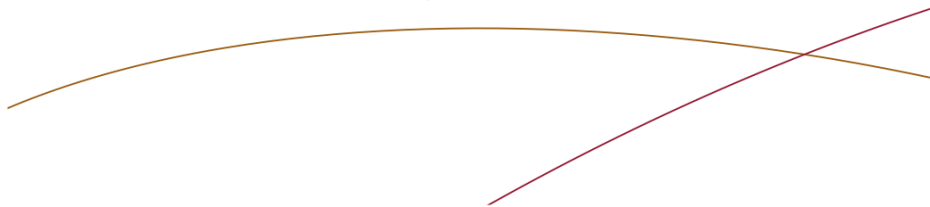


EITG05 – Digital Communications

Lecture 8

Chapter 3: Carrier modulation techniques Bandpass signals, digital and analog modulation

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Monday, October 1, 2018



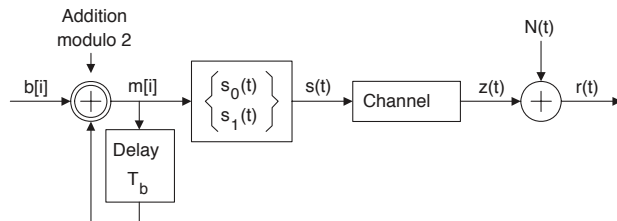
Differential Phase Shift Keying

- With **differential PSK**, the message $m[n] = m_\ell$ is mapped to the phase according to

$$\theta_n = \theta_{n-1} + \frac{2\pi\ell}{M} \quad \ell = 0, \dots, M-1$$

- The transmitted phase θ_n depends on both θ_{n-1} and $m[n]$
- This **differential encoding** introduces memory and the transmitted signal alternatives become dependent

- Example 5.25:** binary DPSK



From last lecture: Non-coherent receivers

- With **phase-shift keying (PSK)** the message $m[n]$ at time nT_s is put into the phase θ_n of the transmit signal

$$s(t) = g(t) \sqrt{2E} \cos(2\pi f_c t + \theta_n), \quad nT_s \leq t \leq (n+1)T_s$$

- The channel introduces some **attenuation** α , some additive **noise** $N(t)$ and also some **phase offset** ν into the received signal

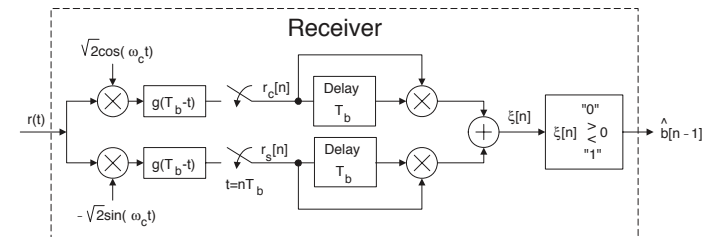
$$r(t) = \alpha g(t) \sqrt{2E} \cos(2\pi f_c t + \theta_n + \nu) + N(t)$$

- Challenge:** the optimal receiver needs to know α and ν
- In some applications an accurate estimation of ν is infeasible (**cost, complexity, size**)
- Non-coherent receivers:** receiver structures that can work well without knowledge of the exact phase offset

How can we modify our PSK transmission accordingly?



Differential Phase Shift Keying ($M = 2$)



- The receiver uses no phase offset ν in the carrier waveforms
- Without noise, the decision variable is

$$\begin{aligned} \xi[n] &= r_c[n] r_c[n-1] + r_s[n] r_s[n-1] \\ &= A \cos(\theta_{n-1} + \nu) A \cos(\theta_{n-2} + \nu) + A \sin(\theta_{n-1} + \nu) A \sin(\theta_{n-2} + \nu) \\ &= A^2 \cos(\theta_{n-1} - \theta_{n-2}) \Rightarrow \text{independent of } \nu \end{aligned}$$

