RADIO SYSTEMS – ETIN15

Lecture no: 6

Demodulation, bit-error probability and diversity arrangements

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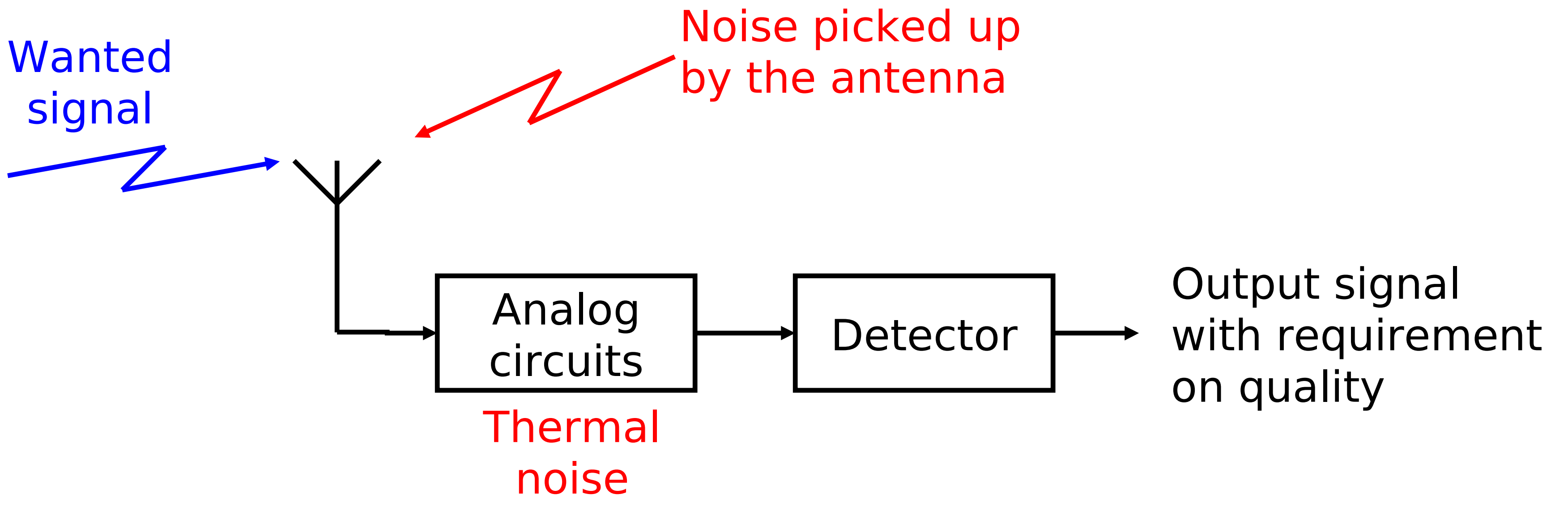
Contents

- Receiver noise calculations [Covered briefly in Chapter 3 of textbook!]
- Optimal receiver and bit error probability
  - Principle of maximum-likelihood receiver
  - Error probabilities in non-fading channels
  - Error probabilities in fading channels
- Diversity arrangements
  - The diversity principle
  - Types of diversity
  - Spatial (antenna) diversity performance

RECEIVER NOISE

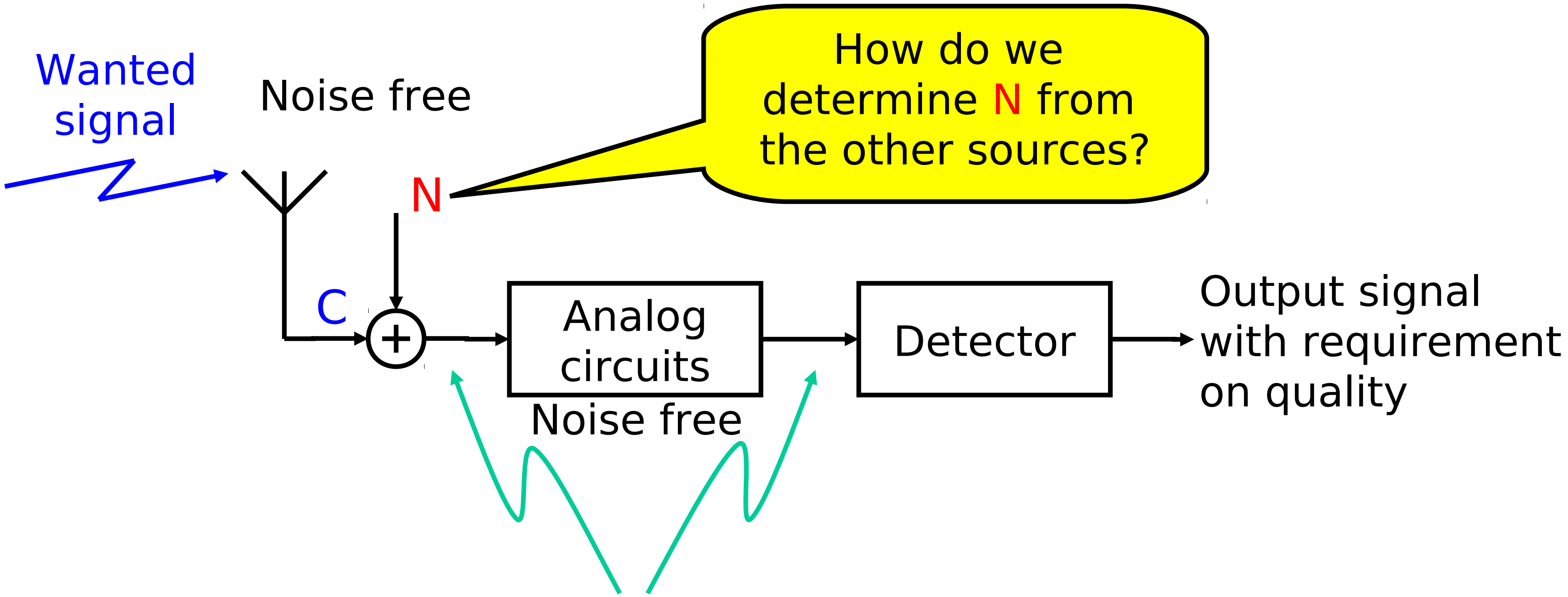
Receiver noise
Noise sources

The noise situation in a receiver depends on several noise sources



Receiver noise
Equivalent noise source

To simplify the situation, we replace all noise sources with a single equivalent noise source.



Same “input quality”, signal-to-noise ratio, C/N in the whole chain.

Receiver noise
Examples

- **Thermal noise** is caused by random movements of electrons in circuits. It is assumed to be Gaussian and the power is proportional to the temperature of the material, in Kelvin.
- **Atmospheric noise** is caused by electrical activity in the atmosphere, e.g. lightning. This noise is impulsive in its nature and below 20 MHz it is a dominating.
- **Cosmic noise** is caused by radiation from space and the sun is a major contributor.
- **Artificial (man made) noise** can be very strong and, e.g., light switches and ignition systems can produce significant noise well above 100 MHz.

Receiver noise
Noise sources

The power spectral density of a noise source is usually given in one of the following three ways:

1) Directly [W/Hz]: N_s

2) Noise **temperature** [Kelvin]: T_s

3) Noise **factor** [1]: F_s

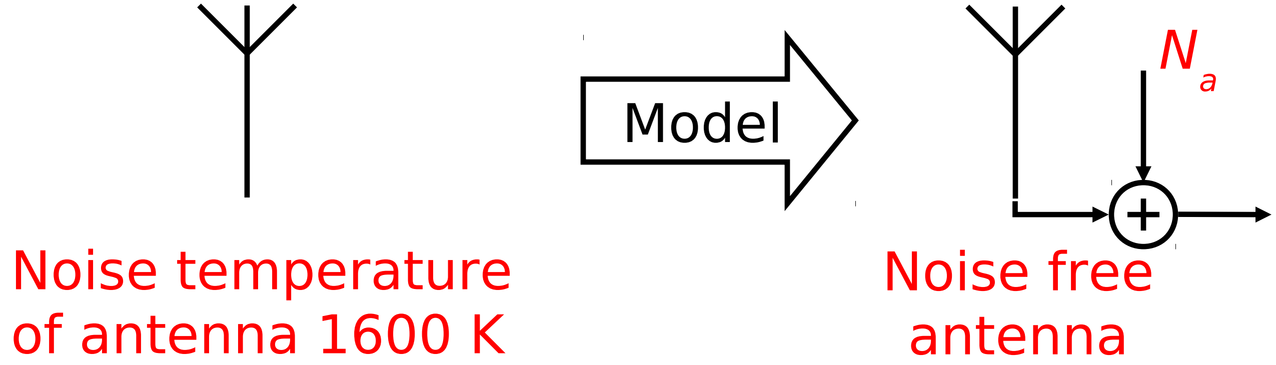
This one is often given in dB and called **noise figure**.

The relation between the three is

$$N_s = kT_s = kF_sT_0$$

where k is **Boltzmann's constant** (1.38×10^{-23} W/Hz) and T_0 is the, so called, **room temperature** of 290 K (17° C).

Antenna example



Power spectral density of antenna noise is

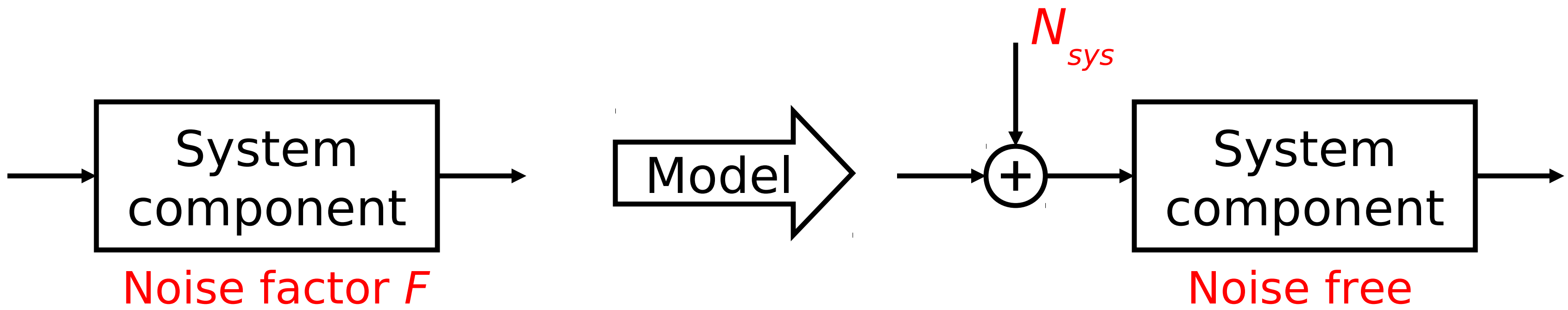
$$N_a = 1.38\times 10^{-23}\times 1600 = 2.21\times 10^{-20}\ \text{W/Hz} = -196.6\ \text{dB [W/Hz]}$$

and its noise factor/noise figure is

$$F_a = 1600/290 = 5.52 = 7.42\ \text{dB}$$

Receiver noise
System noise

The noise factor or noise figure of a system component (with input and output) is defined in a different way than for noise sources:



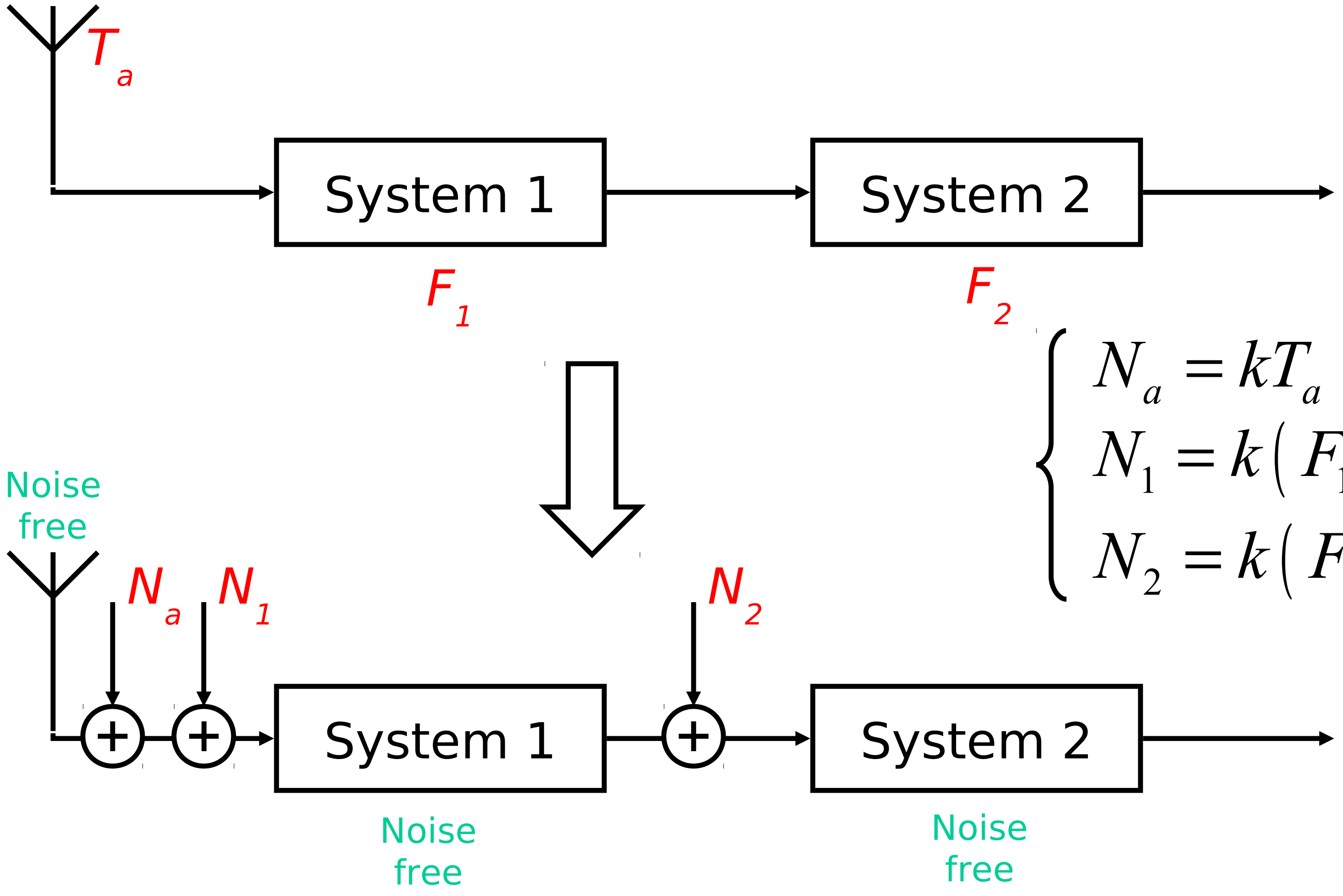
Due to a definition of noise factor (in this case) as the ratio of noise powers on the output versus on the input, when a resistor in room temperature (T_0=290 K) generates the input noise, the PSD of the equivalent noise source (placed **at the input**) becomes

$$N_{sys} = k \underbrace{(F-1)\,T_0}_{\text{Equivalent noise temperature}} \ \mathrm{W/Hz}$$

Don’t use dB value!

