdot \frac{\log_2(M)}{(M-1)/2 + 2}$$

M	$\frac{\log_2(M)}{(M-1)/2+2}$	R_b
2	$\frac{1}{5/2} = 0.4$	40 kbps
4	$\frac{2}{7/2} = \frac{4}{7} \approx 0.5714$	$\approx 57~{\rm kbps}$
8	$\frac{3}{11/2} = \frac{6}{11} \approx 0.5455$	$\approx 55~{\rm kbps}$
16	$\frac{4}{19/2} = \frac{8}{19} \approx 0.4211$	$\approx 42~{\rm kbps}$
32	$\frac{5}{35/2} = \frac{10}{35} \approx 0.2857$	$\approx 29~{\rm kbps}$

From this table it is seen that M = 4, 8, 16 give a higher bit rate than M = 2.



R(*f*): **OFDM-type signals**

An OFDM symbol (signal alternative) x(t) can be modeled as a superposition of N orthogonal QAM signals, each carrying k_n bits, that are transmitted at different frequencies (sub-carriers)

$$x(t) = \sum_{n=0}^{N-1} s_{n,QAM}(t)$$

Assuming each QAM signal has zero mean and that the different carriers have independent bit streams we get

$$R(f) = R_c(f) = R_s E\{|X(f)|^2\} = \sum_{n=0}^{N-1} R_n(f)$$

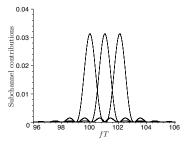
Using our previous results for QAM in each sub-carrier we get

$$R(f) = R_c(f) = \sum_{n=0}^{N-1} \overline{P} \; \frac{|G(f+f_c)|^2 + |G(f-f_c)|^2}{2E_g}$$



R(*f*): **OFDM-type signals**

Illustration of $R_n(f)$ contributed by three neighboring sub-carriers:



• Assuming $f_n = f_0 + n/(T_s - \Delta_h)$ we can estimate the bandwidth as

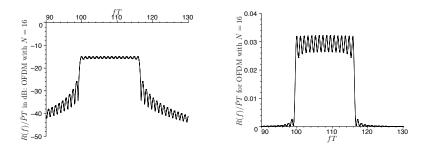
$$W \approx (N+1) f_{\Delta} = \frac{N+1}{1 - \Delta_h/T_s} R_s \approx N \cdot R_s , \quad N \gg 1 , \Delta_h \ll T_s$$

The bandwidth efficiency is then approximated by

$$\rho = \frac{R_b}{W} = \frac{R_s}{W} \sum_{k=0}^{N-1} k_n \approx \frac{1}{N} \sum_{k=0}^{N-1} k_n \text{ [bps/Hz]}$$



Example: R(f) for OFDM



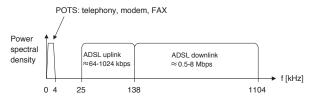
- N = 16 sub-carriers
- ▶ $T = T_s = 0.1 \text{ [ms]}$

•
$$f_{\Delta} = R_s / 0.95 = 10.53 \, [\text{kHz}]$$

• $W \approx \frac{17}{0.95} R_s = 179 [\text{kHz}]$



ADSL: uses plain telephone cable (twisted pair, copper)



In ADSL, a coded OFDM technique is used. The level of the power spectral density in the downstream is roughly -73 dB. As a basic example, let us here assume that the OFDM symbol rate in the downlink is 4000 [symbol/s], and that the subchannel carrier spacing is 5 kHz. Furthermore, it is here also assumed that uncoded 16-ary QAM is used in each subchannel (assumes a very "good" communication link).

For the ADSL downlink above, determine the bit rate in each subchannel, the total bit rate, and the bandwidth efficiency.



What about filtering away the side-lobes?

- ► Let us use a spectral rectangular pulse $X_{srec}(f)$ of amplitude A = 1and width f_{Δ} to strictly limit the bandwidth
- Similar to the time-limited case we can write

$$S_{f_{\Delta}}(f) = S(f) \cdot X_{srec}(f)$$

Taking the inverse Fourier transform on both sides we get

$$s_{f_{\Delta}}(t) = s(t) * x_{srec}(t) = s(t) * Af_0 \frac{\sin(\pi f_0 t)}{\pi f_0 t}$$

- Since x_{srec}(t) is unlimited along the time axis, this is the case for the filtered signal s_{f∆}(t) as well
- The signal $x_{srec}(t)$ defines the ideal Nyquist pulse

As a consequence of filtering, the transmitted symbols will overlap in time domain \Rightarrow inter-symbol-interference (ISI)



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Nyquist Pulse

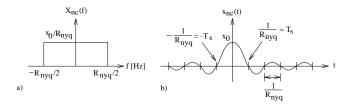


Figure 6.6: a) Ideal Nyquist spectrum; b) Ideal Nyquist pulse.

$$x_{nc}(t) = x_0 \frac{\sin(\pi R_{nyq}t)}{\pi R_{nyq}t}, -\infty \le t \le \infty$$

$$X_{nc}(f) = \begin{cases} x_0/R_{nyq} & |f| \le R_{nyq}/2 \\ 0 & |f| > R_{nyq}/2 \end{cases}$$
(6.39)
(6.39)
(6.39)
(6.39)

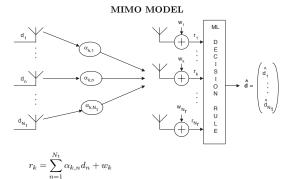
The Nyquist pulse and the effect of ISI will be studied in Chapter 6

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Digital Communications: Lecture 4

÷w?

How can we further improve ρ ?



- MIMO: multiple-input multiple output
- transmission over multiple antennas in the same frequency band
- challenge: the individual wireless channels interfere
- 5G world record 2016: (team from Lund involved) spectral efficiency of 145.6 bps/Hz with 128 antennas



Short summary

- Check different definitions bandwidth (one-sided and two-sided), time-limited signals cannot be strictly band-limited and vice versa
- Filtering and multiplication: linearity of convolution can be useful for combined signals
- ► A summary of bandwidth *W* and asymptotic decay of *R*(*f*) for different pulse shapes is given in Table 2.1
- The power spectral density R(f) and bandwidth efficiency ρ for M-PAM, M-QAM, M-FSK and OFDM are studied on p. 88–102