- Note:** non-coherent reception increases variance of noise



Chapter 3: Carrier modulation techniques

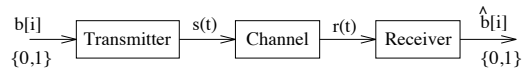
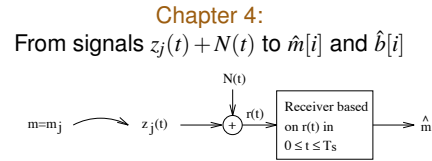
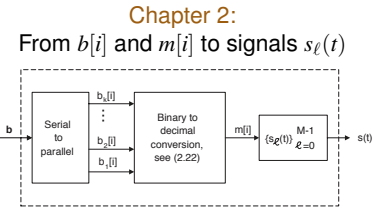


Figure 4.1: A digital communication system.

What we have done so far:



Now more on:

- ▶ properties of bandpass signals
- ▶ the channel: from $s(t)$ over $z(t)$ to $r(t)$
- ▶ efficient receivers for bandpass signals

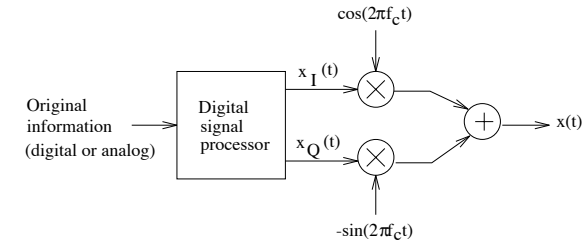


Bandpass Signals

- ▶ A **general bandpass signal** can always be written as

$$x(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t), \quad -\infty \leq t \leq \infty$$

- ▶ $x_I(t)$: **inphase component** $x_Q(t)$: **quadrature component**
- ▶ Corresponding transmitter structure:



- ▶ The **information** is contained in the signals $x_I(t)$ and $x_Q(t)$ (for both analog or digital modulation)
- ▶ Not only wireless systems use carrier modulation

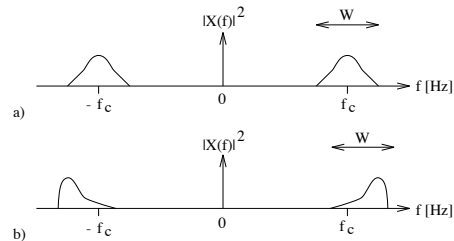


Spectrum of bandpass signals

- ▶ Computing the Fourier transform of $x(t)$ we get

$$X(f) = \frac{X_I(f+f_c) - j X_Q(f+f_c)}{2} + \frac{X_I(f-f_c) + j X_Q(f-f_c)}{2}$$

- ▶ Normally, $X_I(t)$ and $X_Q(t)$ have **baseband** characteristic, and f_c is much larger than their bandwidth
- ▶ The spectrum can be **symmetric** or **non-symmetric** around f_c



- ▶ **Remember:** real signals $x(t)$ always have **even** $|X(f)|$



DSB-SC Carrier Modulation

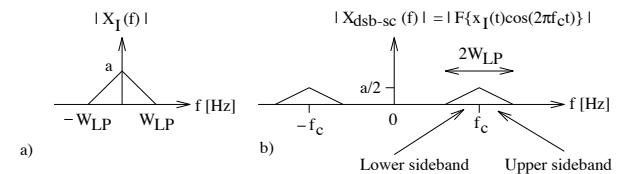
- ▶ **Double sideband-suppressed** (DSB-SC) carrier modulation is a special case of our general model
- ▶ In this case only $x_I(t)$ contains information and $x_Q(t) = 0$, i.e.,