Receiver noise
Several noise sources

A simple example

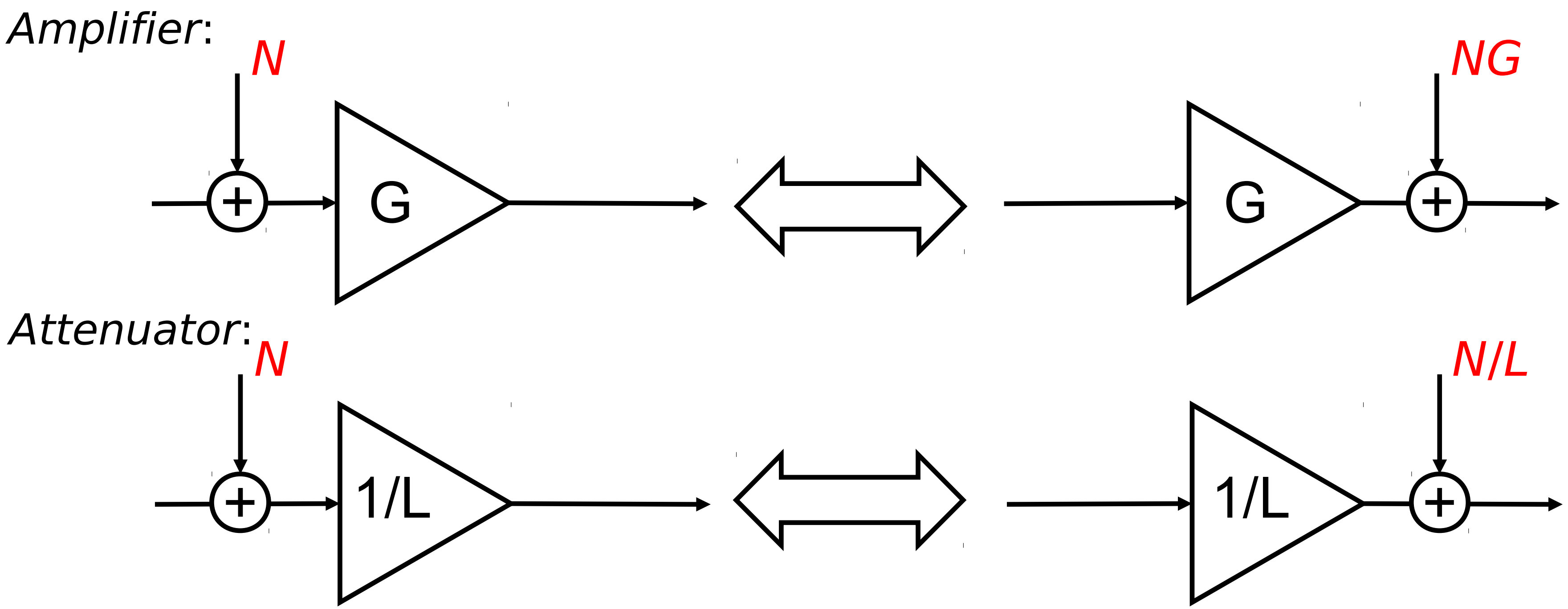


$$\begin{cases} N_a = kT_a \\ N_1 = k\left(F_1 - 1\right)T_0 \\ N_2 = k\left(F_2 - 1\right)T_0 \end{cases}$$

Receiver noise
Several noise sources, cont.

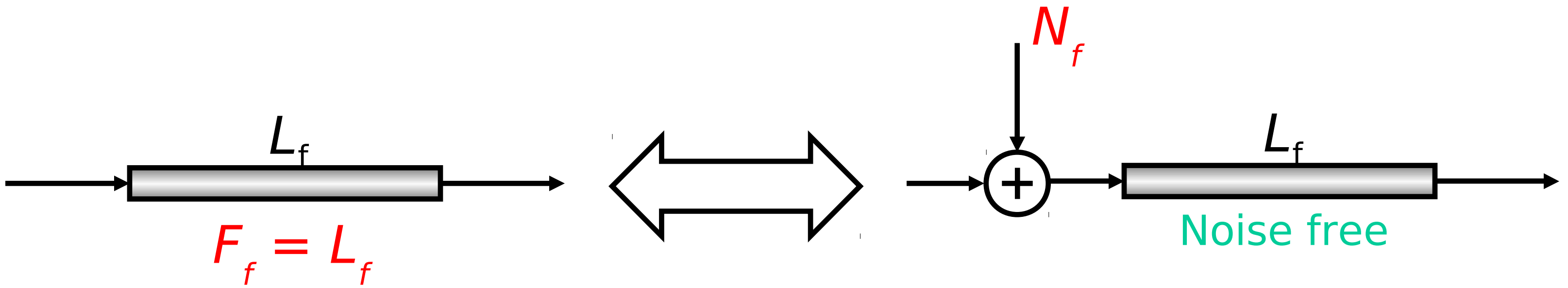
After extraction of the noise sources from each component, we need to move them to one point.

When doing this, we must compensate for amplification and attenuation!



Receiver noise
Pierce's rule

A passive attenuator in room temperature, in this case a feeder, has a noise figure equal to its attenuation.



$$N_f = k\left(F_f - 1\right)T_0 = k\left(L_f - 1\right)T_0$$

Remember to convert ***from*** dB!

Receiver noise
Remember ...

Antenna noise is usually given as a noise temperature!

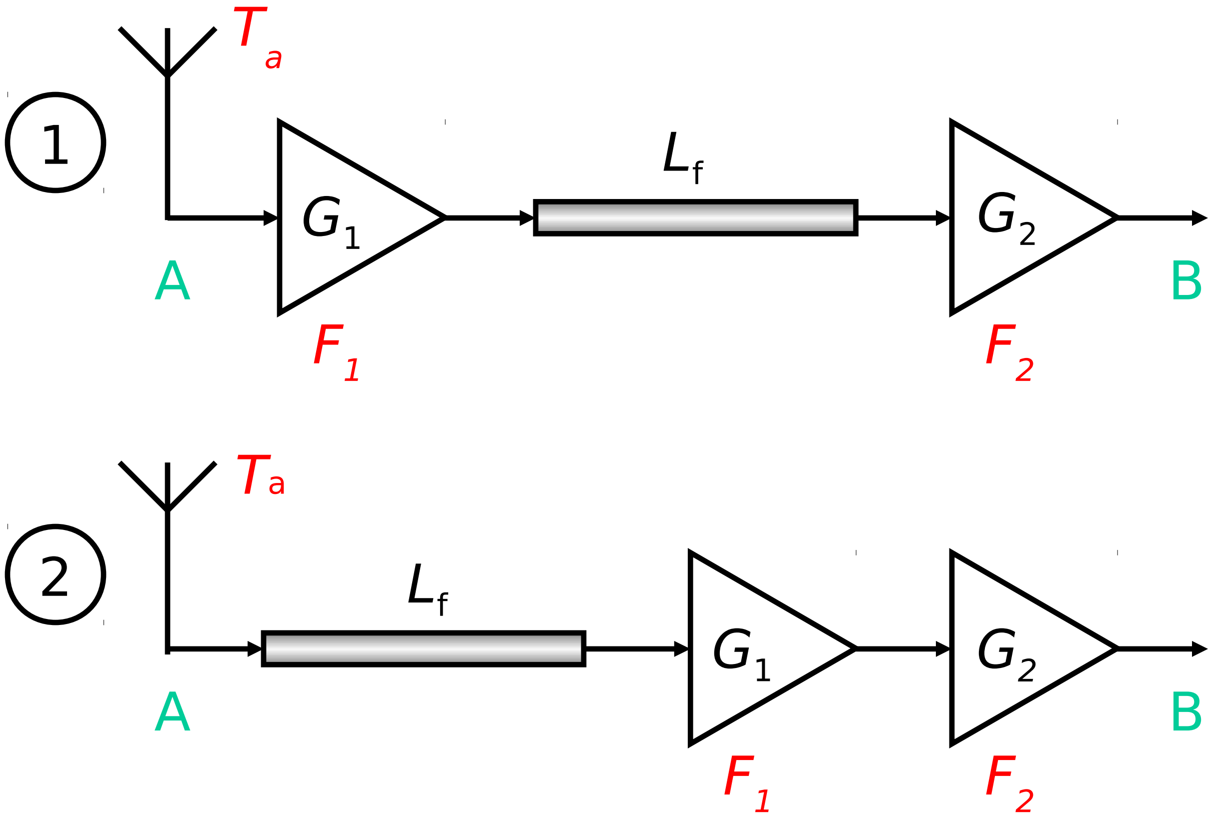
Noise factors or noise figures of different system components are determined by their implementation.

When adding noise from several sources, remember to convert ***from*** the dB-scale noise figures that are usually given, before starting your calculations.

A passive attenuator in (room temperature), like a feeder, has a noise figure/factor equal to its attenuation.

Receiver noise
A final example

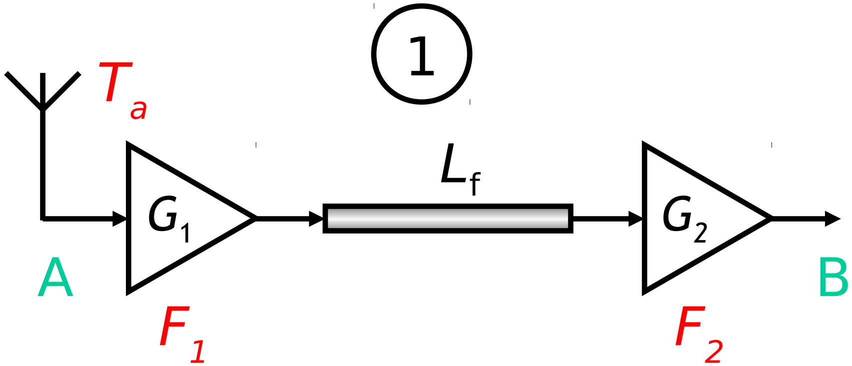
Let's consider two (incomplete) receiver chains with **equal gain** from point A to B:

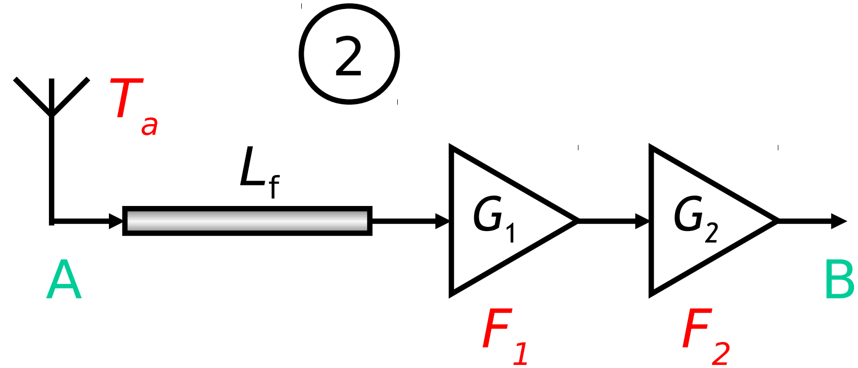


Would there be any reason to choose one over the other?

Let's calculate the equivalent noise at point **A** for both!

Receiver noise
A final example





Equivalent noise sources at point A for the two cases would have the power spectral densities:

1 $$N_0 = kT_a + k\Big(\big(F_1 - 1\big) + \big(L_f - 1\big)/G_1 + \big(F_2 - 1\big)L_f/G_1\Big)T_0$$

2 $$N_0 = kT_a + k\Big(\big(L_f - 1\big) + \big(F_1 - 1\big)L_f + \big(F_2 - 1\big)L_f/G_1\Big)T_0$$

Two of the noise contributions are equal and two are larger in (2), which makes (1) a better arrangement.

This is why we want a low-noise amplifier (LNA) close to the antenna.

Receiver noise
Noise power

We have discussed noise in terms of *power spectral density* N_0 [W/Hz].

