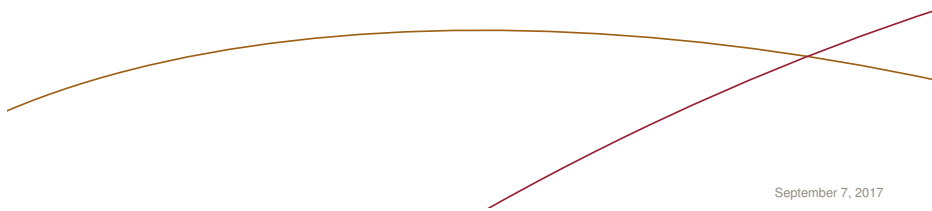


# EITG05 – Digital Communications

## Week 2, Lecture 2

### Bandwidth of Transmitted Signals

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Thursday, September 7, 2017



September 7, 2017

## Fourier transform

$$\begin{aligned} X(f) &= \mathcal{F}\{x(t)\} = \int_{-\infty}^{\infty} x(t) e^{-j2\pi f t} dt \\ &= X_{Re}(f) + j X_{Im}(f) \\ &= |X(f)| e^{j\phi(f)} \end{aligned}$$

$$\begin{aligned} x(t) &= \mathcal{F}^{-1}\{X(f)\} = \int_{-\infty}^{\infty} X(f) e^{+j2\pi f t} df \\ &= \int_{-\infty}^{\infty} |X(f)| e^{+j(2\pi f t + \phi(f))} df \end{aligned}$$

## Week 2, Lecture 2

### Chapter 2: Model of a Digital Communication System

- ▶ 2.5 The bandwidth of the transmitted signal
  - 2.5.5  $R(f)$ :  $M$ -ary PAM signals
  - 2.5.6  $R(f)$ :  $M$ -ary QAM signals
  - 2.5.7  $R(f)$ : OFDM-type of signals
  - 2.5.8  $R(f)$ :  $M$ -ary FSK signals

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**Exercises:** 2.21a,b, 2.22, 2.23, 2.25, 2.29



Michael Lentmaier, Fall 2017

Digital Communications: Week 2, Lecture 2

## Some useful Fourier transform properties

$g(at) \leftrightarrow \frac{1}{ a } G(f/a)$	$g^*(T-t) \leftrightarrow G^*(f)e^{-j2\pi f T}$
$g(-t) \leftrightarrow G(-f)$	$\delta(t) \leftrightarrow 1$
$G(t) \leftrightarrow g(-f)$	$1(dc) \leftrightarrow \delta(f)$
$g(t-t_0) \leftrightarrow G(f)e^{-j2\pi f t_0}$	$e^{j2\pi f c t} \leftrightarrow \delta(f-f_c)$
$g(t)e^{j2\pi f_c t} \leftrightarrow G(f-f_c)$	$\cos(2\pi f_c t) \leftrightarrow \frac{1}{2} (\delta(f+f_c) + \delta(f-f_c))$
$\frac{d}{dt} g(t) \leftrightarrow j2\pi f G(f)$	$\sin(2\pi f_c t) \leftrightarrow \frac{j}{2} (\delta(f+f_c) - \delta(f-f_c))$
$g^*(t) \leftrightarrow G^*(-f)$	$\alpha e^{-\pi\alpha^2 t^2} \leftrightarrow e^{-\pi f^2 / \alpha^2}$

→ full list in Appendix C of the compendium

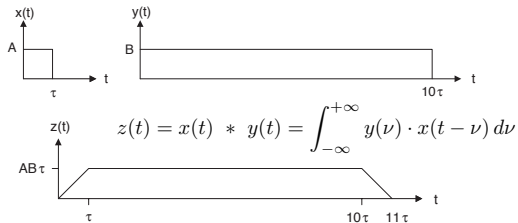


## Some useful Fourier transform properties

- Consider two signals  $x(t)$  and  $y(t)$  and their Fourier transforms

$$x(t) \longleftrightarrow X(f), \quad y(t) \longleftrightarrow Y(f)$$

- Recall the **convolution** operation  $z(t) = x(t) * y(t)$ :