$$x_{dsb-sc}(t) = x_I(t) \cos(2\pi f_c t)$$

- ▶ The Fourier transform then simplifies to

$$X(f) = \frac{X_I(f+f_c)}{2} + \frac{X_I(f-f_c)}{2}$$

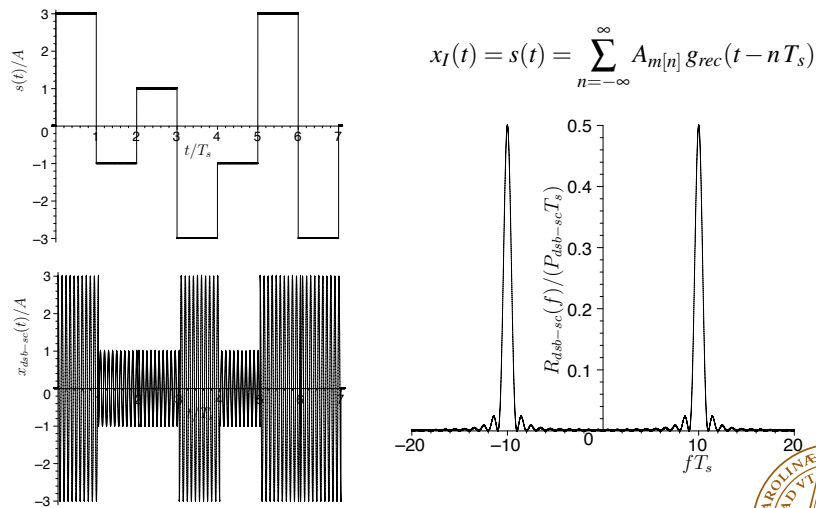
- ▶ $X_I(f)$ is symmetric around $f = 0 \Rightarrow X_I(f)$ is symmetric around f_c



Where does the name come from?



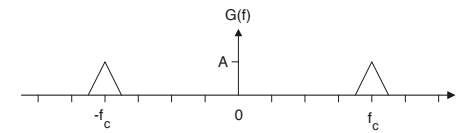
Example 3.1: 4-ary PAM



$$x_I(t) = s(t) = \sum_{n=-\infty}^{\infty} A_m[n] g_{rec}(t - nT_s)$$

How can we revert the frequency shift to f_c ?

Hint: check Example 2.19 (p. 68)

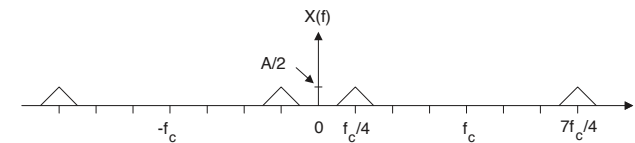


Find the frequency content of

$$x(t) = g(t) \cos(2\pi f_0 t), \quad f_0 = 3f_c/4$$

Solution:

If we apply (2.157) using $G(f)$ above, we obtain the frequency content in $x(t)$ as

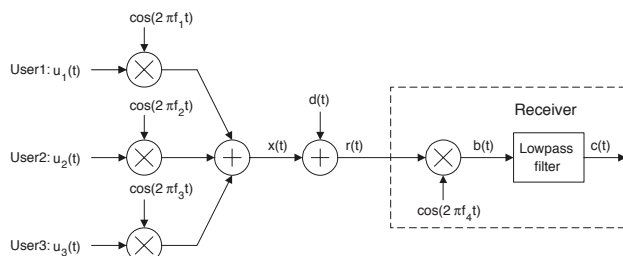
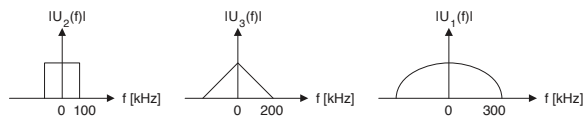


How should we choose f_0 to get the baseband signal back?



Problem 3.9

In the three-user (digital) communication system below, the frequency content in the user information signals $u_1(t)$, $u_2(t)$ and $u_3(t)$ are,



It is known that the individual carrier frequencies are: $f_1 = 3.5$ MHz, $f_2 = 4.0$ MHz, $f_3 = 3$ MHz. The disturbance $d(t)$ is $d(t) = \cos(2\pi 2f_d t)$ where $f_d = 1.7$ MHz. Only frequencies up to 100 kHz pass the lowpass filter.