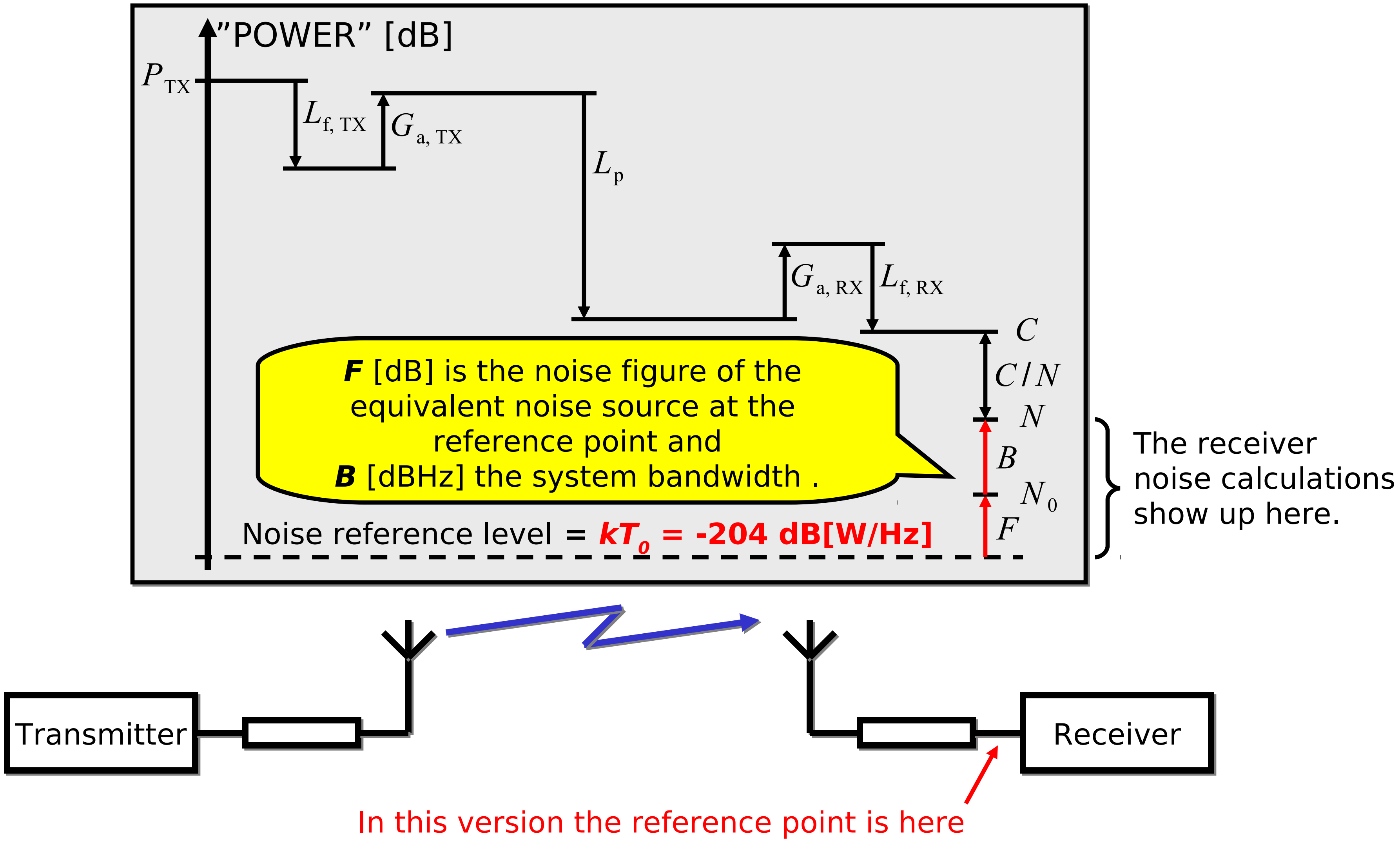
For a certain receiver bandwidth B [Hz], we can calculate the equivalent *noise power*:

$$N = B \times N_0 \text{ [W]}$$

$$N_{|\mathrm{dB}} = B_{|\mathrm{dB}} + N_{0|\mathrm{dB}} \text{ [dBW]}$$

This is the version we will use in our link budget.

Receiver noise
The link budget



OPTIMAL RECEIVER
AND
BIT ERROR PROBABILITY

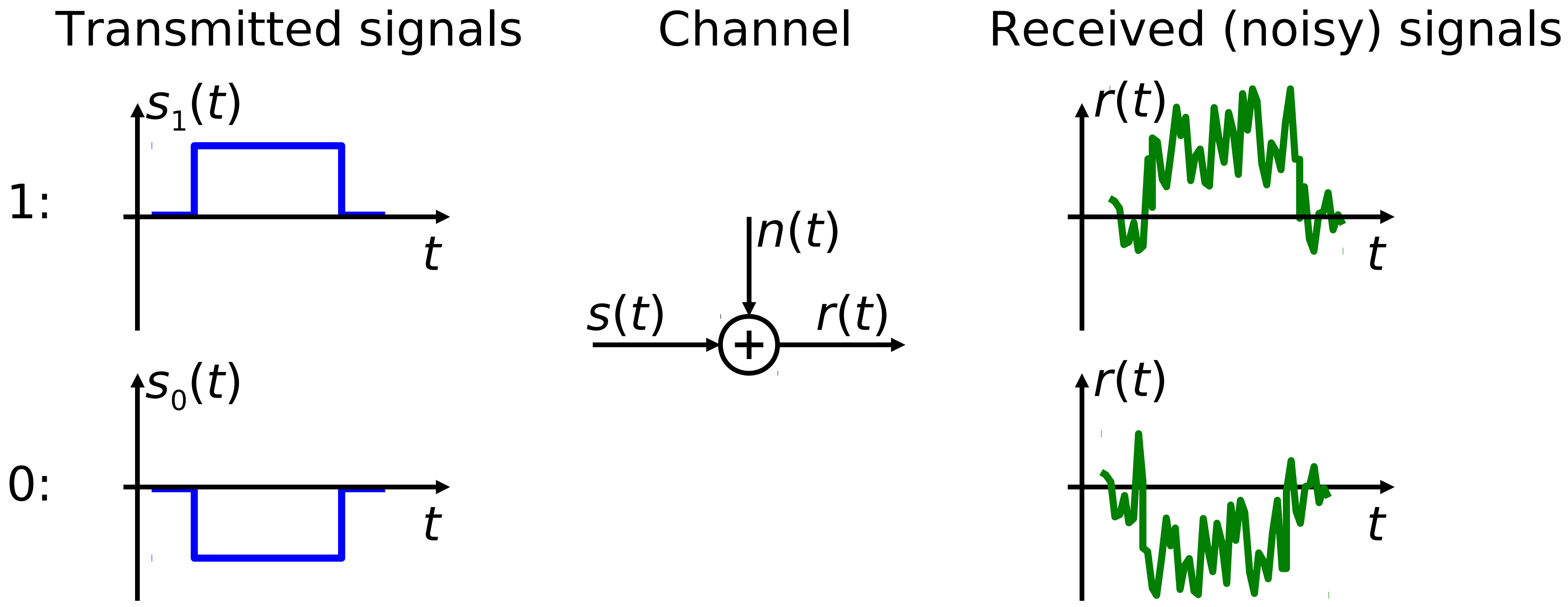
Optimal receiver
What do we mean by optimal?

Every receiver is optimal according to some criterion!

We would like to use optimal in the sense that we achieve a minimal probability of error.

In all calculations, we will assume that the noise is white and Gaussian – unless otherwise stated.

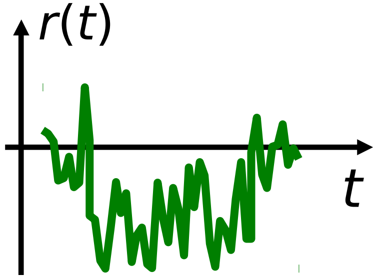
Optimal receiver
Transmitted and received signal



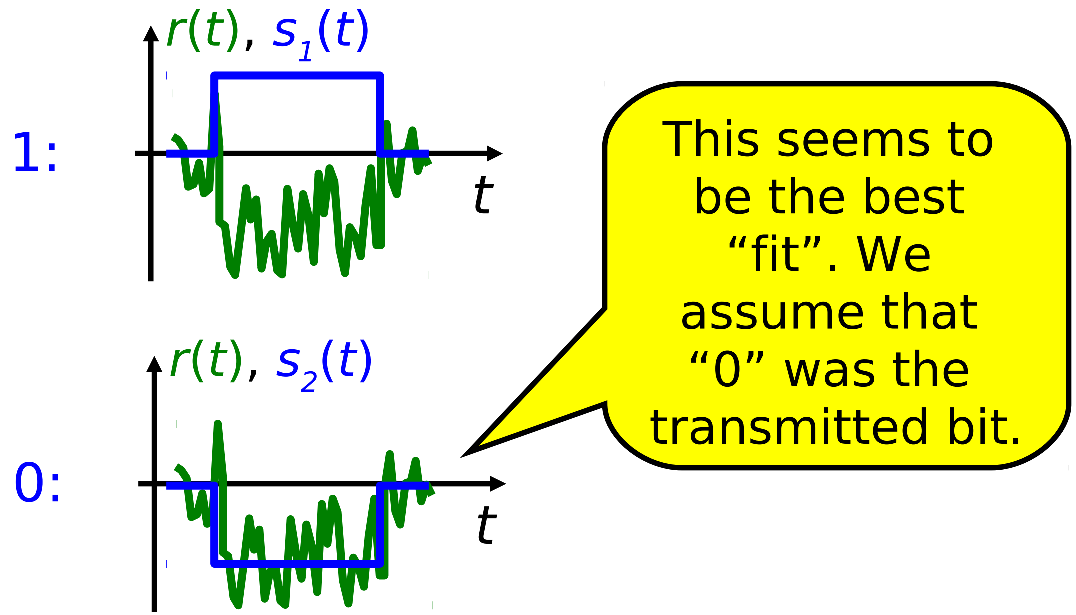
Optimal receiver
A first "intuitive" approach

"Look" at the received signal and compare it to the possible received **noise free** signals. Select the one with the best "fit".

Assume that the following signal is received:



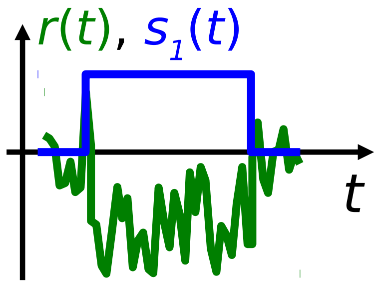
Comparing it to the two possible **noise free** received signals:

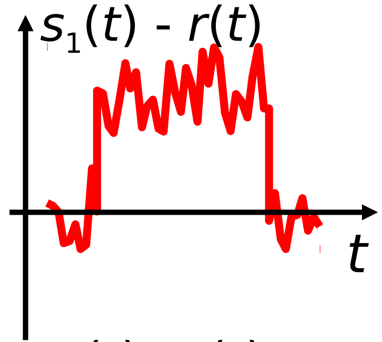


Optimal receiver
Let’s make it more measurable

To be able to better measure the “fit” we look at the **energy** of the **residual** (difference) between received and the possible noise free signals:

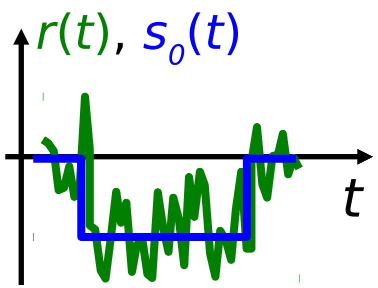
1:

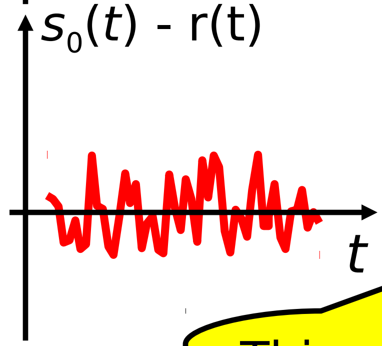




$$e_1 = \int \left| s_1(t) - r(t) \right|^2 dt$$

0:



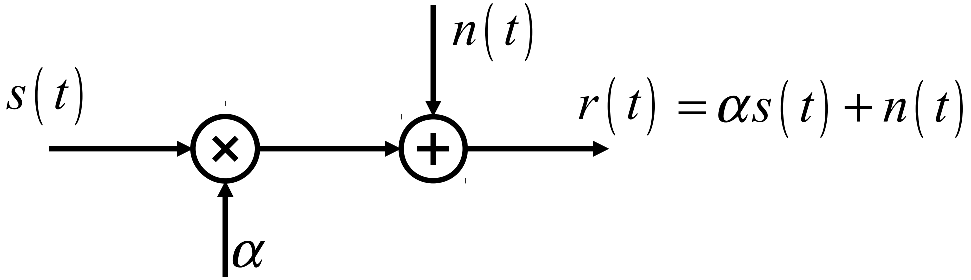


$$e_0 = \int \left| s_0(t) - r(t) \right|^2 dt$$

This residual energy is much smaller. We assume that “0” was transmitted.

Optimal receiver
The AWGN channel

The additive white Gaussian noise (AWGN) channel



$s(t)$ - transmitted signal

α - channel attenuation

$n(t)$ - white Gaussian noise

$r(t)$ - received signal

In our digital transmission system, the transmitted signal $s(t)$ would be one of, let's say M, different alternatives $s_0(t)$, $s_1(t)$, ... , $s_{M-1}(t)$.

Optimal receiver
The AWGN channel, cont.

It can be shown that finding the minimal residual energy (as we did before) is the optimal way of deciding which of $s_0(t)$, $s_1(t)$, … , $s_{M\text{-}1}(t)$ was transmitted over the AWGN channel (if they are equally probable).