- Filtering:**

$$x(t) * y(t) \longleftrightarrow X(f) \cdot Y(f)$$

- Multiplication:**

$$x(t) \cdot y(t) \longleftrightarrow X(f) * Y(f)$$



## Spectrum of time-limited signals

- Consider some **time-limited** signal  $s_T(t)$  of duration  $T$ , with  $s_T(t) = 0$  for  $t < 0$  and  $t > T$
- Assume that within the interval  $0 \leq t \leq T$ , the signal  $s_T(t)$  is equal to some signal  $s(t)$ , i.e.,

$$s_T(t) = s(t) \cdot g_{rec}(t),$$

where  $g_{rec}(t)$  is the **rectangular pulse** of amplitude  $A = 1$

- Taking the Fourier transform on both sides we get

$$S_T(f) = S(f) * G_{rec}(f) = S(f) * AT \frac{\sin(\pi f T)}{\pi f T} e^{-j\pi f T}$$

- Since  $G_{rec}(f)$  is **unlimited** along the frequency axis, this is the case for  $S_T(f)$  as well (convolution increases length)

Time-limited signals can never be strictly band-limited



## Some definitions of bandwidth

- Main-lobe definition:**

$W_{lobe}$  is defined by the width of the main-lobe of  $R(f)$   
This is how we have defined bandwidth in previous examples

- In **baseband** we use the **one-sided** width, while in **bandpass** applications the **two-sided** width is used (positive frequencies)

- Percentage definition:**

$W_{99}$  is defined according to the location of 99% of the power

- For bandpass signals  $W_{99}$  is found as the value that satisfies

$$\int_{f_c - W_{99}/2}^{f_c + W_{99}/2} R(f) df = 0.99 \int_0^{\infty} R(f) df$$

- Other percentages can be used as well:  $W_{90}$ ,  $W_{99.9}$

- Nyquist bandwidth**

Assuming an ideal pulse with finite bandwidth (see Chapter 6)

$$W_{nyq} = \frac{R_s}{2} \text{ [Hz]}$$



## Some definitions of bandwidth

Pulse shape	$W_{lobe}$	% power in $W_{lobe}$	$W_{90}$	$W_{99}$	$W_{99.9}$	Asymptotic decay
rec	$2/T$	90.3	$1.70/T$	$20.6/T$	$204/T$	$f^{-2}$
tri	$4/T$	99.7	$1.70/T$	$2.60/T$	$6.24/T$	$f^{-4}$
hcs	$3/T$	99.5	$1.56/T$	$2.36/T$	$5.48/T$	$f^{-4}$
rc	$4/T$	99.95	$1.90/T$	$2.82/T$	$3.46/T$	$f^{-6}$
Nyquist	$R_s$	100	$0.9R_s$	$0.99R_s$	$0.999R_s$	ideal

Table 2.1: Double-sided bandwidth results for power spectral densities according to (2.212). The  $g_{rec}(t)$ ,  $g_{tri}(t)$ ,  $g_{hcs}(t)$  and  $g_{rc}(t)$  pulse shapes are defined in Appendix D, and  $T$  denotes the duration of the pulse. The Nyquist pulse shape is not limited in time and it is defined in (D.49) with parameters  $\beta = 0$  and  $T = T_s$ .

- This table is useful for **PAM**, **PSK**, and **QAM** constellations
- Except bandwidth  $W$ , the **asymptotic decay** is also relevant



## From last lecture: general $R(f)$

- ▶ The power spectral density  $R(f)$  can be divided into a **continuous part**  $R_c(f)$  and a **discrete part**  $R_d(f)$

$$R(f) = R_c(f) + R_d(f)$$

- ▶ The general expression for the continuous part is

$$\begin{aligned} R_c(f) &= \frac{1}{T_s} \sum_{n=0}^{M-1} P_n |S_n(f) - A(f)|^2 \\ &= \left( \frac{1}{T_s} \sum_{n=0}^{M-1} P_n |S_n(f)|^2 \right) - \frac{|A(f)|^2}{T_s} \end{aligned}$$

- ▶ For the discrete part we have

$$R_d(f) = \frac{|A(f)|^2}{T_s^2} \sum_{n=-\infty}^{\infty} \delta(f - n/T_s)$$



## $R(f)$ : $M$ -ary PAM signals

- ▶ With  $M$ -ary PAM signaling we have

$$s_\ell = A_\ell g(t), \quad \ell = 0, 1, \dots, M-1$$

- ▶ Then

$$S_\ell(f) = A_\ell G(f), \quad \text{and} \quad A(f) = \sum_{\ell=0}^{M-1} P_\ell A_\ell G(f)$$