Envelope and Phase

- ▶ A frequency shift corresponds to a multiplication with $e^{j2\pi f_c t}$
- ▶ For connecting this to the cosine and sine function we use

$$e^{j2\pi f_c t} = \cos(2\pi f_c t) + j \sin(2\pi f_c t)$$

- ▶ The general bandpass signal can then be written in terms of a frequency shifted version of a complex signal $x_I(t) + jx_Q(t)$

$$x(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t) = \text{Re} \{ (x_I(t) + jx_Q(t)) e^{j2\pi f_c t} \}$$

- ▶ Expressing $x_I(t) + jx_Q(t)$ in terms of magnitude and phase we get

$$x(t) = e(t) \cos(2\pi f_c t + \theta(t)), \quad -\infty \leq t \leq \infty$$

with

$$e(t) = \sqrt{x_I^2(t) + x_Q^2(t)} \geq 0$$

$$x_I(t) = e(t) \cos(\theta(t))$$

$$x_Q(t) = e(t) \sin(\theta(t))$$



I-Q Diagram

- In the representation

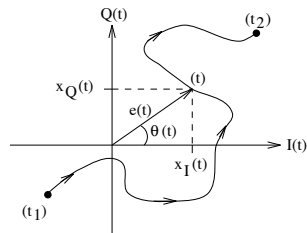
$$x(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t)$$

the information is contained in the **inphase** component $x_I(t)$ and **quadrature** component $x_Q(t)$

- In the representation

$$x(t) = e(t) \cos(2\pi f_c t + \theta(t)), \quad -\infty \leq t \leq \infty$$

the information is contained in the **envelope** $e(t)$ and **instantaneous phase** $\theta(t)$



connection: I-Q diagram



Analog Information Transmission

- Suppose that the information signal is an analog waveform $a(t)$
Examples: music, speech, video

- If we use **digital modulation**, the waveform $a(t)$ is first converted to a binary sequence $b[i]$, which then is mapped to signals $s_\ell(t)$
- In case of **analog modulation**, the waveform $a(t)$ is used directly to modulate the carrier signal

- Let $v(t)$ denote the bandpass signal of an analog transmitter

$$v(t) = v_I(t) \cos(2\pi f_c t) - v_Q(t) \sin(2\pi f_c t), \quad -\infty \leq t \leq \infty$$

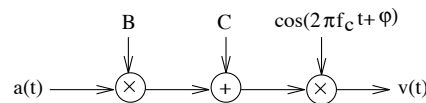
$$= e(t) \cos(2\pi f_c t + \theta(t))$$

- Amplitude modulation (AM):**
the waveform $a(t)$ modulates the envelope $e(t)$ only

- Frequency modulation (FM):**
here $a(t)$ modulates the instantaneous phase $\theta(t)$ only



Amplitude Modulation (AM)



- The **AM signal** is the sum of a DSB-SC signal and carrier wave

$$v(t) = (a(t)B + C) \cos(2\pi f_c t + \varphi)$$

$$= a(t)B \cos(2\pi f_c t + \varphi) + C \cos(2\pi f_c t + \varphi)$$

- Let us introduce the **modulation index**

$$m = \frac{B a_{max}}{C} \leq 1, \quad \text{where } a_{max} = \max |a(t)|$$

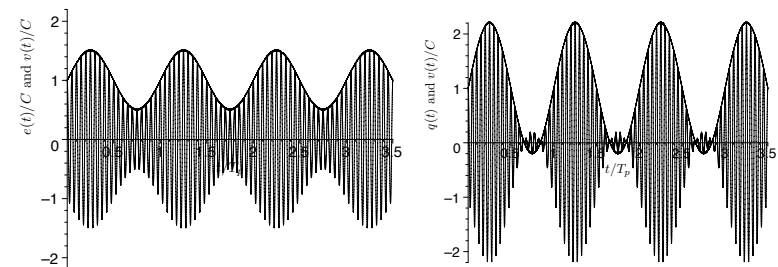
- Using the normalized signal $a_n(t) = a(t)/a_{max}$ we can write