For a received $r(t)$, the residual energy e_i for each possible transmitted alternative $s_i(t)$ is calculated as

$$e_i = \int \left| r(t) - \alpha s_i(t) \right|^2 dt = \int \left(r(t) - \alpha s_i(t) \right) \left(r(t) - \alpha s_i(t) \right)^* dt$$

$$= \int \left| r(t) \right|^2 dt - 2\,\mathrm{Re}\left\{ \alpha^* \int r(t)\, s_i^*(t)\, dt \right\} + |\alpha|^2 \int \left| s_i(t) \right|^2 dt$$

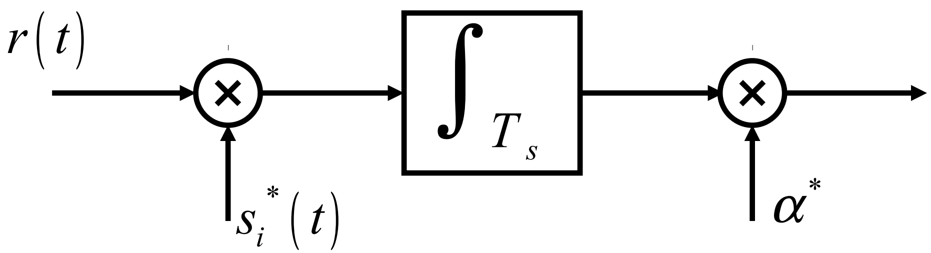
Same for all *i*

The residual energy is minimized by **maximizing** this part of the expression.

Same for all *i*,
if the transmitted
signals are of
equal energy.

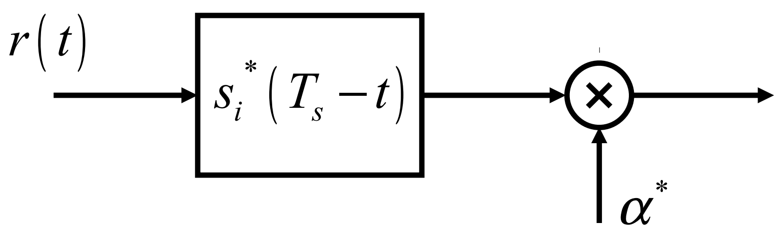
Optimal receiver
The AWGN channel, cont.

The central part of the comparison of different signal alternatives is a correlation, that can be implemented as a correlator:



The real part of the output from either of these is sampled at $t = T_s$

or a matched filter



where T_s is the symbol time (duration).

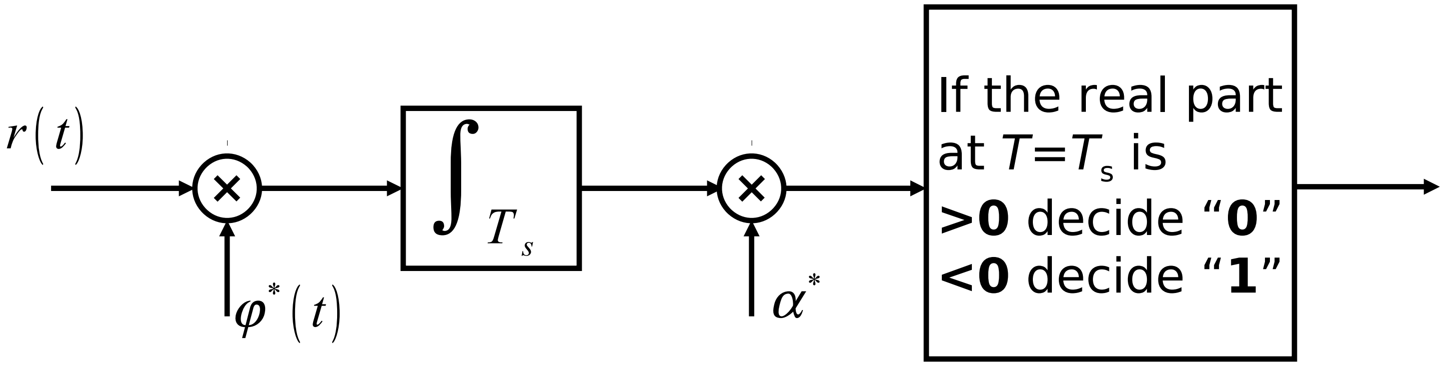
Optimal receiver
Antipodal signals

In antipodal signaling, the alternatives (for “0” and “1”) are

$$s_0(t) = \varphi(t)$$

$$s_1(t) = -\varphi(t)$$

This means that we only need ONE correlation in the receiver for simplicity:

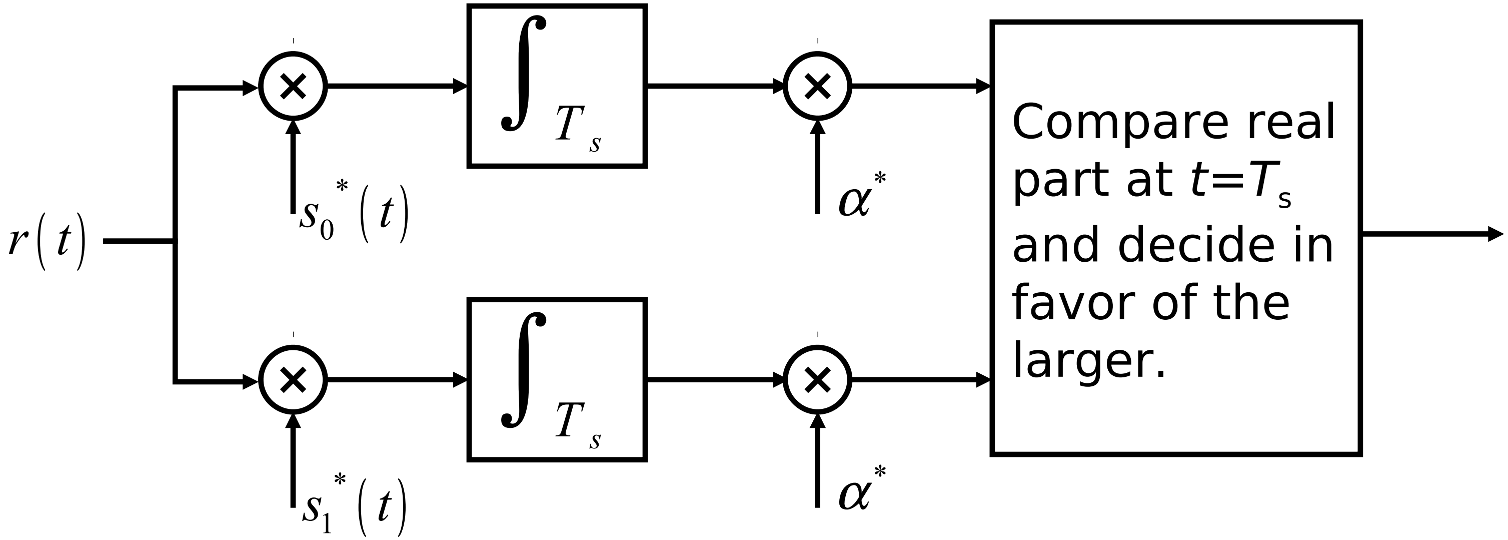


Optimal receiver
Orthogonal signals

In binary orthogonal signaling, with equal energy alternatives $s_0(t)$ and $s_1(t)$ (for "0" and "1") we require the property:

$$\langle s_o(t), s_1(t) \rangle = \int s_0(t) s_1^*(t)\, dt = 0$$

The approach here is to use two correlators:

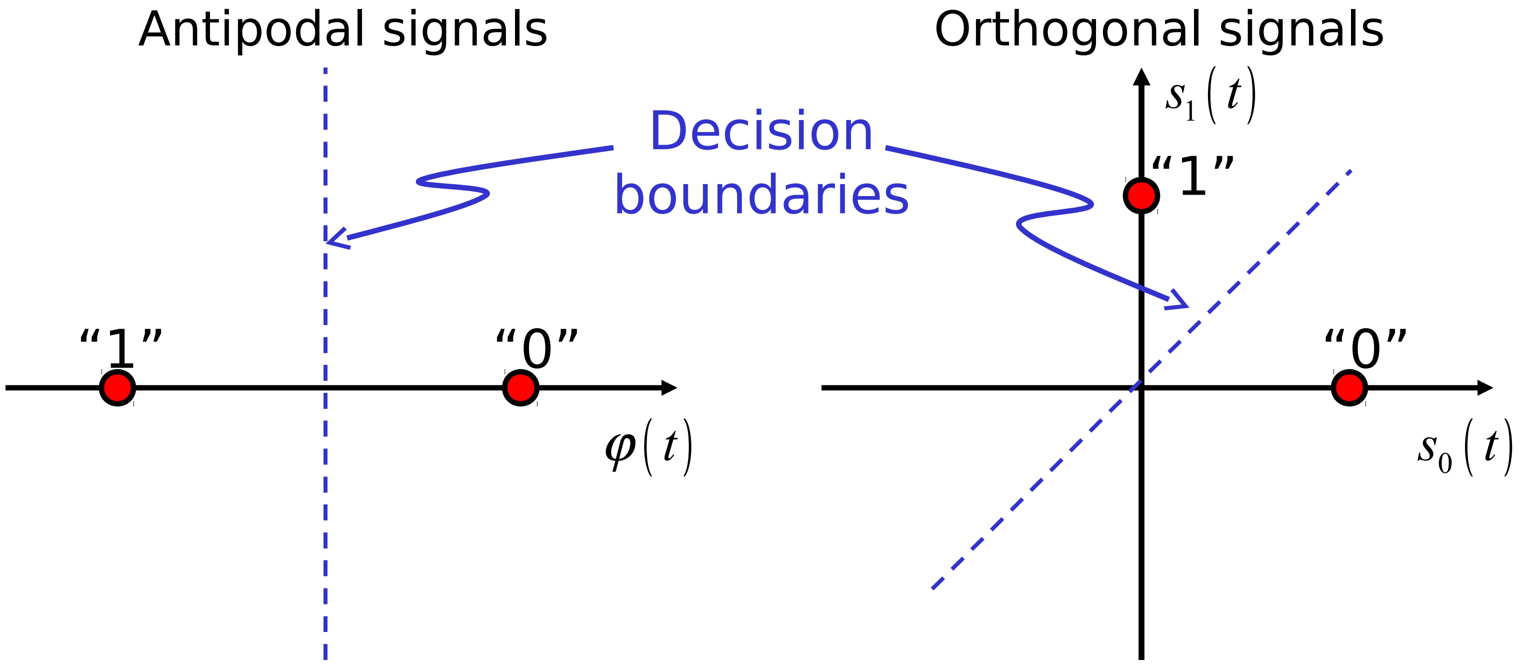


(Only one correlator is needed, if we correlate with $(s_0(t) - s_1(t))^*$.)

Optimal receiver
Interpretation in signal space

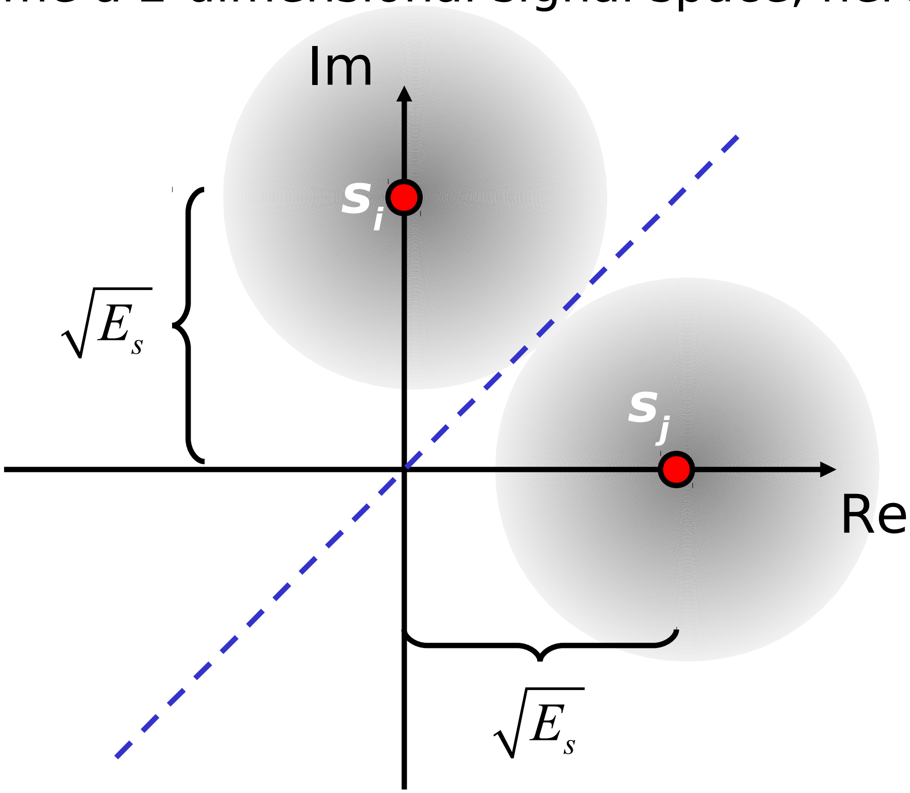
The correlations performed on the previous slides can be seen as inner products between the received signal and a set of basis functions for a signal space.

The resulting values are coordinates of the received signal in the signal space.