- ▶ With this we obtain the **simplified expression**

$$R(f) = \frac{\sigma_A^2}{T_s} |G(f)|^2 + \frac{m_A^2}{T_s^2} |G(f)|^2 \sum_{n=-\infty}^{\infty} \delta(f - n/T_s),$$

where  $m_A$  denotes the **mean** and  $\sigma_A^2 = \bar{E}_s/E_g - m_A^2$  the **variance** of the amplitudes  $A_\ell$

- ▶ Assuming **zero average amplitude**  $m_A = 0$  and using  $\bar{P} = \sigma_A^2 E_g R_s$  this reduces to

$$R(f) = R_c(f) = \frac{\sigma_A^2}{T_s} |G(f)|^2 = \frac{\bar{P}}{E_g} |G(f)|^2$$



## Example 2.28

Assume the bit rate  $R_b = 9600$  [bps],  $M$ -ary PAM transmission and that  $m_A = 0$ . Determine the (baseband) bandwidth  $W$ , defined as the one-sided width of the mainlobe of the power spectral density  $R(f)$ , if  $M = 2$ ,  $M = 4$  and  $M = 8$ , respectively. Furthermore, assume a rectangular pulse shape with amplitude  $A_g$ , and duration  $T = T_s$ . Calculate also the bandwidth efficiency  $\rho$ .

- ▶ What is  $W$  for a given pulse shape and different  $M$ ?
- ▶ Using  $T = T_s$ ,  $m_A = 0$  and  $g(t) = g_{rec}(t)$ , we have

$$R(f) = \frac{\sigma_A^2}{T_s} |G_{rec}(f)|^2$$

- ▶ For the given pulse we get  $W = 1/T_s$ , where  $T_s = k T_b$

$$k = 1 \Rightarrow M = 2 \Rightarrow W = 9600[\text{Hz}]$$

$$k = 2 \Rightarrow M = 4 \Rightarrow W = 4800[\text{Hz}]$$

$$k = 3 \Rightarrow M = 8 \Rightarrow W = 3200[\text{Hz}]$$

- ▶ Bandwidth efficiency:  $\rho = R_b/W = k T_b/T_b = k$



## What does bandwidth efficiency tell us?

In the previous example we had a **bandwidth efficiency** of

$$\rho = \frac{R_b}{W} = k$$

### Saving bandwidth

- ▶ The previous example showed that the **bandwidth**  $W$  can be **reduced by increasing**  $M$
- ▶  $T = T_s = k T_b$  increases with  $M$
- ▶  $W = 1/T = R_b/k$  decreases accordingly

### Improving bit rate

- ▶ Assume instead that the **bandwidth**  $W$  is **fixed** in the same example, i.e., the symbol duration  $T_s = T$  is fixed
- ▶ Then  $R_b = k W$  increases with  $M$
- ▶ Assume for example  $W = 1$  MHz:
  - $R_b = 1$  Mbps if  $M = 2$  ( $k = 1$ )
  - $R_b = 10$  Mbps if  $M = 1024$  ( $k = 10$ )



## $R(f)$ : $M$ -ary QAM signals

- ▶ With  $M$ -ary QAM signaling the signal alternatives are

$$s_\ell(t) = A_\ell g(t) \cos(2\pi f_c t) - B_\ell g(t) \sin(2\pi f_c t), \quad \ell = 0, 1, \dots, M-1$$

- ▶ Then the Fourier transform becomes

$$\begin{aligned} S_\ell(f) &= A_\ell \frac{G(f+f_c) + G(f-f_c)}{2} - j B_\ell \frac{G(f+f_c) - G(f-f_c)}{2} \\ &= (A_\ell - j B_\ell) \frac{G(f+f_c)}{2} + (A_\ell + j B_\ell) \frac{G(f-f_c)}{2} \end{aligned}$$