$$v(t) = (1 + m a_n(t)) C \cos(2\pi f_c t + \varphi)$$



Example: AM signal

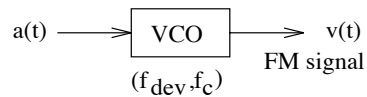
$$e(t)/C = 1 + m a(t), \quad a_n(t) = \sin(2\pi f_p t), \quad f_p = 1/T_p$$



- $m = 0.5 < 1$:
the information signal $a_n(t)$ is contained in the envelope $e(t)$
- $m = 1.2 > 1$: (right picture)
overmodulation: the baseband signal $q(t) = (1 + 1.2 a_n(t))$ is no longer equal to $e(t)$



Frequency Modulation (FM)



- ▶ With **FM modulation**, the transmitted signal is generated by a **voltage controlled oscillator (VCO)**
- ▶ The information carrying signal $a(t)$ is related to the phase $\theta(t)$ by

$$\frac{1}{2\pi} \frac{d\theta(t)}{dt} = f_{dev} \cdot a(t)$$

- ▶ The signal $a(t)$ hence modulates the **instantaneous frequency**

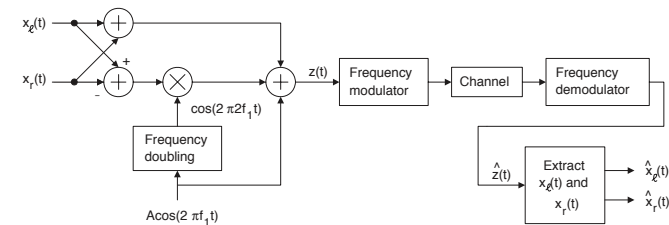
$$f_{ins}(t) = f_c + \frac{1}{2\pi} \frac{d\theta(t)}{dt} = f_c + f_{dev} a(t)$$

- ▶ FM modulation is a **non-linear** operation, hard to analyze

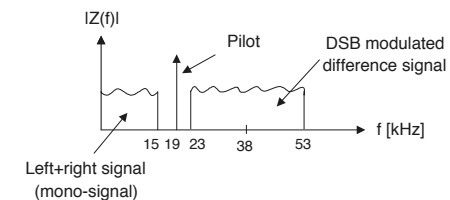


Example 3.13: FM stereo

A possible block-diagram of conventional analog FM stereo is shown below.



$x_l(t)$ and $x_r(t)$ denotes the left and the right audio-channel, respectively, and they are both bandlimited to 15 [kHz]. The frequency $f_1 = 19$ [kHz] (often referred to as a so-called pilot-tone).



Digital Information Transmission

- ▶ In Chapter 2 the signal alternatives $s_\ell(t)$ could have arbitrary shape within the signaling interval $0 \leq t \leq T_s$
- ▶ The bandpass signal for **digital modulation** then has the form

$$x(t) = x_I(t) \cos(2\pi f_c t) - x_Q(t) \sin(2\pi f_c t) \\ = \left(\sum_{n=-\infty}^{\infty} s_{m[n],I}(t - nT_s) \right) \cos(2\pi f_c t) \\ - \left(\sum_{n=-\infty}^{\infty} s_{m[n],Q}(t - nT_s) \right) \sin(2\pi f_c t)$$