Optimal receiver
The noise contribution

Assume a 2-dimensional signal space, here viewed as the complex plane



This normalization of axes implies that the noise centered around each alternative is complex Gaussian

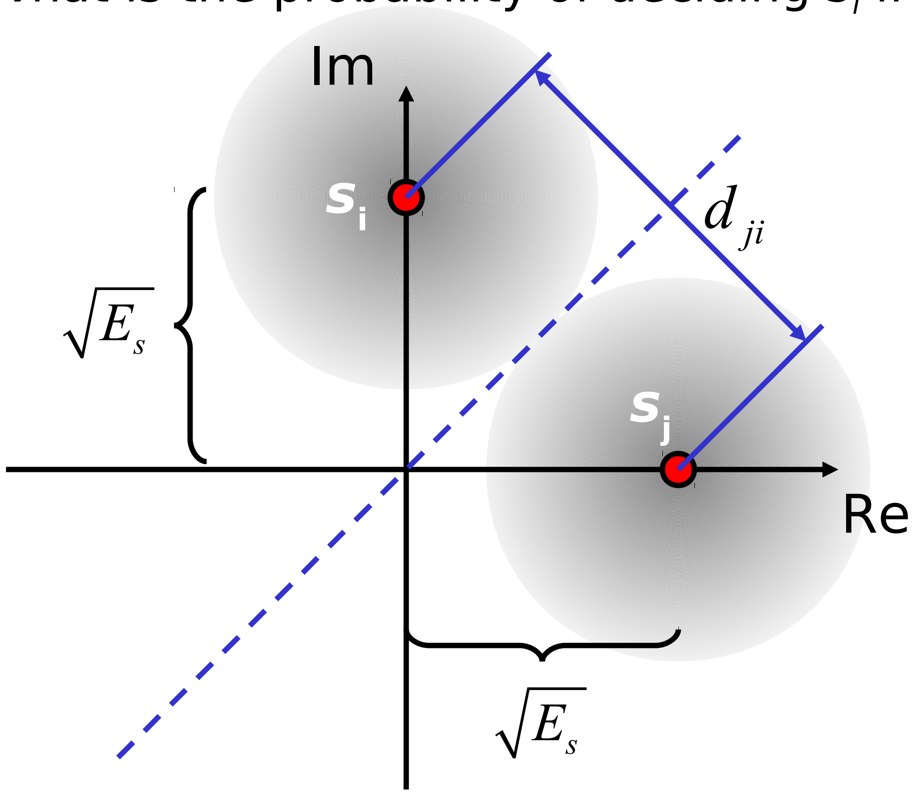
$$\mathrm{N}\left(0,\sigma^2\right) + j\mathrm{N}\left(0,\sigma^2\right)$$

with variance $\sigma^2 = N_0/2$ in each direction.

Fundamental question: What is the probability that we end up on the wrong side of the decision boundary?

Optimal receiver
Pair-wise symbol error probability

What is the probability of deciding s_i if s_j was transmitted?



We need the distance between the two symbols. In this orthogonal case:

$$d_{ji} = \sqrt{\sqrt{E_s}^2 + \sqrt{E_s}^2} = \sqrt{2E_s}$$

The probability of the noise pushing us across the boundary at distance $d_{ji} / 2$ is

$$\Pr\left(s_j \rightarrow s_i\right) = Q\left(\frac{d_{ji}/2}{\sqrt{N_0/2}}\right) = Q\left(\sqrt{\frac{E_s}{N_0}}\right)$$

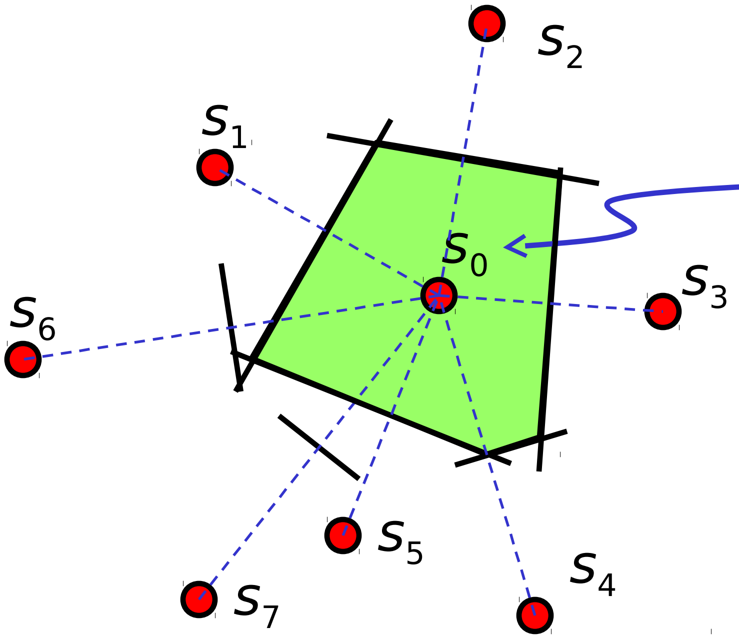
$$= \frac{1}{2}\operatorname{erfc}\left(\sqrt{\frac{E_s}{2N_0}}\right)$$

The book uses **erfc()** instead of **Q()**.

Optimal receiver
The union bound

Calculation of symbol error probability is simple for two signals!

When we have many signal alternatives, it may be impossible to calculate an exact symbol error rate.



When s_0 is the transmitted signal, an error occurs when the received signal is outside this polygon.

The UNION BOUND is the **sum of all pair-wise error probabilities**, and constitutes an upper bound on the symbol error probability.

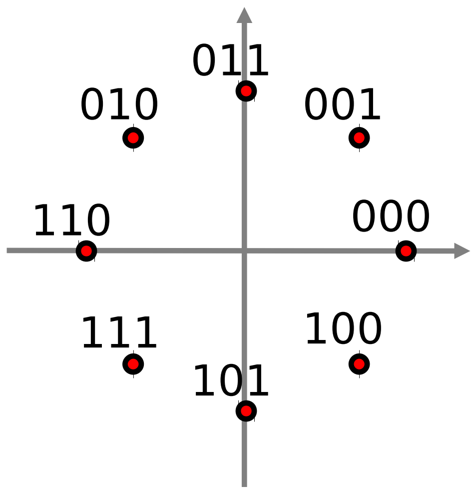
The higher the SNR, the better the approximation!

Optimal receiver
Symbol- and bit-error rates

The calculations so far have discussed the probabilities of selecting the incorrect signal alternative (symbol), i.e. the symbol-error rate.

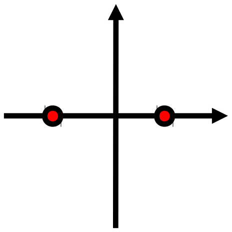
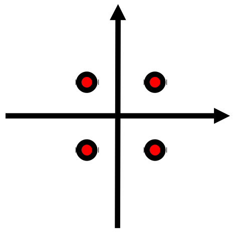
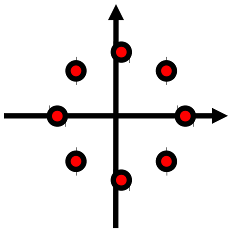
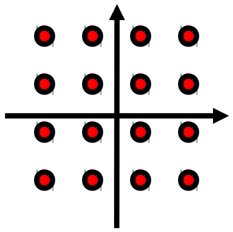
When each symbol carries K bits, we need 2^K symbols.

Gray coding is used to assigning bits so that the nearest neighbors only differ in one of the K bits. This minimizes the bit-error rate.



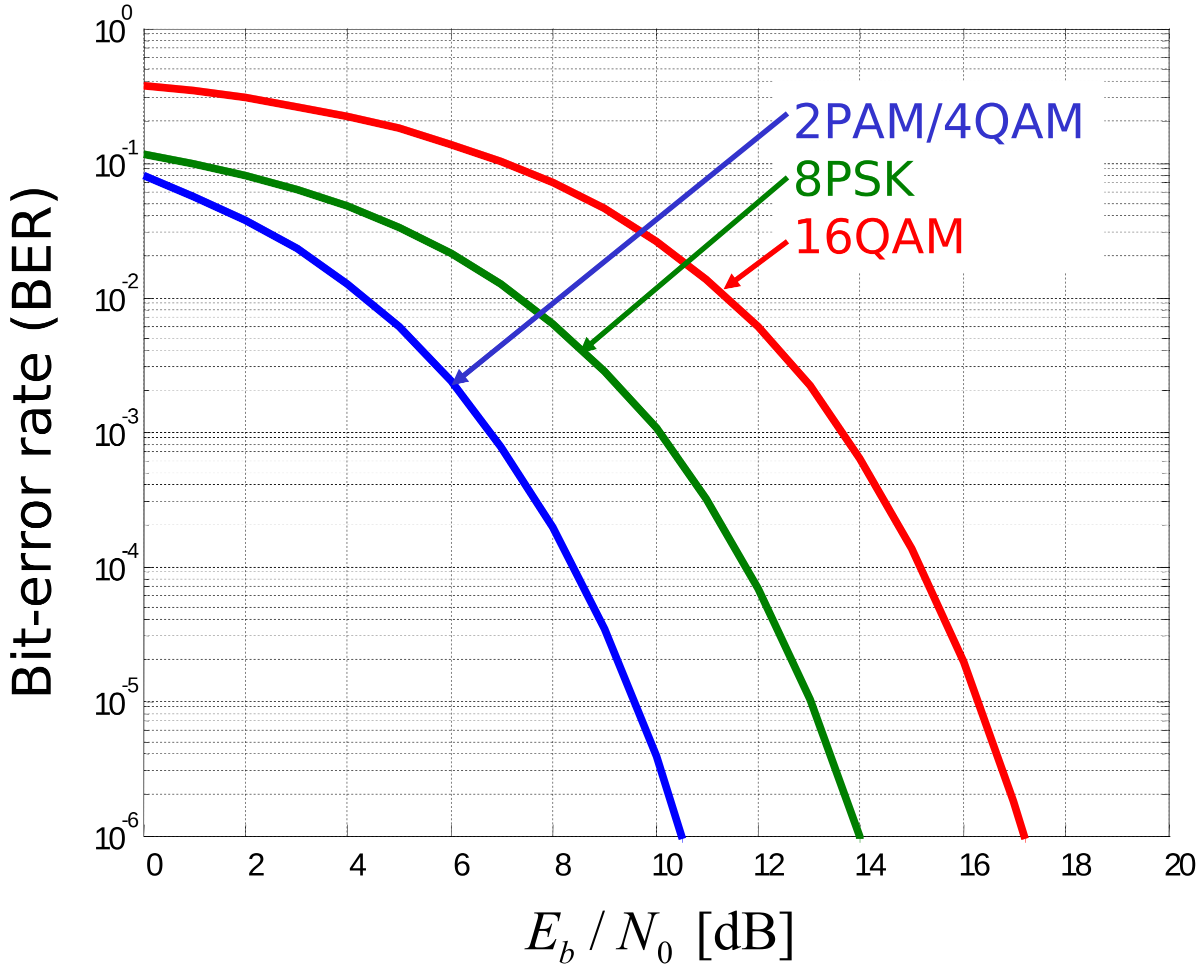
Gray-coded 8PSK

Optimal receiver
Bit-error rates (BER)

EXAMPLES:	2PAM	4QAM	8PSK	16QAM
				
Bits/symbol	1	2	3	4
Symbol energy	E_b	$2E_\mathrm{b}$	$3E_\mathrm{b}$	$4E_\mathrm{b}$
BER	$Q\left(\sqrt{\frac{2E_b}{N_0}}\right)$	$Q\left(\sqrt{\frac{2E_b}{N_0}}\right)$	$\sim\frac{2}{3}Q\left(\sqrt{0.87\frac{E_b}{N_0}}\right)$	$\sim\frac{3}{2}Q\left(\sqrt{\frac{E_{b,\max}}{2.25N_0}}\right)$

Gray coding is used when calculating these BER.

Optimal receiver
Bit-error rates (BER), cont.



Optimal receiver
Where do we get E_b and N_0?

Where do those magic numbers E_b and N_0 come from?

The noise power spectral density N_0 is calculated according to

$$N_0 = k T_0 F_0 \Leftrightarrow N_{0|\mathrm{dB}} = -204 + F_{0|\mathrm{dB}}$$

where F_0 is the noise factor of the "equivalent" receiver noise source.

The bit energy E_b can be calculated from the received power C (at the **same** reference point as N_0). Given a certain data-rate d_b [bits per second], we have the relation

$$E_b = C / d_b \Leftrightarrow E_{b|\mathrm{dB}} = C_{|\mathrm{dB}} - d_{b|\mathrm{dB}}$$

THESE ARE THE EQUATIONS THAT RELATE DETECTOR PERFORMANCE ANALYSIS TO LINK BUDGET CALCULATIONS!

Optimal receiver
What about fading channels?

We have (or can calculate) BER expressions for non-fading AWGN channels.