- ▶ Assuming a **zero average signal**  $a(t) = 0$  and  $f_c T \geq 1$  this simplifies to

$$R(f) = R_c(f) = \bar{P} \frac{|G(f+f_c)|^2 + |G(f-f_c)|^2}{2E_g}$$



## $R(f)$ : $M$ -ary QAM signals

- ▶ Remember that  $M$ -ary QAM signals contain  $M$ -ary PSK and  $M$ -ary bandpass PAM signals as special cases:

$$\text{BP-PAM: } B_\ell = 0$$

$$\text{PSK: } A_\ell = \cos(v_\ell), \quad B_\ell = \sin(v_\ell)$$

- ▶  $\Rightarrow$  our results for  $R(f)$  of  $M$ -ary QAM signals include these cases
- ▶ For **symmetric constellations**, such that  $a(t) = 0$ , the simplified version applies
- ▶ The bandwidth  $W$  is determined by  $|G(f-f_c)|^2$  and hence the two-sided main-lobe of  $|G(f)|^2$

$\Rightarrow$  if the same pulse  $g(t)$  is used then  $M$ -ary QAM,  $M$ -ary bandpass PAM and  $M$ -ary PSK have the same bandwidth  $W$



## Example

Bandwidth consumption for BPSK, QPSK and 16-QAM assuming equal  $R_b$  and  $f_c = 100R_b$

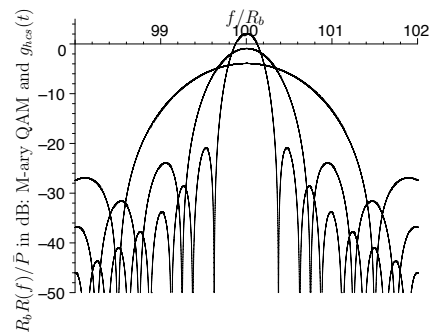


Figure 2.20: The power spectral density for binary QAM (BPSK, widest main-lobe), 4-ary QAM (QPSK), and 16-ary QAM (smallest main-lobe). The figure shows  $10 \log_{10}(R_b R(f)/\bar{P})$  [dB] in the frequency interval  $98R_b \leq f \leq 102R_b$ . The carrier frequency is  $f_c = 100R_b$  [Hz], and a  $T_s = kT_b$  long  $g_{hcs}(t)$  pulse is assumed. See also (2.227) and (2.230).



## $R(f)$ : $M$ -ary FSK signals

- ▶ With  $M$ -ary **frequency shift keying** (FSK) signaling the signal alternatives are

$$s_\ell(t) = A \cos(2\pi f_\ell t + v), \quad 0 \leq t \leq T_s$$

- ▶ Choosing  $v = -\pi/2$  this can be written as

$$s_\ell(t) = g_{rec}(t) \sin(2\pi f_\ell t), \quad \text{with } T = T_s,$$

since  $s_\ell(t) = 0$  outside the symbol interval

- ▶ The Fourier transform is then

$$S_\ell(f) = j \frac{G_{rec}(f+f_c) - G_{rec}(f-f_c)}{2}$$

- ▶ The **exact** power spectral density  $R(f)$  can now be computed by the general formula (2.202)–(2.204)



## $R(f)$ : $M$ -ary FSK signals

- Let us find an **approximate** expression for the FSK bandwidth  $W$
- Assume that

$$f_\ell = f_0 + \ell f_\Delta, \quad \ell = 0, \dots, M-1$$

- Then the bandwidth  $W$  can be approximated by

$$W \approx R_s + f_{M-1} - f_0 + R_s = (M-1)f_\Delta + 2R_s$$

- Consider now **orthogonal** FSK with  $f_\Delta = I \cdot R_s/2$  for some  $I > 0$
- The **bandwidth efficiency** is then

$$\rho = \frac{R_b}{W} \approx \frac{R_b}{(M-1)f_\Delta + 2R_s} = \frac{R_b}{((M-1)I/2 + 2)R_s} = \frac{\log_2 M}{(M-1)I/2 + 2}$$

**Observe:** the bandwidth efficiency of orthogonal  $M$ -ary FSK gets small if  $M$  is large

Last week we saw:  $M$ -ary FSK has good energy and Euclidean distance properties  $\Rightarrow$  trade-off



## Example 2.36

Assume that orthogonal  $M$ -ary FSK is used to communicate digital information in the frequency band  $1.1 \leq f \leq 1.2$  [MHz].

For each  $M$  below, find the largest bit rate that can be used (use bandwidth approximations):

- i)  $M = 2$     ii)  $M = 4$     iii)  $M = 8$     iv)  $M = 16$     v)  $M = 32$

Which of the  $M$ -values above give a higher bit rate than the  $M = 2$  case?