- ▶ In case of **M-ary QAM** we have

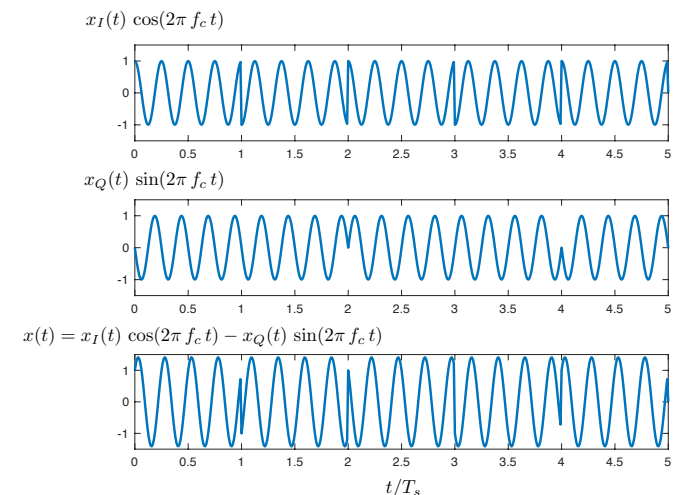
$$x_I(t) = \sum_{n=-\infty}^{\infty} A_{m[n]} g(t - nT_s), \quad x_Q(t) = \sum_{n=-\infty}^{\infty} B_{m[n]} g(t - nT_s)$$

- ▶ Also **M-ary FSK** signals have bandpass characteristics



A simple Matlab example

How does a QPSK signal look like? Here is an example:



And how it was done:

```

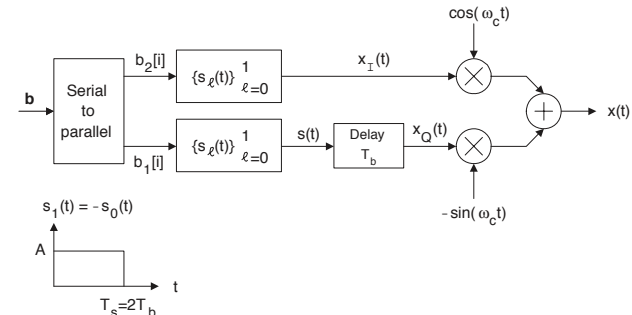
1 % Example: QPSK signal
2
3 t=0:0.01:5;
4 fc=4;
5 pRec=ones(1,(length(t)-1)/5);
6 sI=zeros(1,length(t)); sQ=zeros(1,length(t));
7
8 dataI=[1 -1 1 -1 1];
9 indPulse=1:(length(t)-1)/5;
10 for i=1:length(dataI)
11     sI(indPulse)=dataI(i)*pRec;
12     indPulse=indPulse+length(indPulse);
13 end;
14
15 dataQ=[-1 -1 1 1 -1];
16 indPulse=1:(length(t)-1)/5;
17 for i=1:length(dataQ)
18     sQ(indPulse)=dataQ(i)*pRec;
19     indPulse=indPulse+length(indPulse);
20 end;
21
22 sCarI=cos(2*pi*t*fc); sCarQ=sin(2*pi*t*fc);
23
24 figure(1);
25 subplot(3,1,1); plot(t,sI.*sCarI);
26 set(gca,'YLim',[-1.5 1.5]); xlabel('tT_s');
27
28 subplot(3,1,2); plot(t,sQ.*sCarQ);
29 set(gca,'YLim',[-1.5 1.5]); xlabel('tT_s');
30
31 subplot(3,1,3); plot(t,sI.*sCarI - sQ.*sCarQ);
32 set(gca,'YLim',[-1.5 1.5]); xlabel('tT_s');
33
34

```



Example 3.5: offset QPSK

Below, two information carrying baseband signals $x_I(t)$ and $s(t)$ are first generated. Binary antipodal signaling with a rectangular pulse shape is used for both $x_I(t)$ and $s(t)$. The signal $x_Q(t)$ is a delayed version of $s(t)$, $x_Q(t) = s(t - T_b)$.