If the channel is Rayleigh-fading, then E_b/N_0 will have an exponential distribution (N_0 is assumed to be constant)

$$pdf\left(\gamma_b\right) = \frac{1}{\overline{\gamma_b}} e^{-\gamma_b/\overline{\gamma_b}}$$

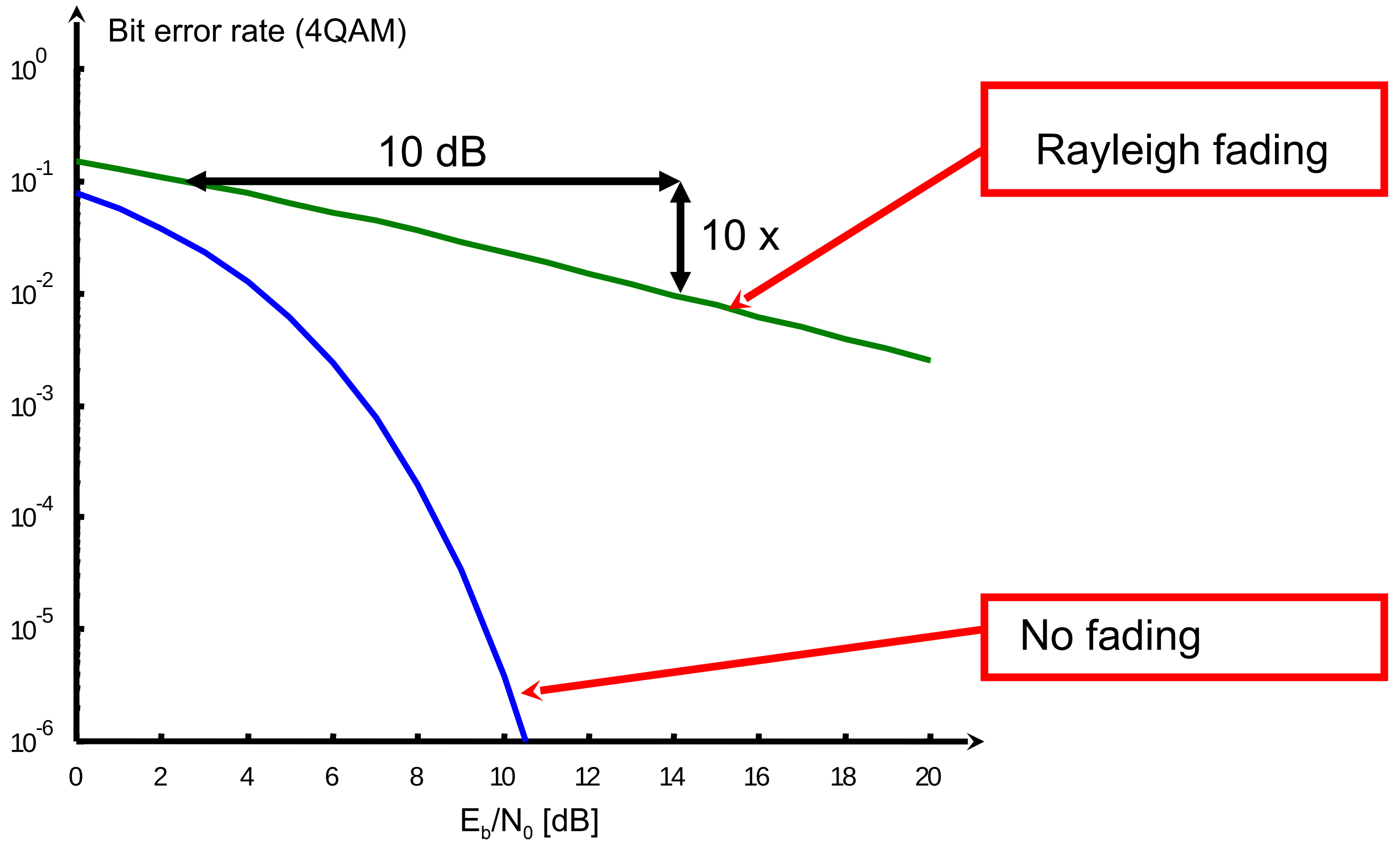
γ_b	-- E_b/N_0
$\overline{\gamma_b}$	-- average E_b/N_0

The BER for the Rayleigh fading channel is obtained by averaging:

$$BER_{\mathrm{Rayleigh}}\left(\overline{\gamma_b}\right) = \int_0^\infty BER_{\mathrm{AWGN}}\left(\gamma_b\right) \times pdf\left(\gamma_b\right) d\gamma_b$$

Optimal receiver
What about fading channels?

THIS IS A SERIOUS PROBLEM!



DIVERSITY ARRANGEMENTS

Diversity arrangements
Let’s have a look at fading again

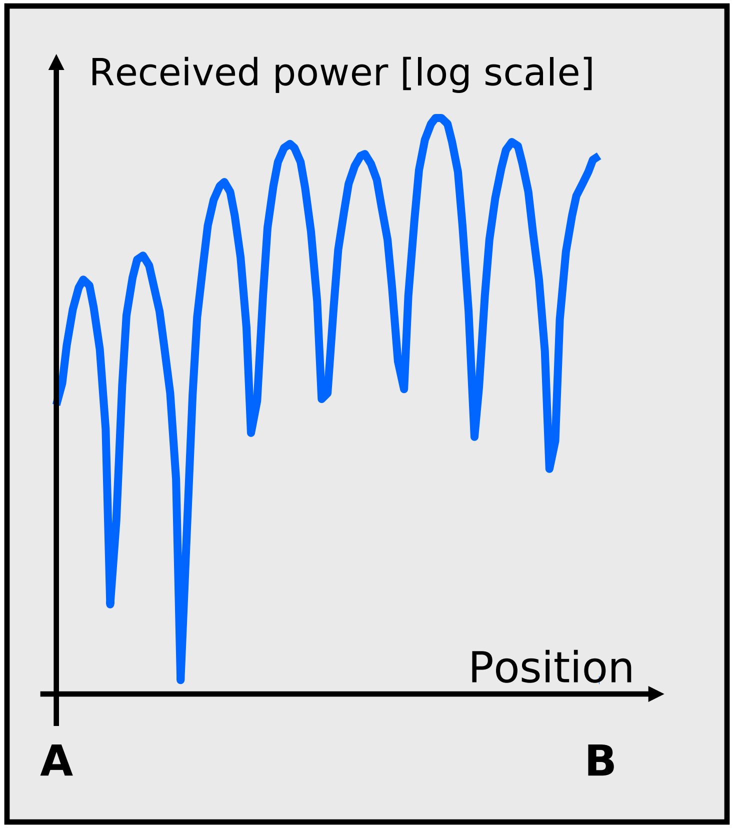
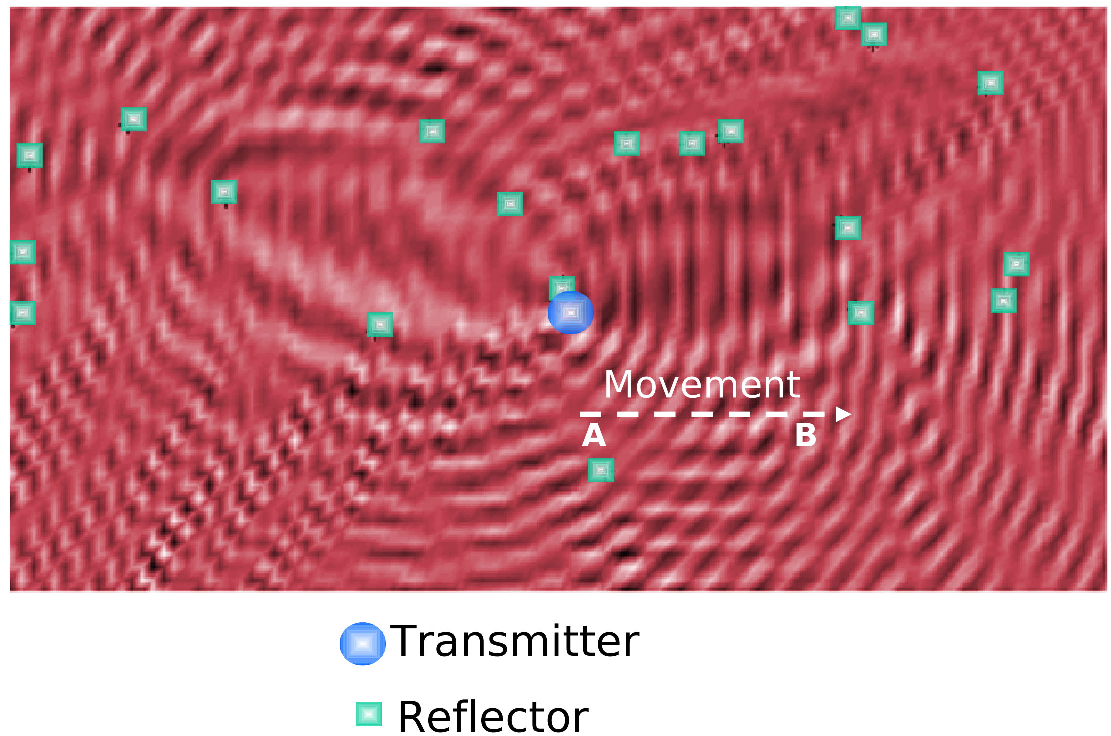


Illustration of interference pattern from above



Having TWO separated antennas in this case may increase the probability of receiving a strong signal on at least one of them.

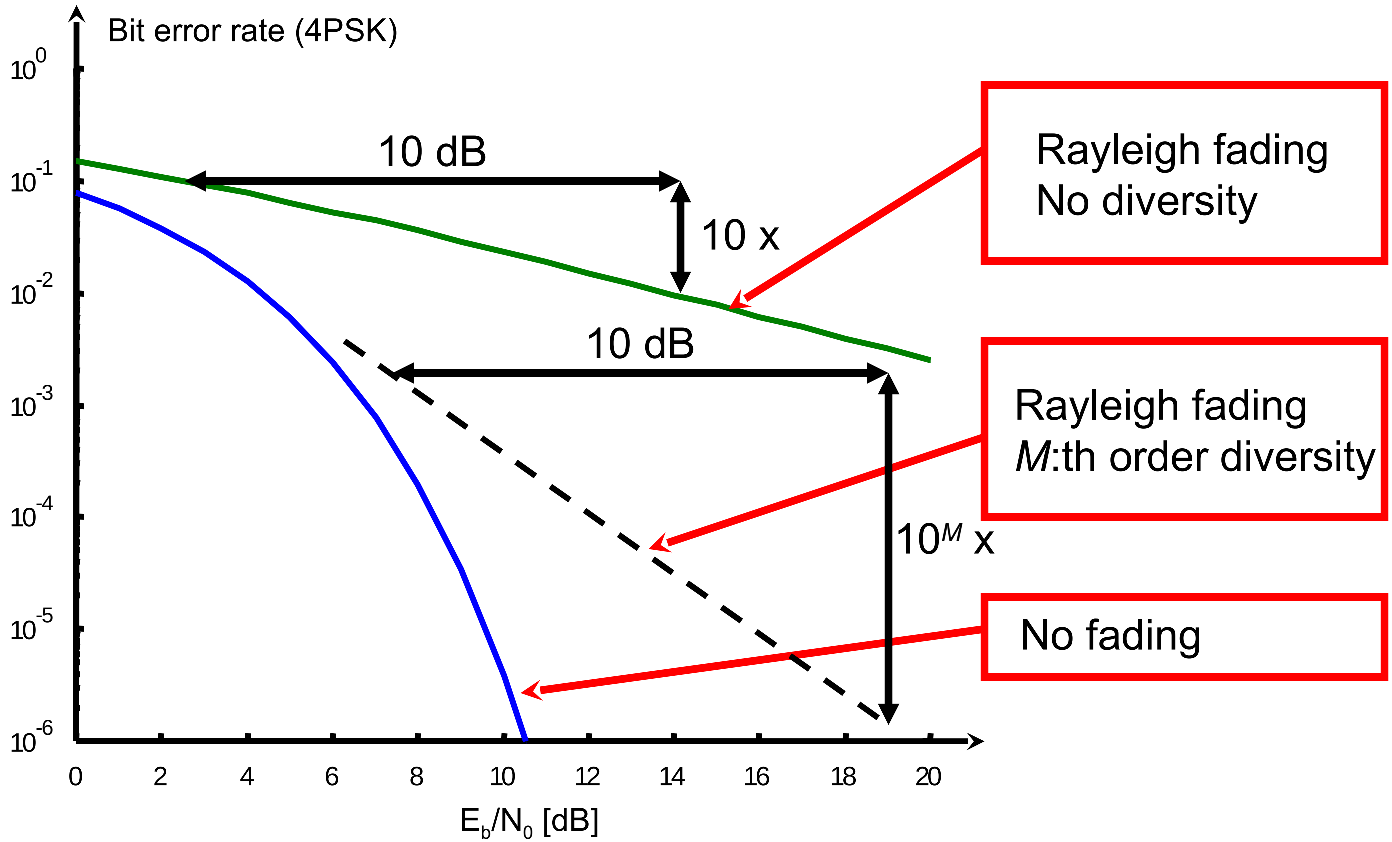
Diversity arrangements
The diversity principle

The principle of diversity is to transmit the same information on M statistically independent channels.

By doing this, we increase the chance that the information will be received properly.

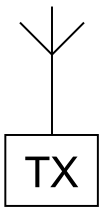
The example given on the previous slide is one such arrangement: antenna diversity.

Diversity arrangements General improvement trend

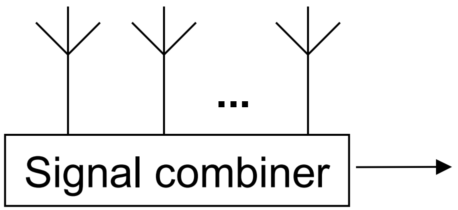


Diversity arrangements
Some techniques

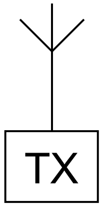
Spatial (antenna) diversity

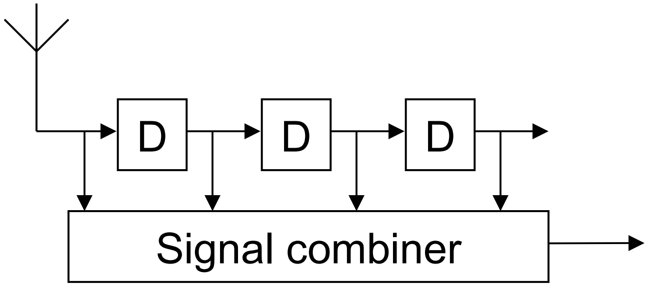


We will focus on this one today!