**Solution:**

It is given that  $W_{M\text{-FSK}} = 100$  [kHz]. From (2.245), the largest bit rate is obtained with  $I = 1$ :

$$R_b \approx 10^5 \cdot \frac{\log_2(M)}{(M-1)/2 + 2}$$

$M$	$\frac{\log_2(M)}{(M-1)/2 + 2}$	$R_b$
2	$\frac{1}{5/2} = 0.4$	40 kbps
4	$\frac{2}{7/2} = \frac{4}{7} \approx 0.5714$	$\approx 57$ kbps
8	$\frac{3}{11/2} = \frac{6}{11} \approx 0.5455$	$\approx 55$ kbps
16	$\frac{4}{19/2} = \frac{8}{19} \approx 0.4211$	$\approx 42$ kbps
32	$\frac{5}{35/2} = \frac{10}{35} \approx 0.2857$	$\approx 29$ kbps

From this table it is seen that  $M = 4, 8, 16$  give a higher bit rate than  $M = 2$ . □



## $R(f)$ : OFDM-type signals

- An **OFDM symbol** (signal alternative)  $x(t)$  can be modeled as a superposition of  $N$  **orthogonal QAM signals**, each carrying  $k_n$  bits, that are transmitted at different frequencies (sub-carriers)

$$x(t) = \sum_{n=0}^{N-1} s_{n,QAM}(t)$$

- Assuming each QAM signal has **zero mean** and that the different carriers have **independent bit streams** we get

$$R(f) = R_c(f) = R_s E\{|X(f)|^2\} = \sum_{n=0}^{N-1} R_n(f)$$

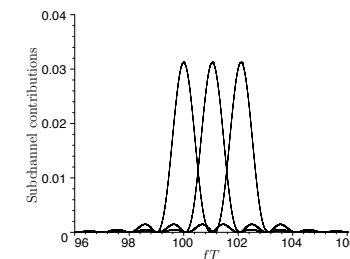
- Using our previous results for QAM in each sub-carrier we get

$$R(f) = R_c(f) = \sum_{n=0}^{N-1} \bar{P} \frac{|G(f+f_c)|^2 + |G(f-f_c)|^2}{2E_g}$$



## $R(f)$ : OFDM-type signals

Illustration of  $R_n(f)$  contributed by three neighboring sub-carriers:



- Assuming  $f_n = f_0 + n/(T_s - \Delta_h)$  we can **estimate** the bandwidth as

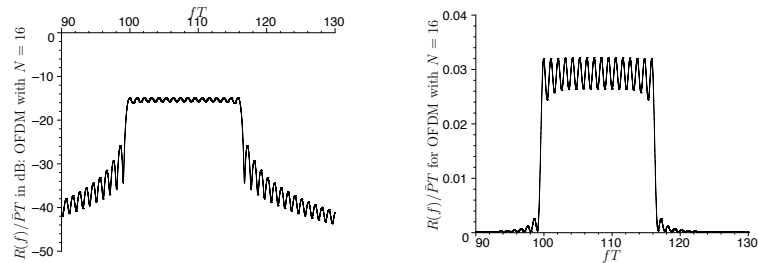
$$W \approx (N+1)f_\Delta = \frac{N+1}{1 - \Delta_h/T_s} R_s \approx N \cdot R_s, \quad N \gg 1, \Delta_h \ll T_s$$

- The **bandwidth efficiency** is then approximated by

$$\rho = \frac{R_b}{W} = \frac{R_s}{W} \sum_{k=0}^{N-1} k_n \approx \frac{1}{N} \sum_{k=0}^{N-1} k_n \text{ [bps/Hz]}$$



## Example: $R(f)$ for OFDM

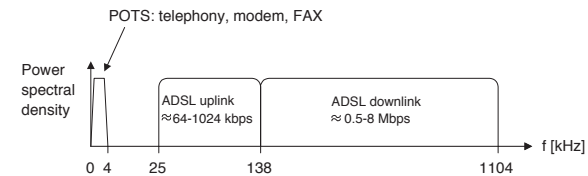


- ▶  $N = 16$  sub-carriers
- ▶  $T = T_s = 0.1$  [ms]
- ▶  $f_\Delta = R_s/0.95 = 10.53$  [kHz]
- ▶  $W \approx \frac{17}{0.95} R_s = 179$  [kHz]



## Example 2.35

**ADSL:** uses plain telephone cable (twisted pair, copper)



In ADSL, a coded OFDM technique is used. The level of the power spectral density in the downstream is roughly -73 dB. As a basic example, let us here assume that the OFDM symbol rate in the downlink is 4000 [symbol/s], and that the subchannel carrier spacing is 5 kHz. Furthermore, it is here also assumed that uncoded 16-ary QAM is used in each subchannel (assumes a very "good" communication link).