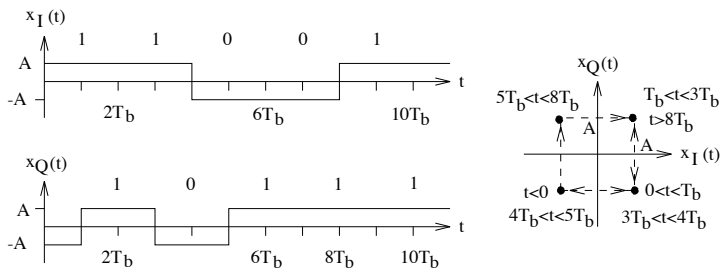


The information bit rate (in b) is $R_b = 1/T_b$. Hence, the signaling rate in the quadrature components is $R_s = R_b/2$.



QPSK signal with delayed transmission of $x_Q(t)$

Example 3.5: offset QPSK



- ▶ **Special feature:** $x_I(t)$ and $x_Q(t)$ can never change at the same time
- ▶ it follows that the envelope does not pass the origin, i.e., $e(t) > 0$
- ▶ the variation of instantaneous power $\mathcal{P}(t) = e^2(t)/2$ is small, which allows more efficient power amplifiers

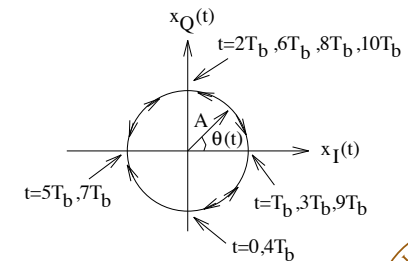
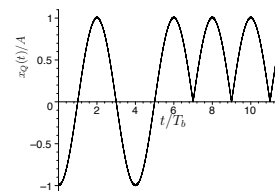
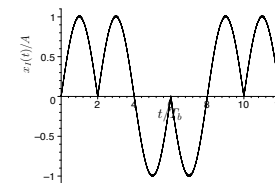


Example 3.6: constant envelope signaling

Change pulse shape: half cycle sinusoidal $g_{hcs}(t)$ instead of $g_{rec}(t)$

The squared envelope becomes

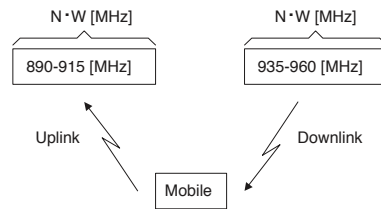
$$\begin{aligned}
 e^2(t) &= x_I^2(t) + x_Q^2(t) \\
 &= A^2 \sin^2(\pi t / (2T_b)) + A^2 \cos^2(\pi t / (2T_b)) \\
 &= A^2 \Rightarrow \text{constant envelope } e(t) = A
 \end{aligned}$$



Continuous phase modulation (CPM) is used in GSM

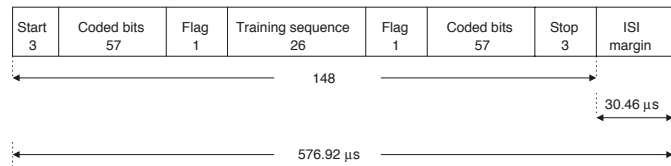


Example 3.7: GSM



Each sub-band of W [Hz] carries information from X users, which are time-multiplexed using X time-slots. The total number of speech-channels (or data-channels) in the uplink (and in the downlink) is $N \cdot X$.

A specific user is allocated one of the N sub-bands, and one of the X time-slots. A time-slot has duration 576.92 [μ s], and 148 binary symbols are transmitted within this time, see the figure below.



From 2G to 4G

- ▶ **GSM:** (Global System for Mobile Communications) based on combined time-division multiple access (TDMA) and frequency division multiple access (FDMA)
- ▶ **UMTS:** (Universal Mobile Telecommunications Service) based on wideband code division multiple access (W-CDMA) each user has an individual code, no TDMA or FDMA
- ▶ **LTE (advanced):** (Long Term Evolution) orthogonal frequency-division multiple access (OFDMA)

Multiple access:

refers to how different active users are separated