Frequency diversity





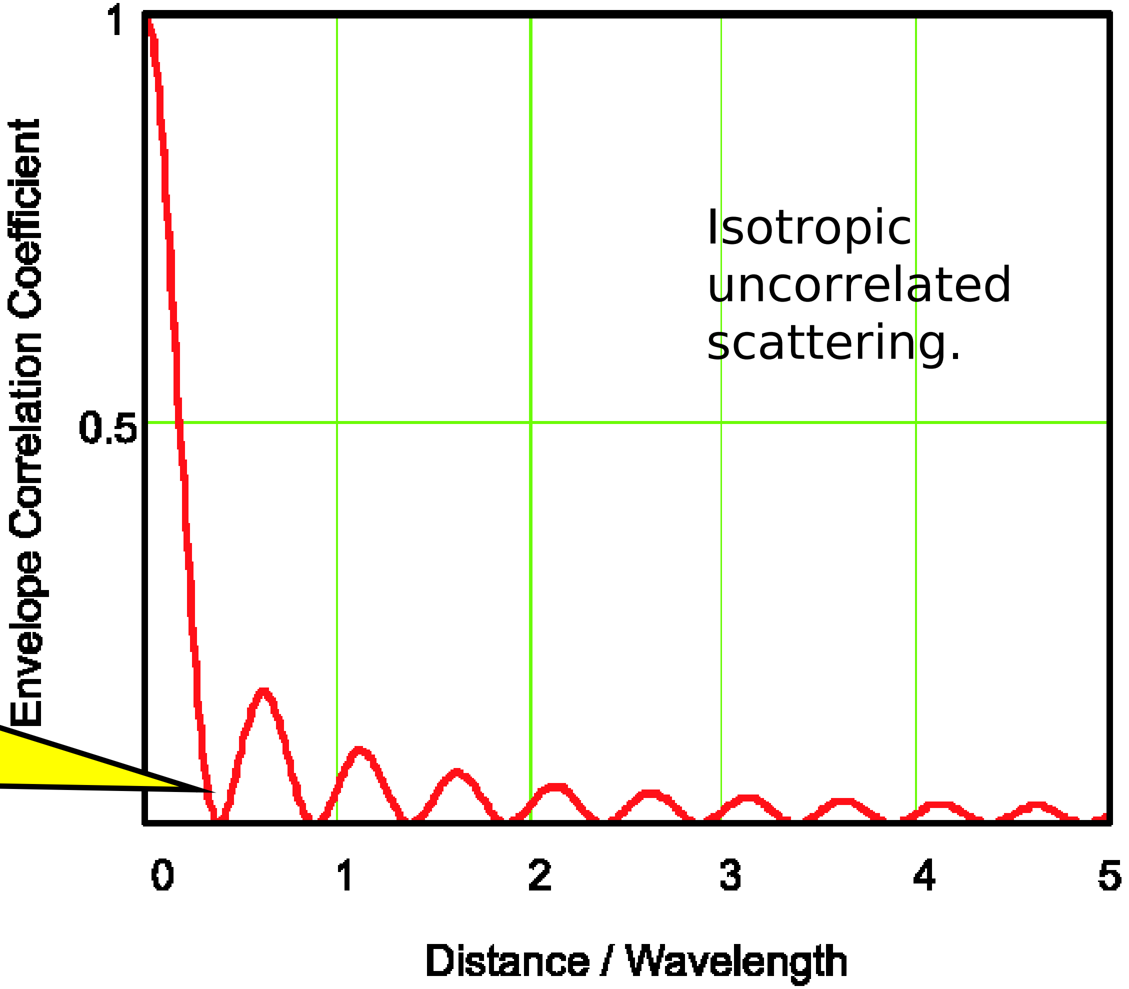
Temporal diversity

(We also have angular and polarization diversity)

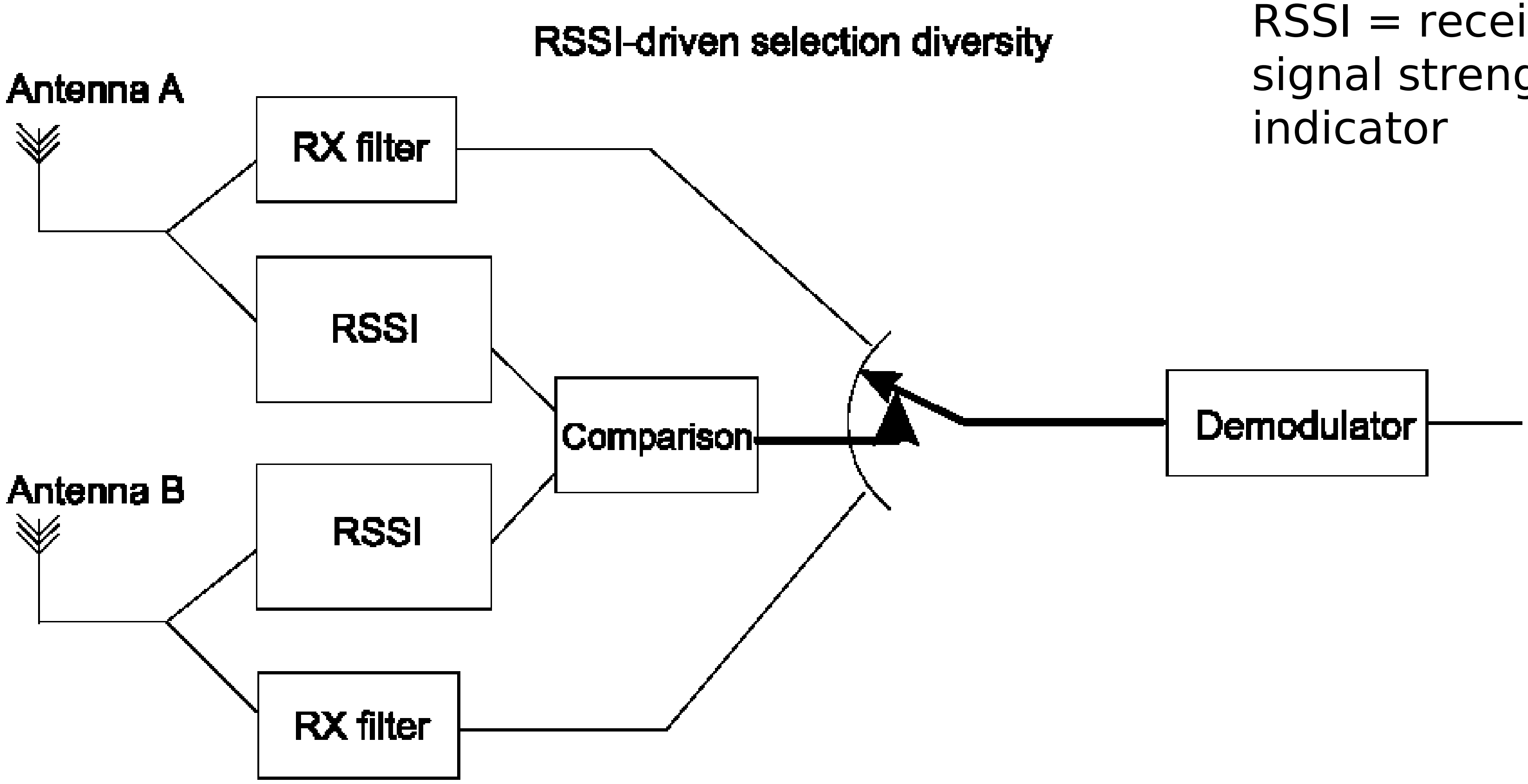
Spatial (antenna) diversity
Fading correlation on antennas

With several antennas, we want the fading on them to be as independent as possible.

E.g.: An antenna spacing of about 0.4 wavelength gives zero correlation.

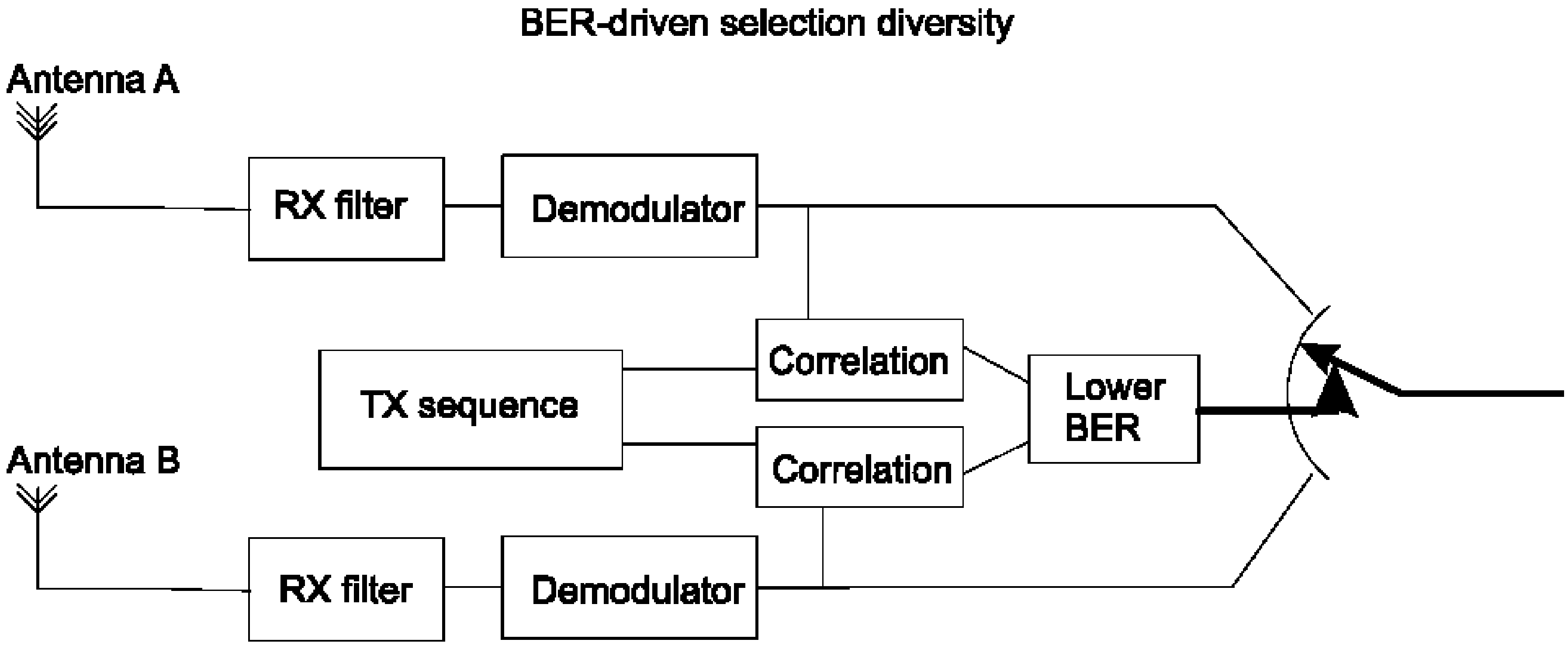


Spatial (antenna) diversity
Selection diversity



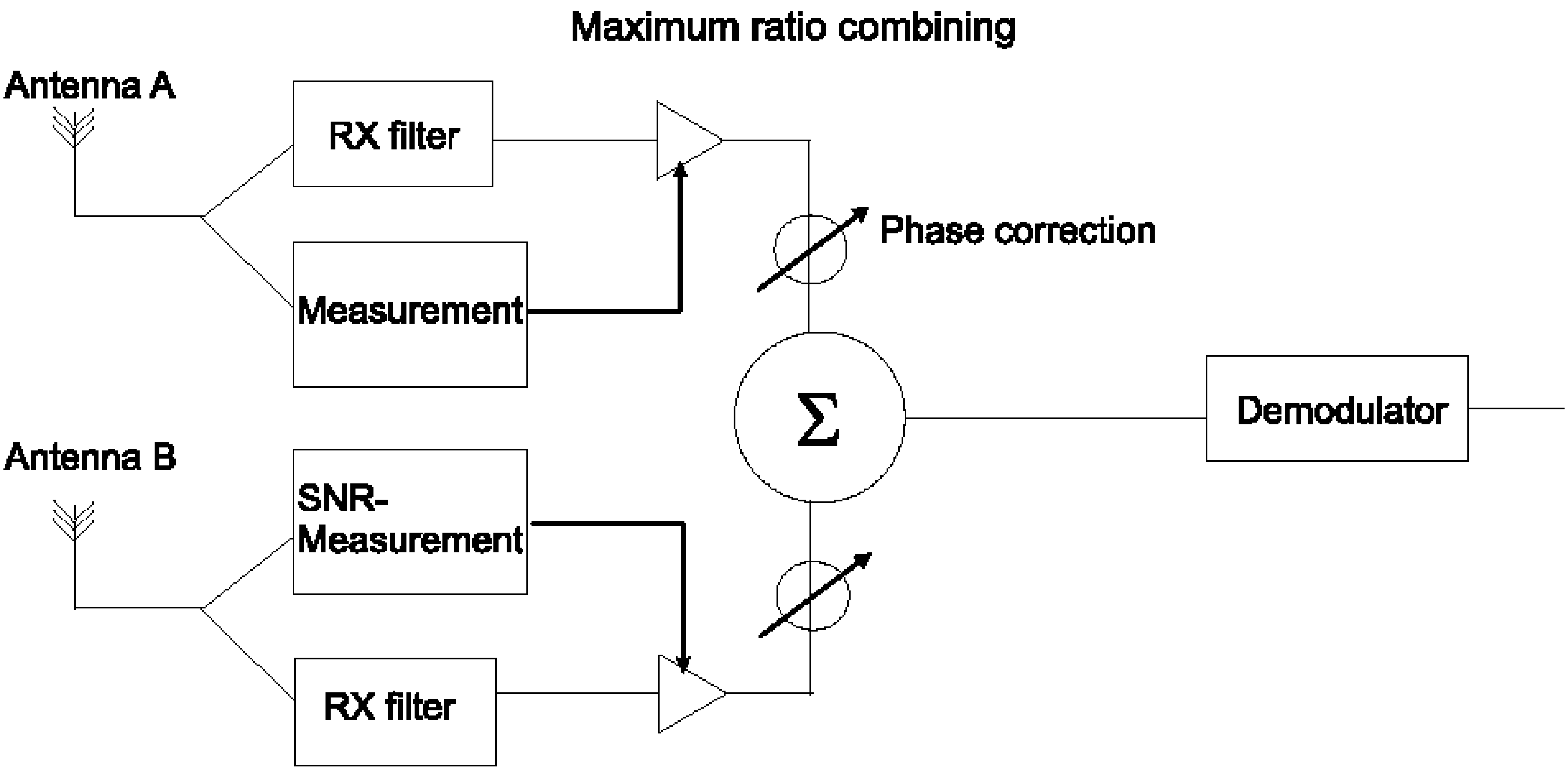
RSSI = received signal strength indicator

Spatial (antenna) diversity
Selection diversity, cont.