For the ADSL downlink above, determine the bit rate in each subchannel, the total bit rate, and the bandwidth efficiency.



## What about filtering away the side-lobes?

- ▶ Let us use a **spectral rectangular pulse**  $X_{srec}(f)$  of amplitude  $A = 1$  and width  $f_\Delta$  to strictly limit the bandwidth
- ▶ Similar to the time-limited case we can write

$$S_{f_\Delta}(f) = S(f) \cdot X_{srec}(f)$$

- ▶ Taking the **inverse** Fourier transform on both sides we get

$$s_{f_\Delta}(t) = s(t) * x_{srec}(t) = s(t) * Af_0 \frac{\sin(\pi f_0 t)}{\pi f_0 t}$$

- ▶ Since  $x_{srec}(t)$  is **unlimited** along the time axis, this is the case for the **filtered signal**  $s_{f_\Delta}(t)$  as well
- ▶ The signal  $x_{srec}(t)$  defines the ideal **Nyquist pulse**

As a consequence of filtering, the transmitted symbols will overlap in time domain  $\Rightarrow$  inter-symbol-interference (ISI)



## Nyquist Pulse

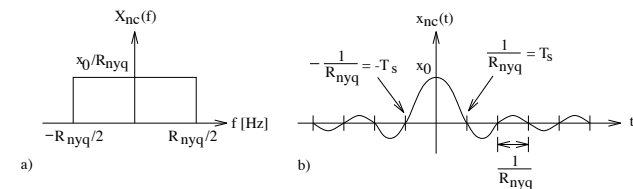


Figure 6.6: a) Ideal Nyquist spectrum; b) Ideal Nyquist pulse.

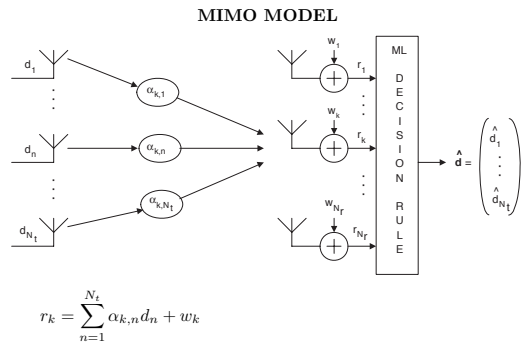
$$x_{nc}(t) = x_0 \frac{\sin(\pi R_{nyq} t)}{\pi R_{nyq} t}, \quad -\infty \leq t \leq \infty \quad (6.39)$$

$$X_{nc}(f) = \begin{cases} x_0/R_{nyq} & , |f| \leq R_{nyq}/2 \\ 0 & , |f| > R_{nyq}/2 \end{cases} \quad (6.40)$$

The Nyquist pulse and the effect of ISI will be studied in Chapter 6



## How can we further improve $\rho$ ?



- ▶ **MIMO**: multiple-input multiple output
- ▶ transmission over multiple antennas in the same frequency band
- ▶ challenge: the individual wireless channels interfere
- ▶ **5G world record 2016**: (team from Lund involved) spectral efficiency of 145.6 bps/Hz with 128 antennas



## Example: discrete frequencies in $R(f)$

- ▶ Assume  $M = 2$
- ▶ Let  $s_0(t) = 0$  and  $s_1(t) = 5$  with a pulse duration  $T = T_b/2$
- ▶ With this the average signal becomes

$$a(t) = \frac{s_0(t) + s_1(t)}{2} = 2.5, \quad 0 \leq t \leq T$$

- ▶ We can then write (within the pulse duration  $T$ )

$$s_0(t) = -2.5 + a(t), \quad s_1(t) = +2.5 + a(t)$$

### Observe:

1. this method is a waste of signal energy since  $a(t)$  does not carry any information
2. repetition of  $a(t)$  in every symbol interval creates some **periodic signal component** in the time domain, which leads to **discrete frequencies** in the frequency domain