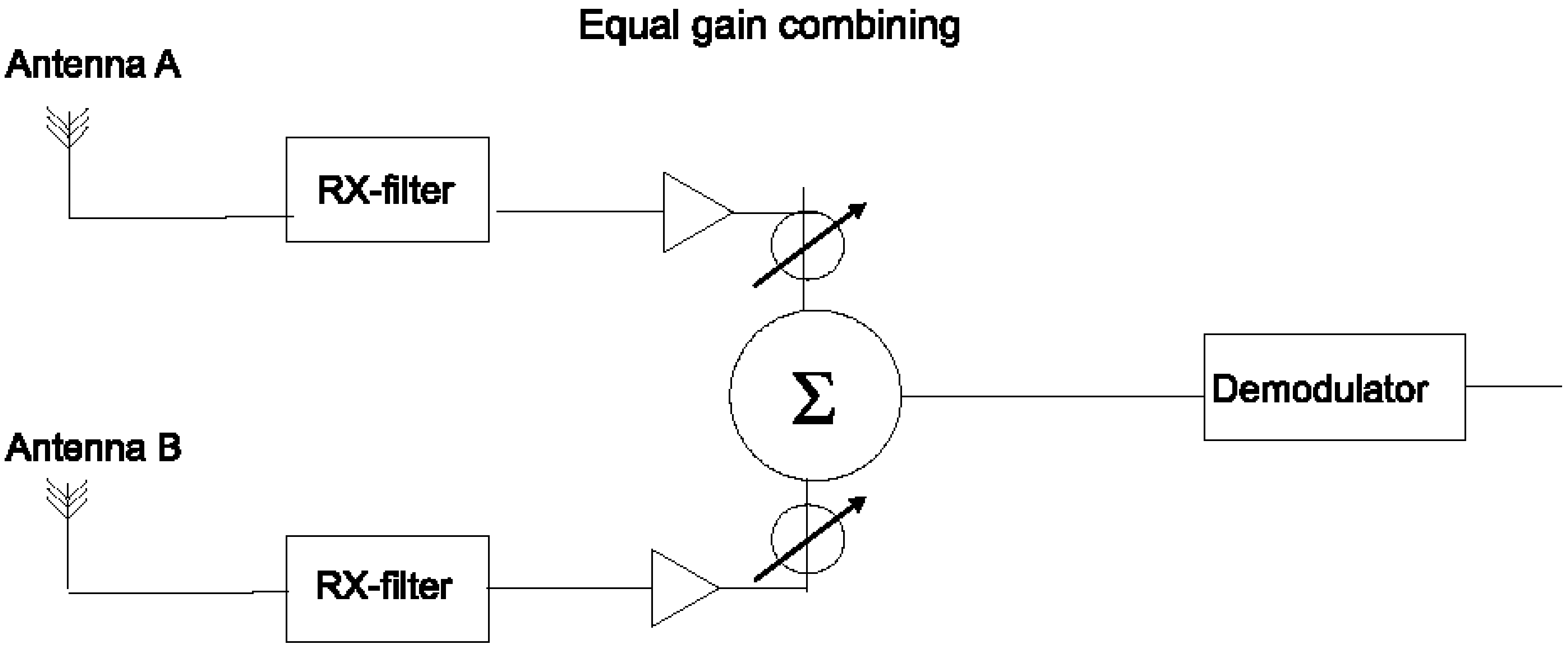
By measuring BER instead of RSSI, we have a better guarantee that we obtain a low BER.

Spatial (antenna) diversity Maximum ratio combining



This is the optimal way (SNR sense) of combining antennas.

Spatial (antenna) diversity

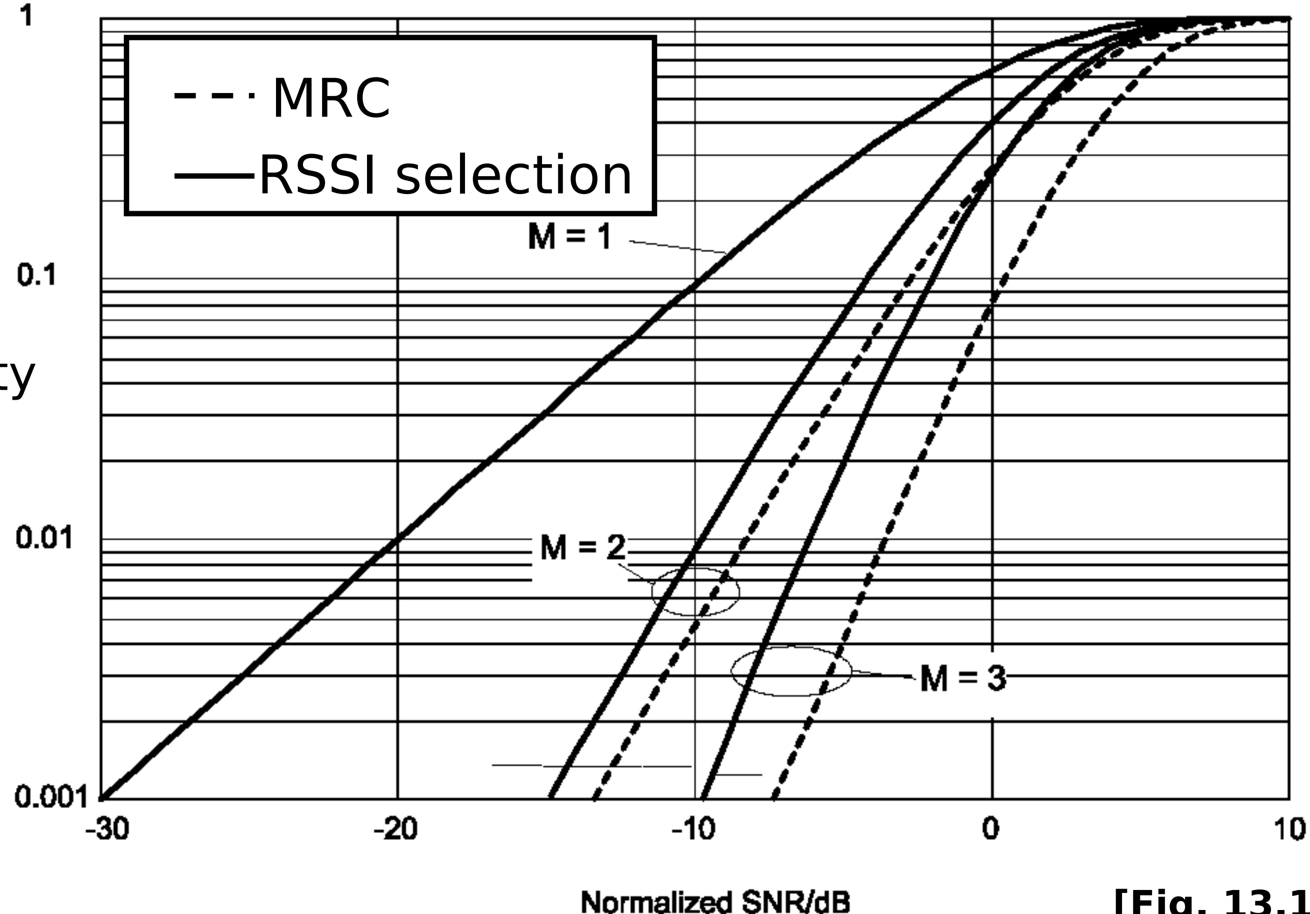


Simpler than MRC, but almost the same performance.

Spatial (antenna) diversity Performance comparison

Cumulative distribution of SNR

Comparison of SNR distribution for different number of antennas *M* and two different diversity techniques.

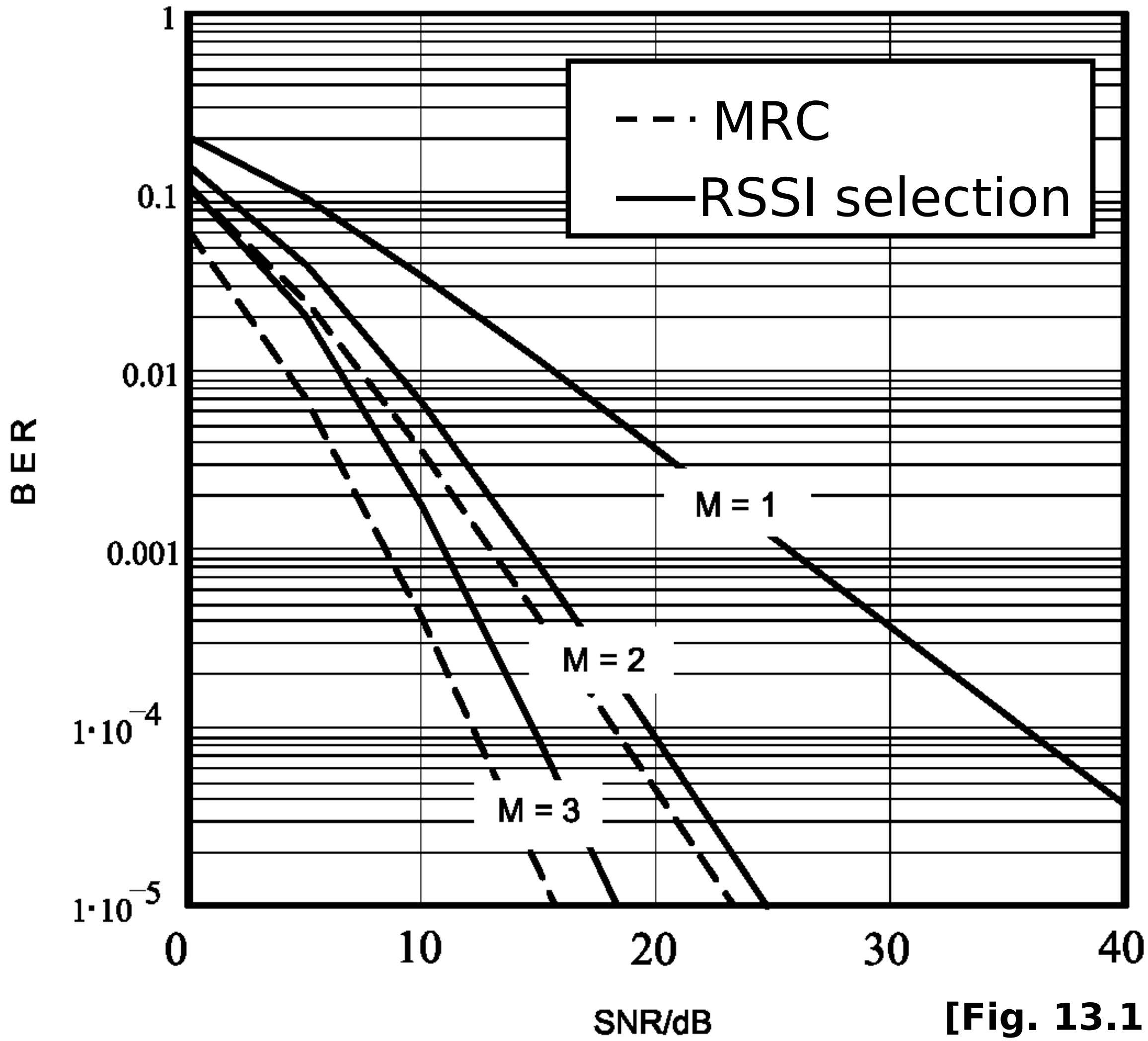


[Fig. 13.10]

These curves can be used to calculate fading margins.

Spatial (antenna) diversity Performance comparison, cont.

Comparison of 2ASK/2PSK BER for different number of antennas *M* and two different diversity techniques.



[Fig. 13.11]

Summary

- Optimal (**maximum likelihood**) receiver in AWGN channels
- Interpretation of received signal as a point in a **signal space**
- Euclidean distances between symbols determine the **probability of symbol error**
- **Bit error rate** (BER) calculations for some signal constellations
- **Union bound** (better at high SNRs) can be to derive approximate BER expressions
- **Fading** leads to serious BER problems
- **Diversity** is used to combat fading
- Focus on **spatial (antenna) diversity**
- Performance comparisons for **RSSI selection** and **maximum ratio combining** diversity.